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SM2A-07-BP15

# NASA SUPPORT MANUAL

## APOLLO DESCRIPTION MANUAL FOR BOILERPLATE 15

151

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## INTRODUCTION

This manual pertains to the mission, and provides physical and operational descriptions of boilerplate 15, part No. B14-000002-201, manufactured by Space and Information Systems Division of North American Aviation, Inc., Downey, California. Supporting documentation and ground support equipment is described in general terms. Functional schematics and block diagrams are also included in this manual. The applicability of this manual is listed in the Index of Apollo Support Manuals and Procedures, SM1A-1.

SECTION I

MISSION AND OBJECTIVES

1-1. PURPOSE.

1-2. This section describes the mission and objectives of boilerplate 15 (figure 1-1). A mission profile is shown in figure 1-2.

1-3. BOILERPLATE 15 MISSION.

1-4. The mission prescribed for boilerplate 15 is the second in a series to develop and qualify compatibility of the Apollo spacecraft with the Saturn I launch vehicle and to define the launch and exit environmental parameters. The spacecraft will be launched by a Saturn I booster from the Atlantic Missile Range (AMR) at a launch azimuth of 90 degrees from true north. A flight azimuth of 105 degrees will be obtained soon after launch by a programed roll maneuver.

1-5. FIRST ORDER TEST OBJECTIVES.

1-6. First order test objectives of the boilerplate 15 flight test are as follows:

- a. Demonstrate the physical compatibility of the launch vehicle and spacecraft under preflight and flight conditions.
- b. Determine the launch and exit environmental parameters to verify design criteria.
- c. Demonstrate the alternate mode of launch escape tower jettison, using the launch escape and pitch control motors.

1-7. SECOND ORDER TEST OBJECTIVES.

1-8. Second order test objectives of the boilerplate 15 flight test are as follows:

- a. Demonstrate the structural integrity of the launch escape system under flight-loading conditions.
- b. Demonstrate the compatibility of the R&D communications and instrumentation systems with the launch vehicle systems.

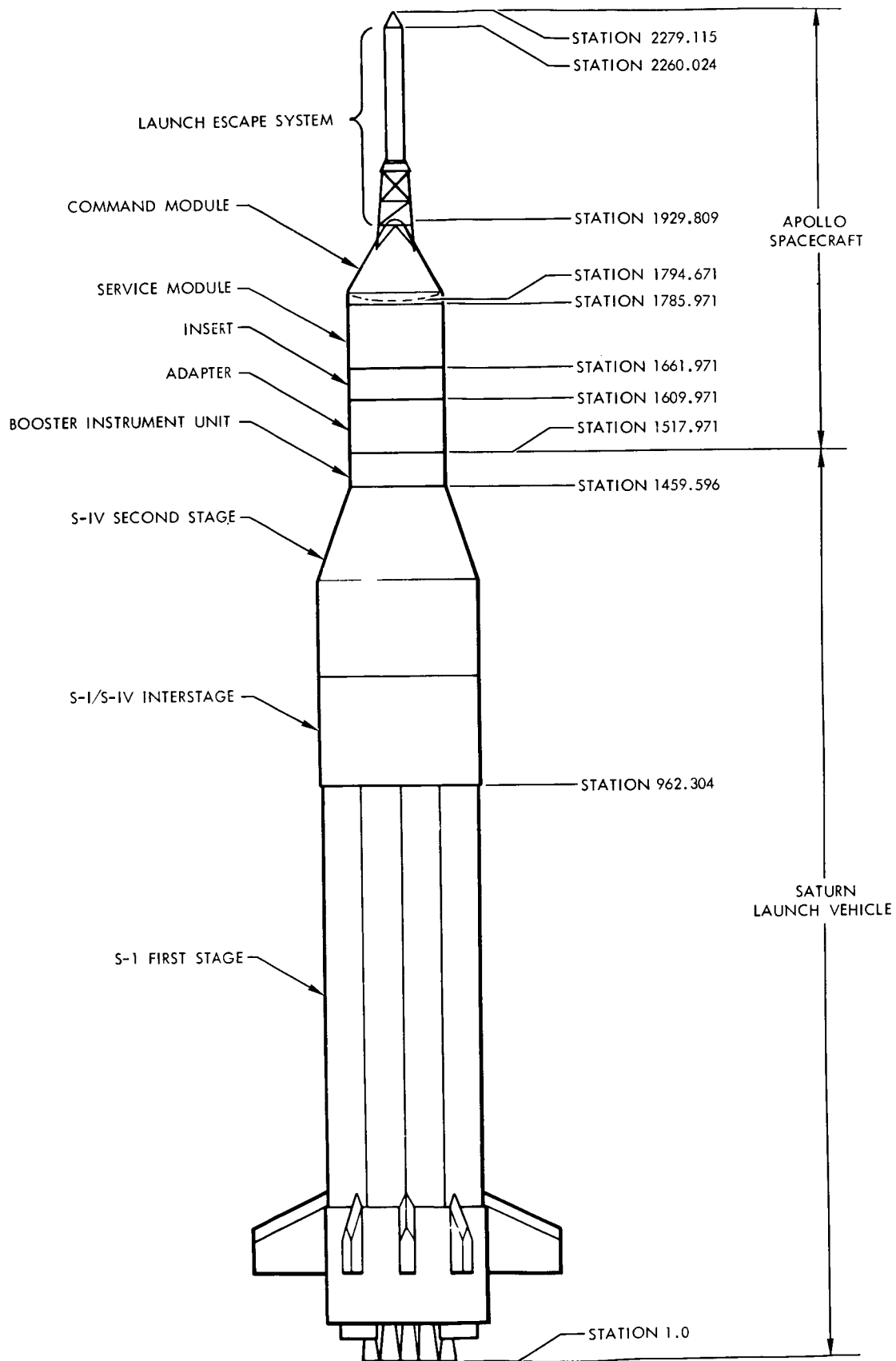
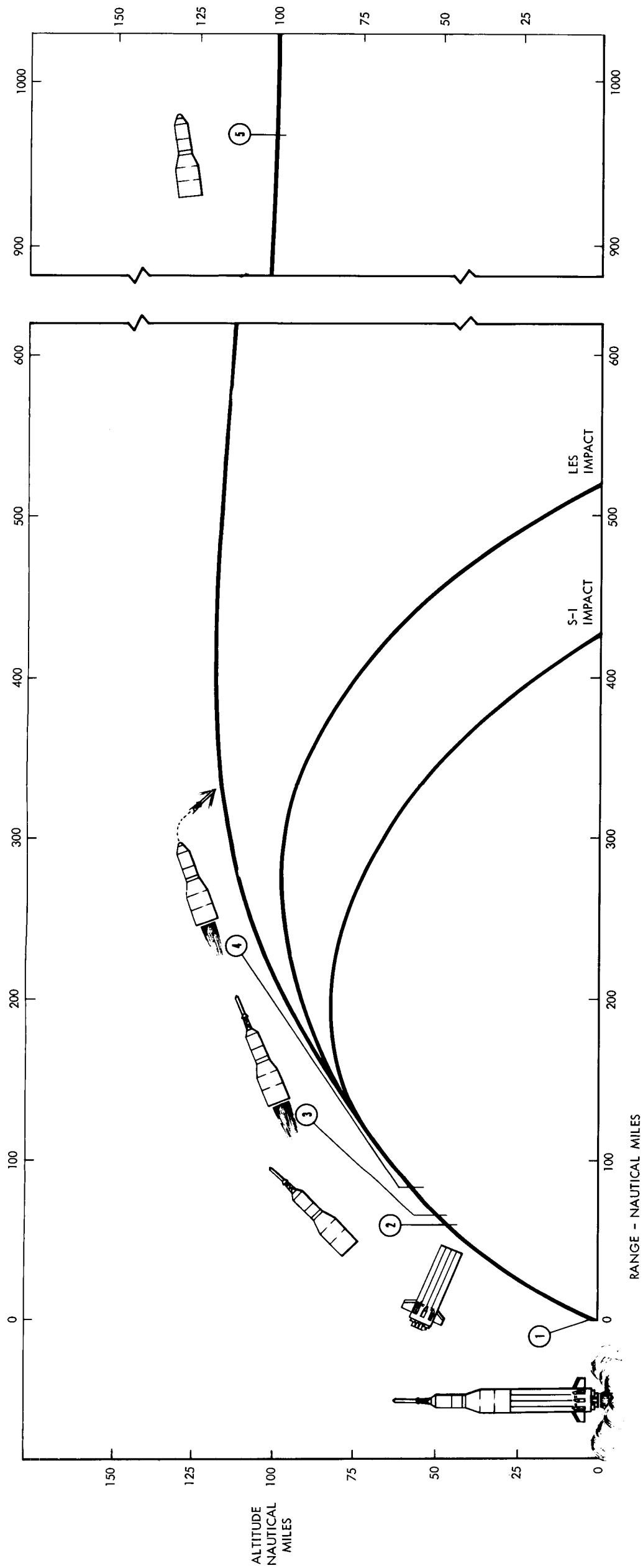


Figure 1-1. Booster Compatibility Space Vehicle





SEQUENCE OF MAJOR EVENTS					
1	LAUNCH (LIFT-OFF):	3	S-IV IGNITION	5	S-IV BURNOUT AND ORBIT INJECTION
2	S-I BURNOUT AND SEPARATION	4	LES JETTISON		

Figure 1-2. Flight Sequence and Trajectory

SECTION II  
PHYSICAL DESCRIPTION

2-1. PURPOSE.

2-2. This section contains a physical description of the launch escape system, command module, service module, insert, and adapter. The boilerplate 15 spacecraft, mounted on a Saturn I launch vehicle, comprises the complete test vehicle. (See figure 1-1.)

2-3. LAUNCH ESCAPE ASSEMBLY.

2-4. Structural relationships and physical location of the components of the assembly are shown in figure 2-1. Pertinent physical characteristics are contained in table 2-1.

Table 2-1. Launch Escape Assembly Physical Characteristics

Overall Dimensions:	
Length	33 feet
Weight	6600 pounds
Tower Structure:	
Length	118 inches
Width (top of tower)	36 inches
Width (bottom of tower)	50.6 inches
Weight	533 pounds
Structural Skirt:	
Length	18.25 inches
Diameter	48.8 inches
Weight	227 pounds (approx)
Launch Escape Motor:	
Length	185.3 inches
Diameter at nozzle exit	28 inches
Diameter of motor structure	26 inches
Weight	4767 pounds (approx)
Tower Jettison Motor:	
Length	55.6 inches
Diameter at nozzle exit	28 inches
Diameter of motor structure	26 inches
Weight	529 pounds (approx)

Table 2-1. Launch Escape Assembly Physical Characteristics (Cont)

## Pitch Control Motor Structure:

Length (includes ballast and motor structure)	18.62 inches
Diameter	26 inches
Weight	158 pounds (approx)

## Pitch Control Motor:

Length	22 inches
Diameter of body	8.79 inches
Diameter of flange	10.51 inches
Weight	47 pounds (approx)

## Ballast:

Diameter of lead discs	20.5 inches
Thickness	1.13 inches
Weight	189 pounds (approx)

## Ballast Enclosure:

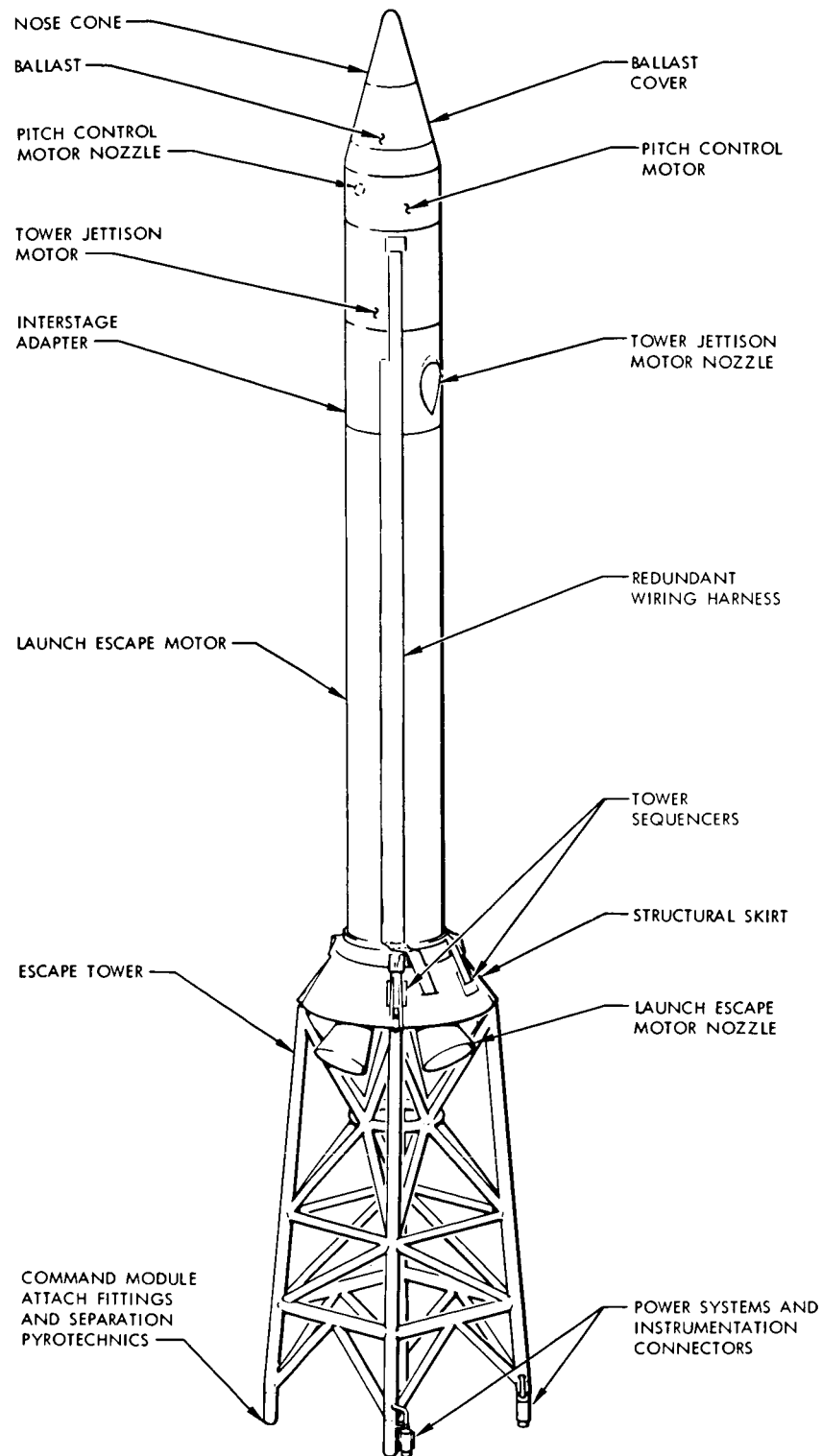
Length	29 inches
Diameter (forward end)	13.1 inches
Diameter (aft end)	26 inches
Weight	73 pounds (approx)

## Nose Cone (Q-Ball):

Length	19.09 inches
Diameter (forward end)	2 inches
Diameter (aft end)	13.03 inches
Weight	35.1 pounds (approx)

## 2-5. STRUCTURE.

2-6. A truss-type tower structure is the base of the launch escape assembly. The tower is an open frame of welded titanium tubing covered with silica-filled Buna-N rubber for insulation. Each of the four legs is attached to the command module by an explosive bolt (figure 2-2). Attachments at the top of each tower leg facilitate tower alignment (figure 2-3). A structural skirt is attached between the top of the tower structure and the base of the launch escape motor. The housing of the launch escape motor forms a structure between the structural skirt and the interstage structure. The interstage structure (figure 2-4) is a welded cylindrical structure which houses the tower jettison motor exhaust nozzles and various electrical components. Two access doors facilitate installation and removal of the components. The housing of the tower jettison motor and the pitch control motor form a structure between the interstage structure and the ballast housing. The ballast housing (figure 2-5) and the nose cone (MSFC-furnished Q-ball) are of welded Inconel sheet construction, and are bolted together to form a single conical structure to house the sheet lead ballast, sensors, and electronic modules installed in the nose cone (Q-ball).



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Figure 2-1. Launch Escape Assembly

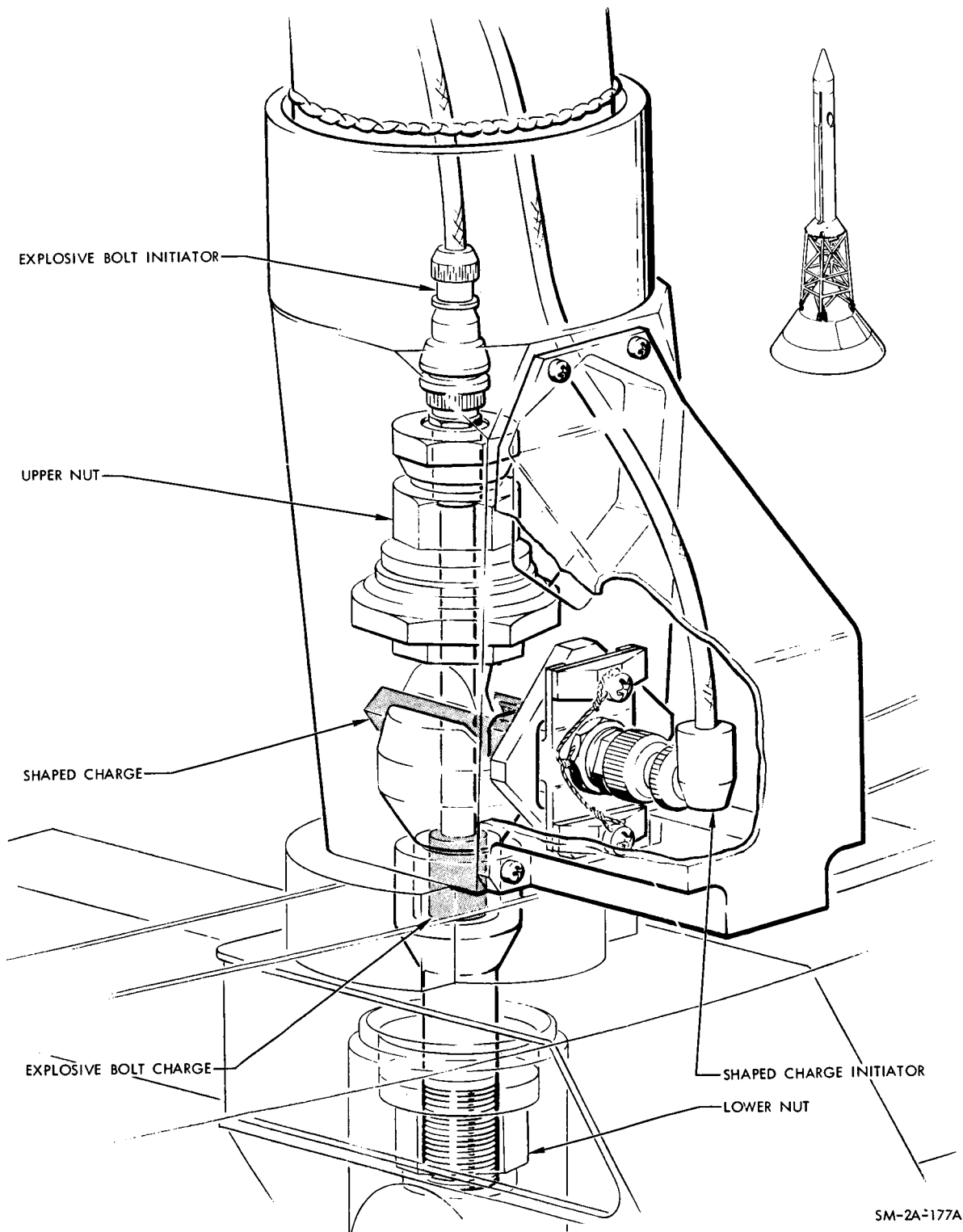
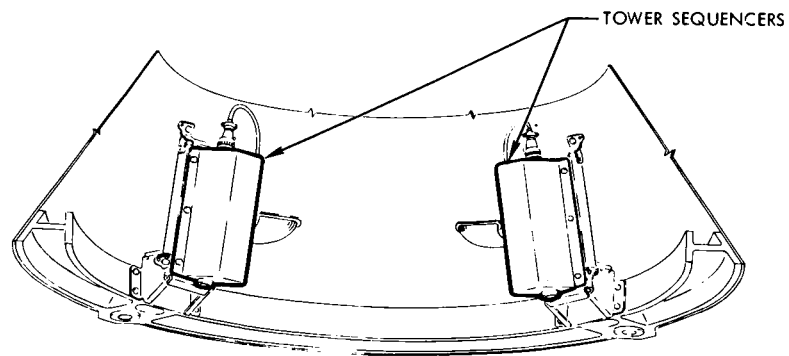
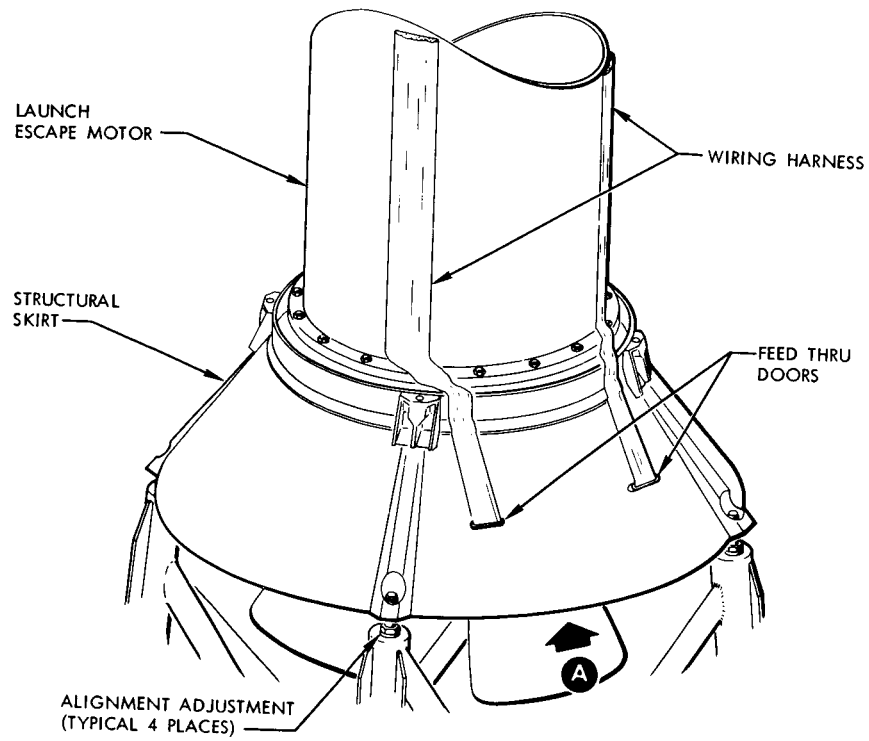


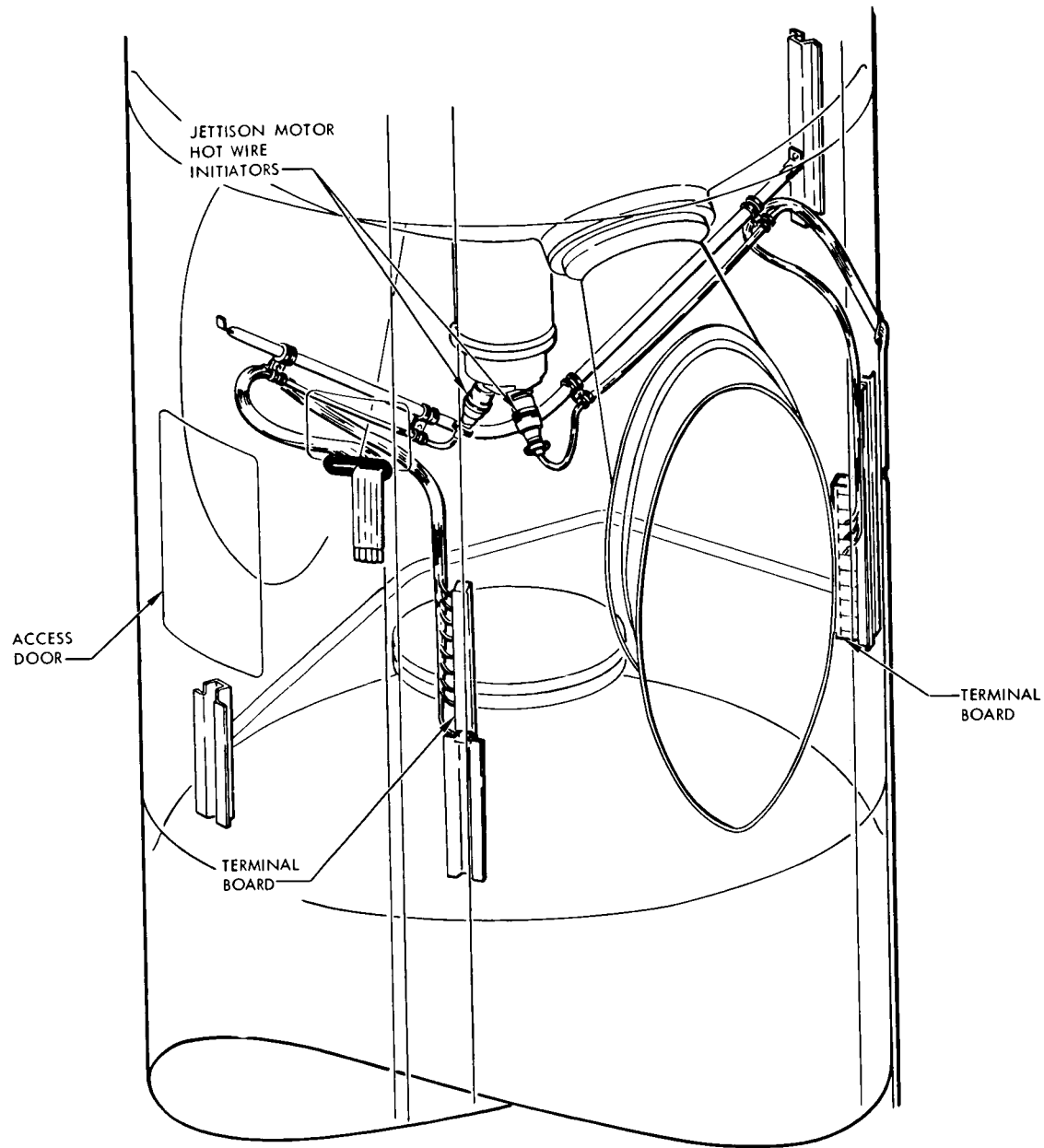
Figure 2-2. Escape Tower Explosive Bolt



VIEW A

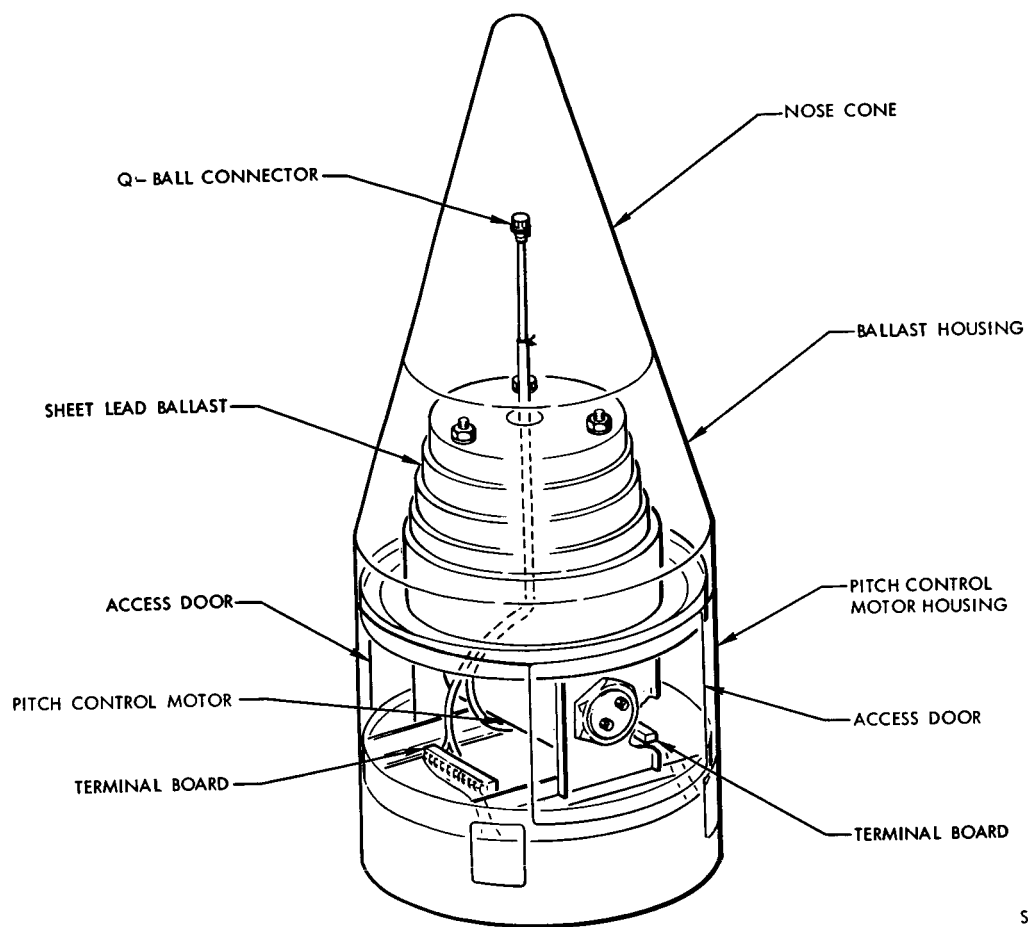
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Figure 2-3. Launch Escape Motor and Structural Skirt Area



SM-4A-60A

Figure 2-4. LES Interstage Adapter Area Components



SM-2A-377

Figure 2-5. Nose Cone and Pitch Control Motor Area



## 2-7. MOTORS.

2-8. Three launch escape assembly motors are stacked above the tower structure. The pitch control motor is located just under the ballast with the motor nozzle extending outward on a horizontal plane through the pitch control motor housing. Two doors, approximately 180 degrees apart, permit access to the hot wire initiators and associated wiring. The jettison motor (figure 2-4) is located just below the pitch control motor. Two fixed nozzles extend downward through the interstage area, canted to exit through the structure housing just above the launch escape motor fuel tank. Two doors permit access to hot wire initiators and associated wiring in the jettison motor and interstage adapter areas. The launch escape motor housing extends from the jettison motor nozzles to interface with the structural skirt. (See figure 2-3.) The four launch escape motor nozzles are canted to thrust away from the command module. Igniters are located under the structural skirt.

## 2-9. ELECTRICAL AND ELECTRONIC COMPONENTS.

2-10. The electrical and electronic components in the launch escape assembly consist of launch escape sequencers, hot wire initiators, and associated wiring harnesses and attachments. Two logic and two pyro batteries, located in the command module, supply power to operate the launch escape assembly. Redundant wiring harnesses, bonded to the exterior of the launch escape motor, and associated redundant harnesses are integral to the tower structure. Each tower structure harness has a breakaway plug that allows the harness to detach from the command module when the launch escape tower is jettisoned. The wiring harnesses provide means for connecting the rocket motor and separation circuits with the sequence controllers, and the instrumentation components with the communications equipment.

## 2-11. SEQUENCERS.

2-12. Three sequencers are provided to program the sequence of events during the mission. Two tower sequencers (figure 2-3), located on the structural skirt, are identical in size and shape. Each tower sequencer is approximately 2.5 inches in width, 8.25 inches deep, and 3.75 inches high. A mission sequencer is installed in the command module and is a single-enclosed assembly approximately 15 inches wide, 8.25 inches deep, and 7 inches high.

## 2-13. HOT WIRE INITIATORS.

2-14. The two hot wire initiators (figure 2-4) for the tower jettison motor are threaded plug devices. Both initiators contain the electrical circuitry and explosives necessary to detonate the motor igniters. The initiator body is 1 inch long with a 0.75-inch flange, 0.45 inch from the threaded end. Threads are located on one end and an electrical connector at the other end. The electrical connector contains four pins to supply power to two independent bridgewire circuits.

## 2-15. UMBILICAL CONNECTORS.

2-16. Two electrical umbilical connectors join the electrical systems of the launch escape assembly and the command module. These connectors are located on the plane-of-separation adjacent to the escape tower leg wells of the forward heat shield of the command module. The receptacle portion of the connector is attached to the command module structure. The plug is attached to the nearest tower leg by a lanyard. When the escape tower separates from the command module, the lanyard pulls the plug from the receptacle. The plugs are part of the launch escape tower wiring installation and separate with the tower. The receptacles are part of the command module wiring installation and remain with the command module.

2-17. COMMAND MODULE. (See figures 2-6 and 2-7.)

2-18. The boilerplate command module simulates the production command module in external size and shape. Physical characteristics for the command module are listed in table 2-2. The reference axes are shown in figure 2-8.

Table 2-2. Command Module Physical Characteristics

Shape	Conical
Height	134 inches
Diameter	154 inches
Weight	9262 pounds

2-19. STRUCTURE.

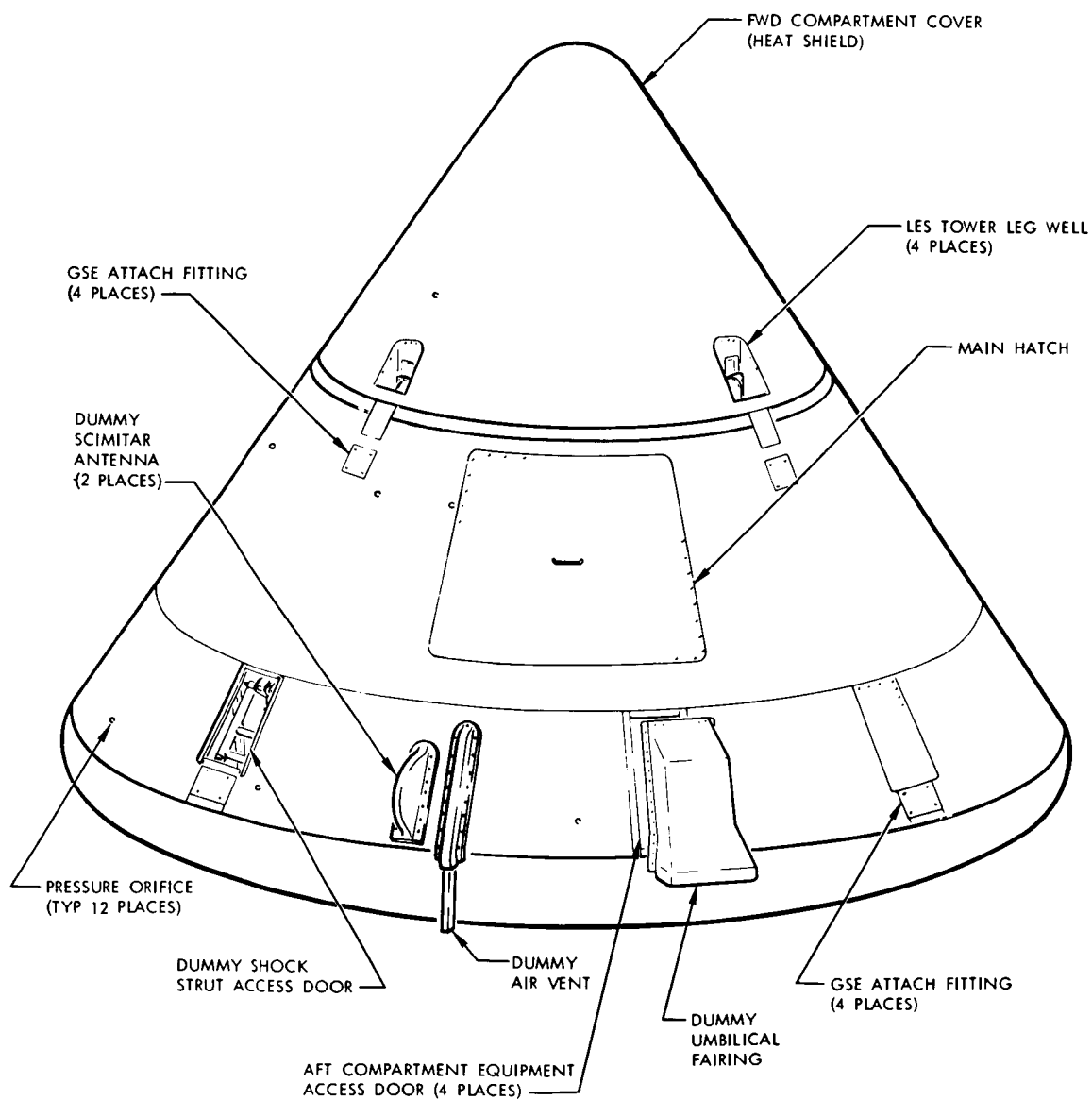
2-20. The command module structure is conical with a convex base and a rounded apex. The sides are semimonocoque aluminum structures and terminate in the forward and aft heat shields. The command module is covered with a cork material to protect the aluminum structure against aerodynamic heating. A main hatch in the side of the primary structure permits access to the interior. Shelves and brackets along the inner wall afford mounting provisions for equipment. Compartmentation is described in table 2-3.

Table 2-3. Command Module Compartmentation

Compartment	Production Configuration Function	Boilerplate 15 Contents
Primary structure	Crew compartment.	Launch escape tower sequencer, R&D communications and instrumentation, ballast to simulate weight and center of gravity, egress tube to simulate production tube volume and main hatch, and R&D cooling system.
Forward compartment	Houses parachute system of ELS, reaction thrust jets, and associated equipment.	Radome and telemetry antenna.
Aft compartment	Houses dummy shock struts, environmental control system storage facilities, and C/M to S/M umbilicals.	Aft heat shield attachment fittings, GSE attach fittings, umbilical connectors, equipment access doors, service module mating bearing pads, and tension ties.

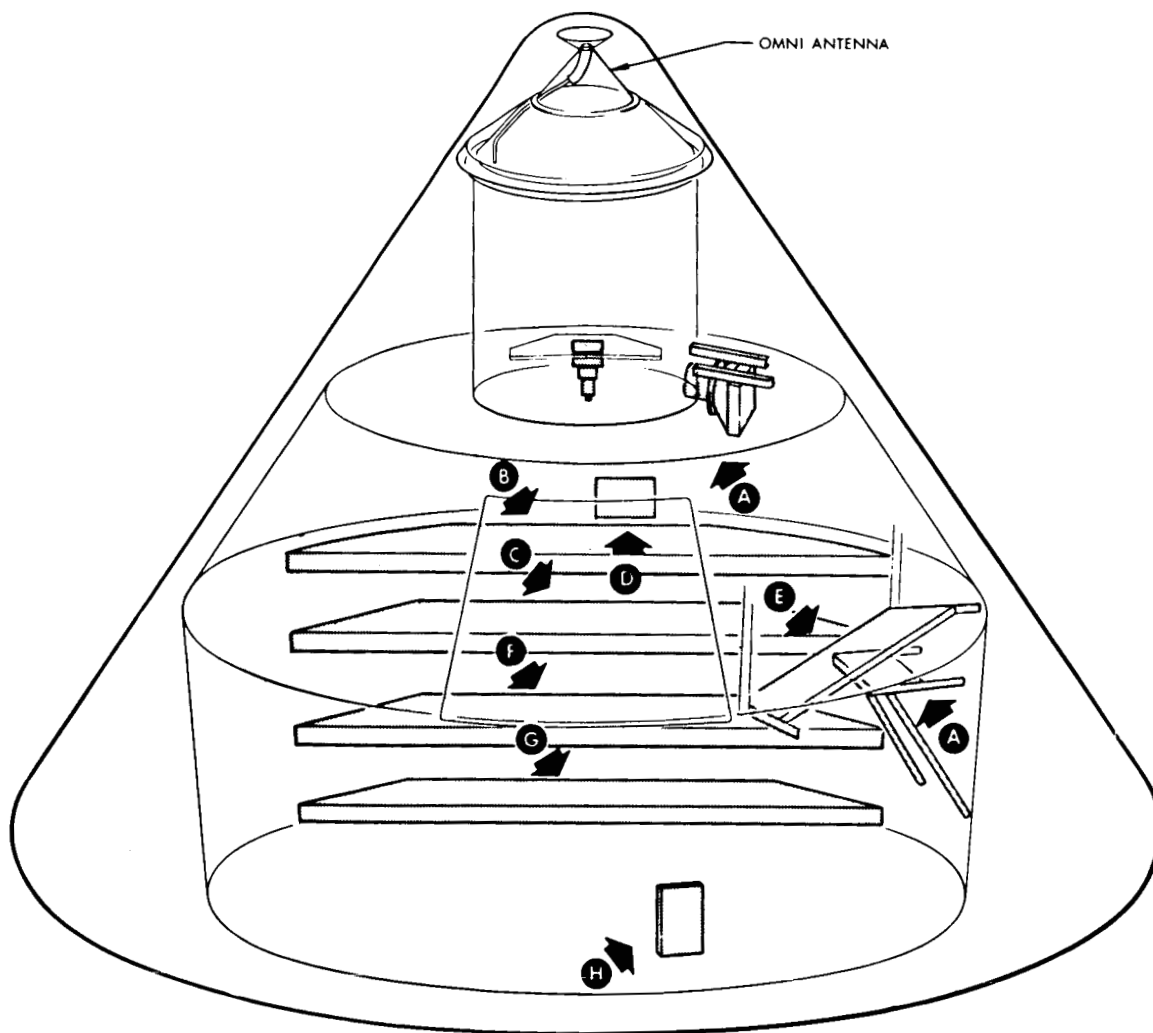
2-21. FORWARD HEAT SHIELD.

2-22. The forward heat shield forms the apex of the command module. It consists of a sheet metal cover and a fiberglass honeycomb radome assembled together with the assembly bolted to the command module. There are no provisions for separating the forward heat shield, since recovery is not planned.



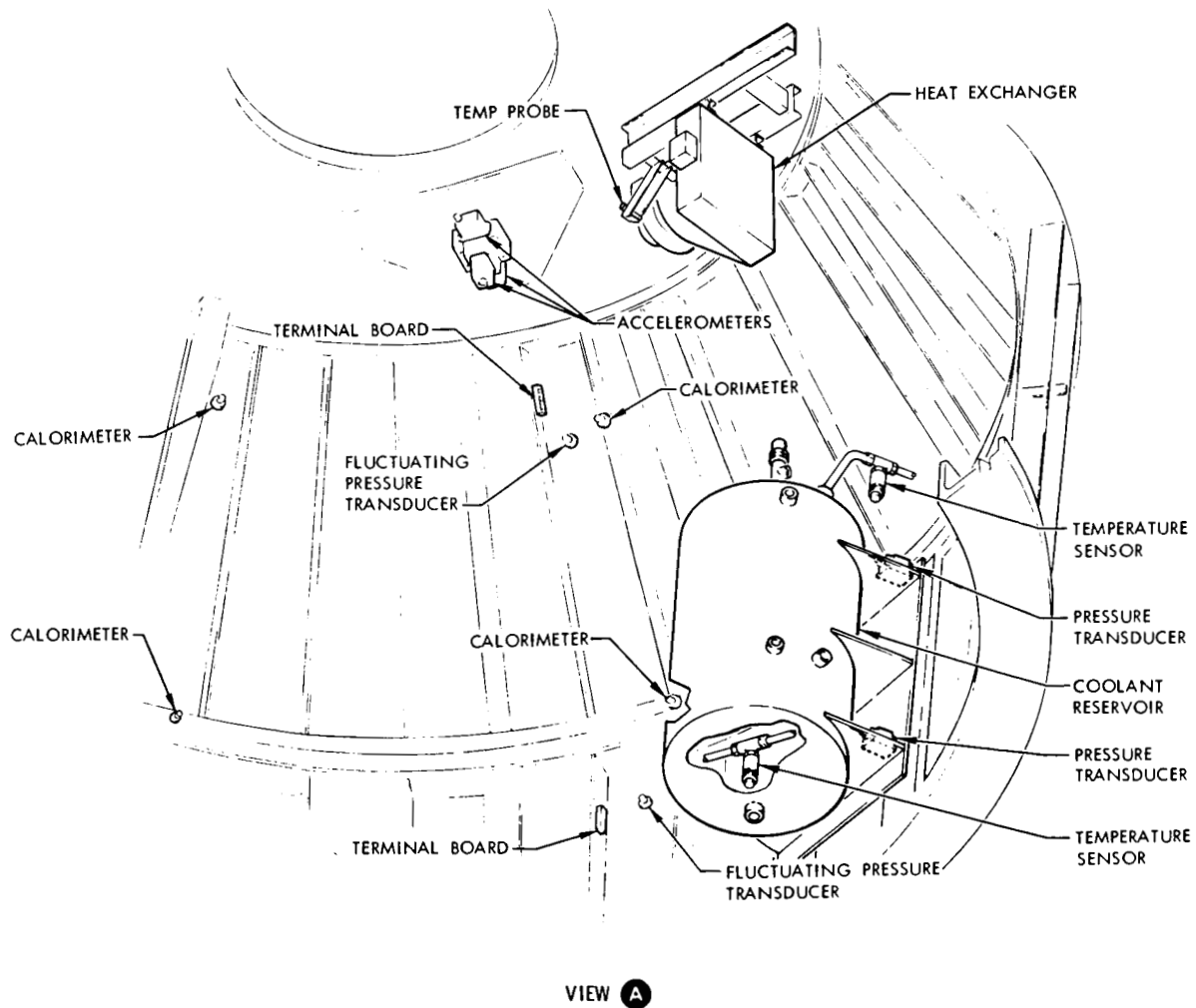
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Figure 2-6. Command Module



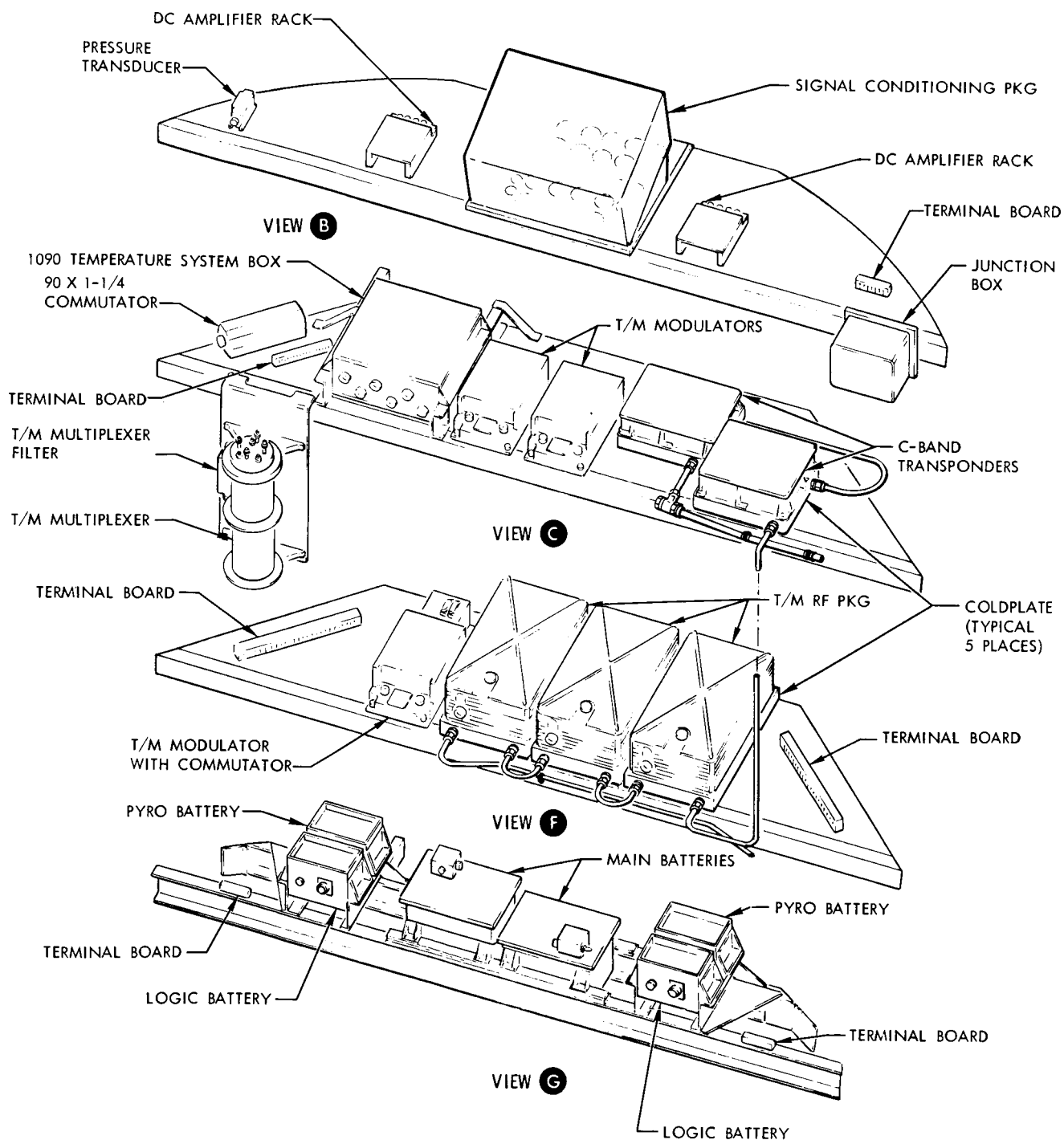
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Figure 2-7. Command Module Interior (Sheet 1 of 5)



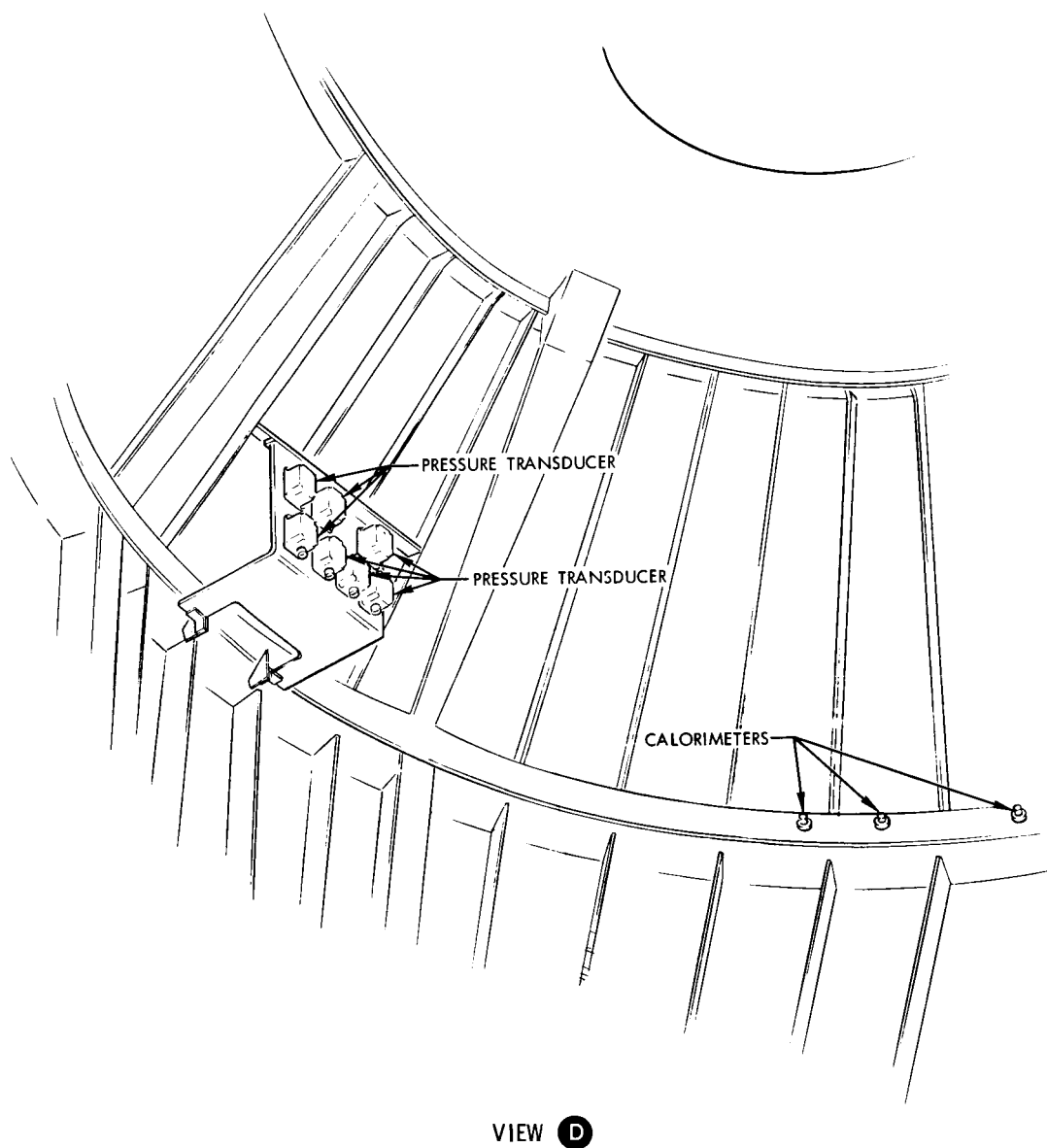
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Figure 2-7. Command Module Interior (Sheet 2 of 5)



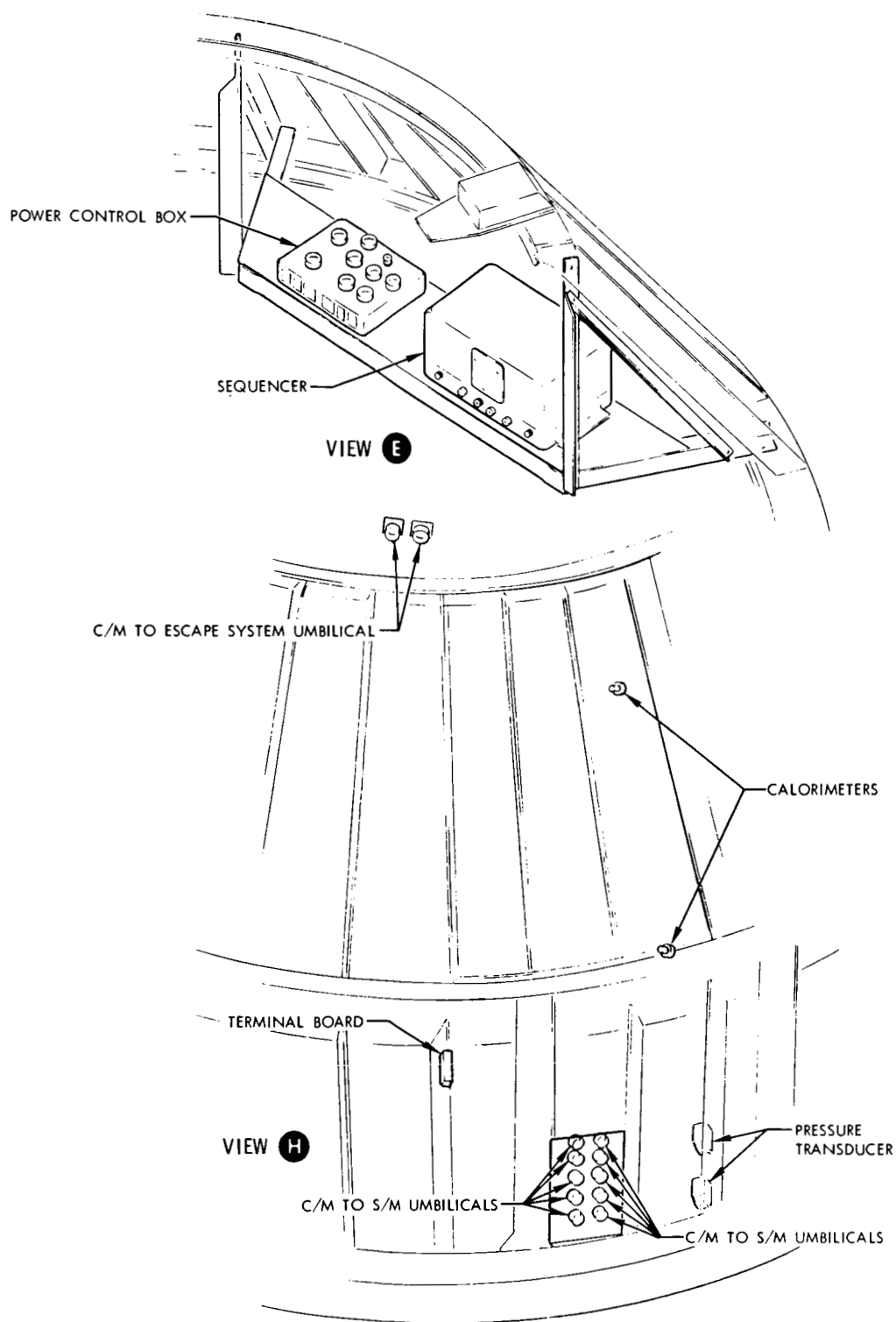
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Figure 2-7. Command Module Interior (Sheet 3 of 5)



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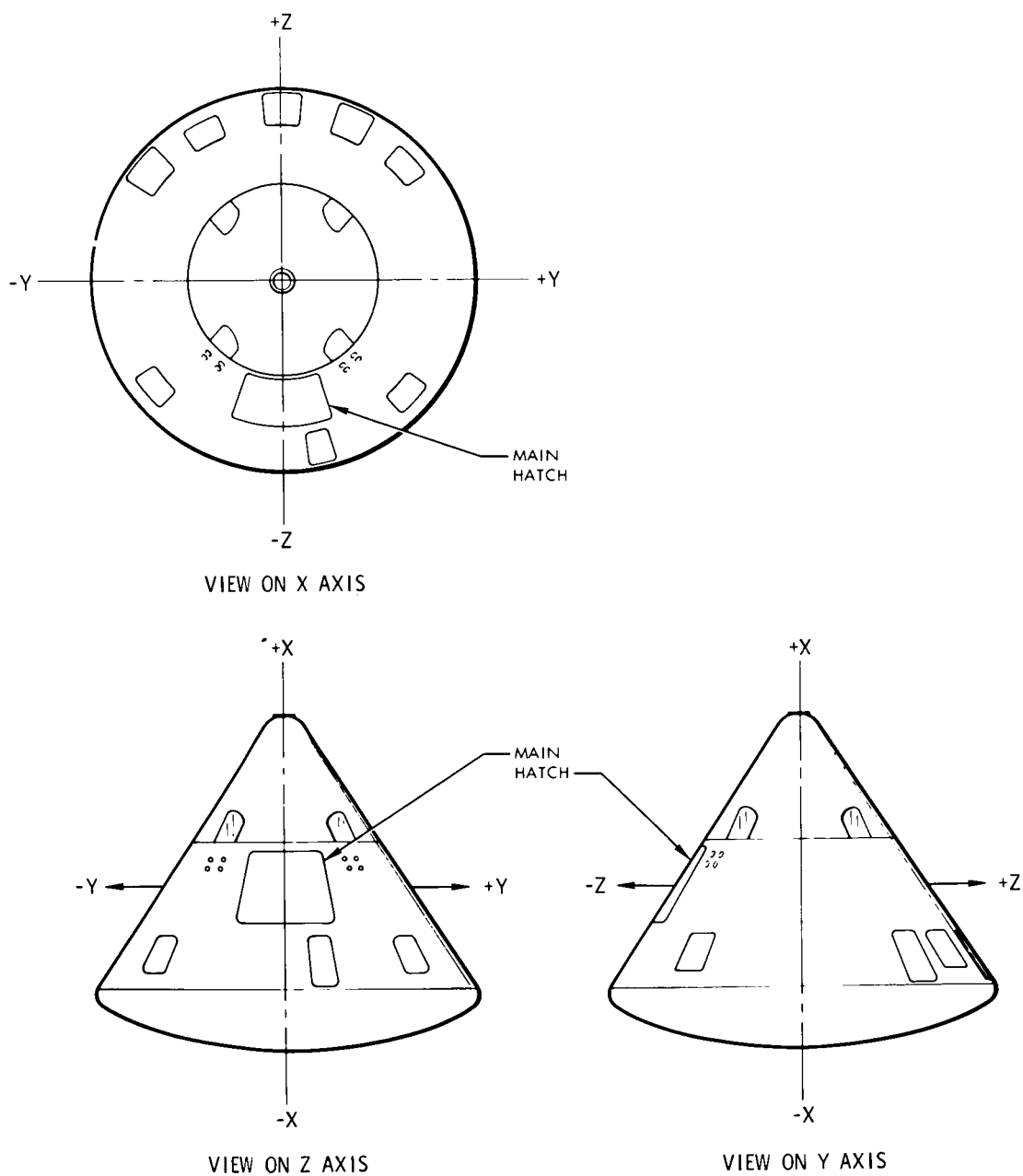
Figure 2-7. Command Module Interior (Sheet 4 of 5)



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Figure 2-7. Command Module Interior (Sheet 5 of 5)





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Figure 2-8. Command Module Reference Axis

## 2-23. AFT HEAT SHIELD.

2-24. The aft heat shield forms the convex base of the command module. It is constructed of aluminum honeycomb bonded to the inner and outer skins of the laminated fiberglass. Three adjustable struts (dummy shock struts) and one tension tie join the aft heat shield to the command module basic structure. (See figure 2-9.) Two holes are provided in the shield for installation of the umbilical electrical connectors. Nine holes are provided to permit attachment of the service module to the command module structure. Six of the holes are for the command module bearing points; the other three are for the tension-tie bolts. (See figure 2-10.)

## 2-25. INTERIOR.

2-26. The interior (crew compartment) area of the command module contains shelves and brackets for mounting the electrical power, R&D instrumentation, and equipment cooling systems. (See figure 2-7.) The interior area is insulated from the side walls with a quilted fiberglass material. The insulation helps to provide and maintain a constant temperature of not greater than 150 degrees Fahrenheit and to reduce the heat flow inside the compartment.

2-27. SERVICE MODULE, INSERT, AND ADAPTER. (See figure 2-11.)

2-28. The service module includes the insert and is used in the boilerplate 15 configuration primarily to transmit loads from the launch vehicle to the spacecraft. The command module rests on the service module at six compression bearing points. Three tension-tie bolts hold the command module mating bearing points firmly seated. The six bearing bolts are adjusted to facilitate command module-to-service module alignment. An exterior non-structural fairing is located between the command module and the service module. The fairing houses a non-functioning separation mechanism, a support structure for distributing basic loads imposed by the command module to the service module, and fixed umbilical connections between the two modules. The command module and service module will not be separated during the mission; and, therefore, no pyrotechnics are installed. The service module-to-insert and insert-to-adapter interfaces are joined with 24 bolts each. The adapter is bolted to the instrument unit using 32 bolts. The holes for these 32 bolts are cadmium plated to provide electrical bonding.

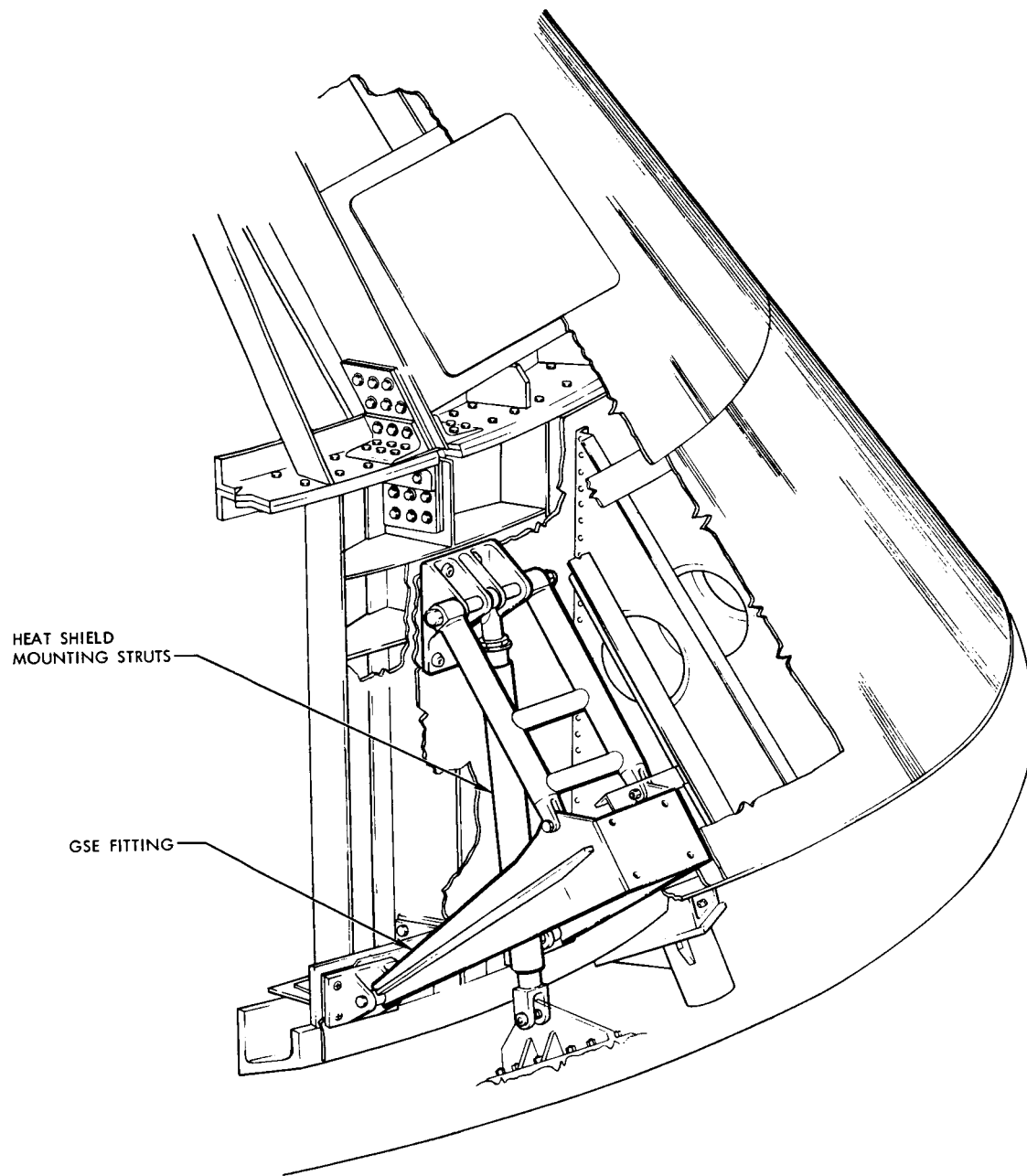
2-29. A part of the spacecraft instrumentation system is located in the service module, listed as follows:

Service module (between stations 1785.596 and 1661.596, figure 1-1)

- Seven calorimeters
- Two strain gages
- Eleven fluctuating pressure transducers
- Three vibration transducers
- Two accelerometers
- One acoustical-sensing device.

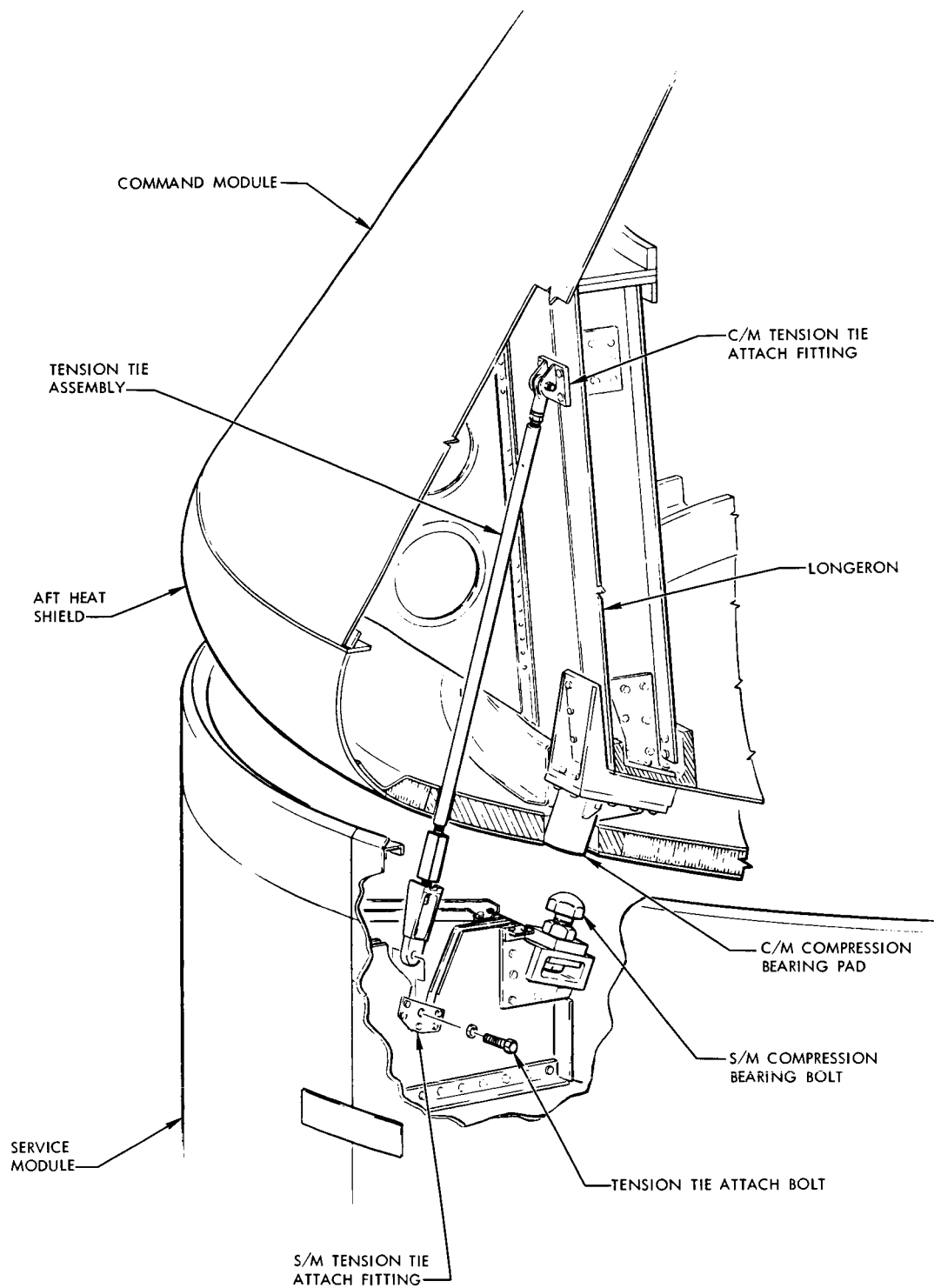
Adapter (between stations 1609.596 and 1517.596, figure 1-1)

- Four strain gages
- One calorimeter
- Two vibration transducers
- Two fluctuating pressure transducers.



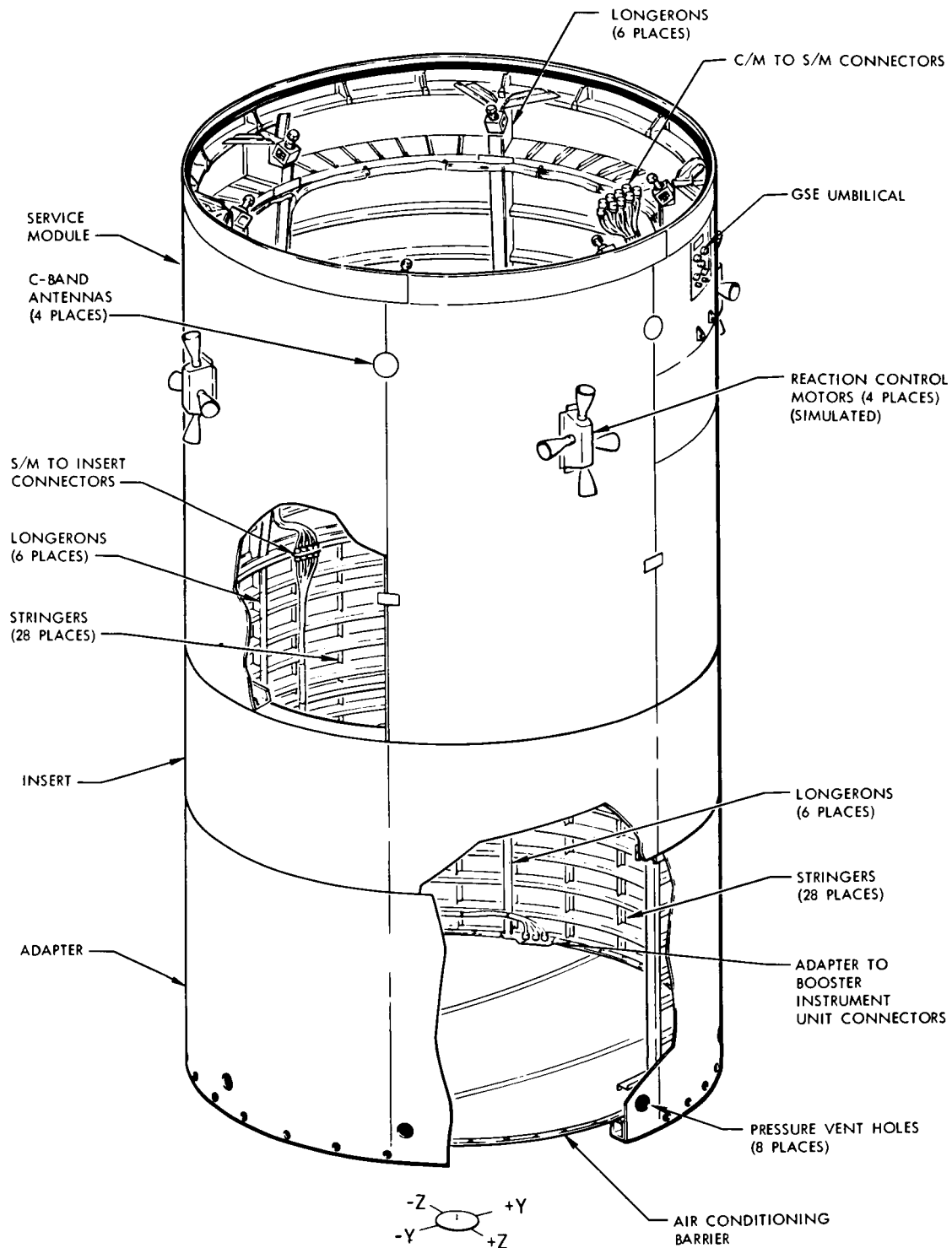
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Figure 2-9. Dummy Shock Strut and GSE Attach Fitting



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Figure 2-10. Service Module Tension Tie



SM-2A-366C

Figure 2-11. Service Module and Adapter

2-30. Ballast is installed in the service module and adapter to simulate weight and center of gravity of the spacecraft. Fiberglass reaction control system nozzles are mounted in place on the service module to simulate external configuration.

2-31. The adapter contains Apollo-Saturn interface wiring and an air-conditioning barrier in addition to the instrumentation (paragraph 2-29). The air-conditioning barrier consists of a double layer of nylon cloth impregnated on both sides with a chloroprene rubber compound. The barrier forms a bulkhead at the extreme aft end of the adapter.

#### 2-32. STRUCTURE.

2-33. The service module, insert, and adapter are cylindrical, of semimonocoque type structure, 154 inches in diameter, with an aluminum outer skin. The service module (less insert) is 124 inches in length. The skin is riveted to aluminum ring frames attached to six longerons. The longerons are T-shaped, the rim part being fabricated of steel and the web of aluminum.

2-34. The insert is 52 inches in length. The skin is riveted to upper and lower ring frames. The upper frame is composed of aluminum angles and webs riveted together; the lower frame is constructed of rectangular aluminum tubing. The upper and lower ring frames are riveted to six steel and aluminum longerons and 28 aluminum stringers.

2-35. The adapter is 92 inches in length. The skin is riveted to longerons and stringers. Eight holes in the aluminum skin, evenly spaced around the aft end of the adapter, provide venting for pressures which may build up in the adapter.

#### 2-36. INTERFACE EQUIPMENT.

2-37. Boilerplate 15 interface equipment consists of bolts, tension ties, and umbilical connectors.

2-38. TENSION TIES. (See figure 2-10.)

2-39. COMMAND MODULE-TO-SERVICE MODULE TENSION-TIE BOLTS. The tension-tie bolts utilized to bolt the command module to the service module are steel rod and turnbuckle assemblies. The assemblies are cadmium plated. The turnbuckle is used to preload the command module to the service module compression bearing points. The assemblies are approximately 42 inches long. Two of the assemblies use 7/8-inch hexagon steel rods 28.5 inches long. The third tie at longeron No. 1 uses 1-1/4-inch round steel rod 28.6 inches long on which hexagonal wrench flats have been machined. No pyrotechnic charges are installed on boilerplate 15 configuration. The tension tie at longeron No. 1 also is utilized as a vertical strut to help hold the aft heat shield in place.

#### 2-40. UMBILICAL CONNECTORS.

2-41. The umbilical connectors on boilerplate 15 consist of electrical connectors and plugs located in the planes-of-separation of the modules, a GSE umbilical connector for ground support equipment, and a coolant umbilical connector. These connectors join the electrical systems of the modules while the modules are attached and provide a means of disconnecting the electrical systems upon module separation. There is no requirement for module separation during boilerplate 15 mission; therefore, the necessary hardware for umbilical disconnect is omitted except for GSE separation. The GSE umbilical supplies the electrical power while the boilerplate is on the pad. The coolant umbilical supplies the fluid coolant from GSE equipment on the pad.

2-42. GSE UMBILICAL CONNECTOR. A GSE umbilical is located in the skin of the service module approximately 18 inches below the top, on the +Z-plane (figure 2-8). This umbilical is equipped with a primary (pneumatic) and a backup (hydraulic) release mechanism. Both systems are armed by a signal from NASA control GSE. Pneumatic and hydraulic pressures are supplied by facility equipment. On initial command, a solenoid actuates the nitrogen pressure which ejects the umbilical. If this system fails to operate, 10 milliseconds later, a hydraulic actuator trips a lanyard which then disconnects the umbilical.

2-43. COMMAND MODULE-TO-SERVICE MODULE UMBILICAL CONNECTORS. Umbilical connector receptacles are recessed into the outer surface of the aft heat shield of the command module. They are approximately 12 inches from the outer edge and located near longeron No. 6. The receptacles are part of the command module aft compartment wiring installation. The plug portions of the connectors are part of the service module wiring installation.

2-44. SERVICE MODULE-TO-INSERT UMBILICAL CONNECTOR. Umbilical connector receptacles on the aft separation plane of the service module connect the plugs located in the extension forward end.

2-45. ADAPTER-TO-INSTRUMENT UNIT UMBILICAL CONNECTOR. Umbilical connector receptacles on the aft separation plane of the adapter, connect to plugs located in the forward end of the booster instrument unit. The instrument unit will not be separated from the adapter.

2-46. LAUNCH VEHICLE. (See figure 1-1.)

2-47. The boilerplate 15 launch vehicle is a Saturn I configuration (designated SA-6) consisting of a Saturn S-I first stage, a Saturn S-IV second stage, and a booster instrument unit.

2-48. FIRST STAGE.

2-49. The S-I stage is powered by eight Rocketdyne H-1 engines with a total thrust of 1,500,000 pounds. Propellants for these engines consist of 850,000 pounds of oxidizer LO<sub>2</sub> and fuel RP-1. The general appearance is cylindrical with aerodynamic stabilizing fins at the extreme aft end of the cylinder. The airframe is approximately 21 feet in diameter and is approximately 80 feet in length. First stage engine cutoff occurs 147.7 seconds after ignition. An S-I/S-IV interstage section 18 feet in diameter is jettisoned with the first stage.

2-50. SECOND STAGE.

2-51. The S-IV stage is powered by six Pratt & Whitney RL10-A3 engines with a total thrust of 90,000 pounds. Propellants for these engines consist of 100,000 pounds of oxidizer LO<sub>2</sub> and fuel LH<sub>2</sub>. The airframe is approximately 18 feet in diameter with the forward end tapering to 13 feet to interface with the instrument unit and the spacecraft. The S-IV booster burns 473.8 seconds, placing the booster, instrument unit, and spacecraft into orbit approximately 100 nautical miles from earth. No recovery is planned.

2-52. BOOSTER INSTRUMENT UNIT.

2-53. The instrument unit interfaces with the booster and spacecraft. It is approximately 13 feet in diameter and contains the guidance and control system, flight sequencers, booster telemetry system, tracking system, and electrical power system.

### SECTION III

#### LAUNCH ESCAPE SYSTEM

#### 3-1. PURPOSE.

3-2. The boilerplate 15 launch escape system will demonstrate the structural adequacy of the design by the static and dynamic loads imposed while on the ground, and during lift-off and boost phases.

#### 3-3. OPERATIONAL DESCRIPTION.

3-4. The operational description of the launch escape system (from prelaunch to tower jettison) is as follows: The mission sequencer logic bus and tower sequencer pyro bus are armed prior to booster ignition by manual commands. The mission sequencer logic circuitry arms an S-I/S-IV separation relay in the booster instrument unit. At time of S-I/S-IV separation, the relay closes and a 12-second timer in the instrument unit is activated. At time runout, the separation-plus-12-second signal operates the relay motors in the tower sequencers, closing the motor and separation squib contacts, and thus supplying 28 volts simultaneously to all jettison motor and separation squibs. Figure 3-1 is a functional block diagram showing sequence of events. Table 3-1 is a time history of the events leading to tower jettison.

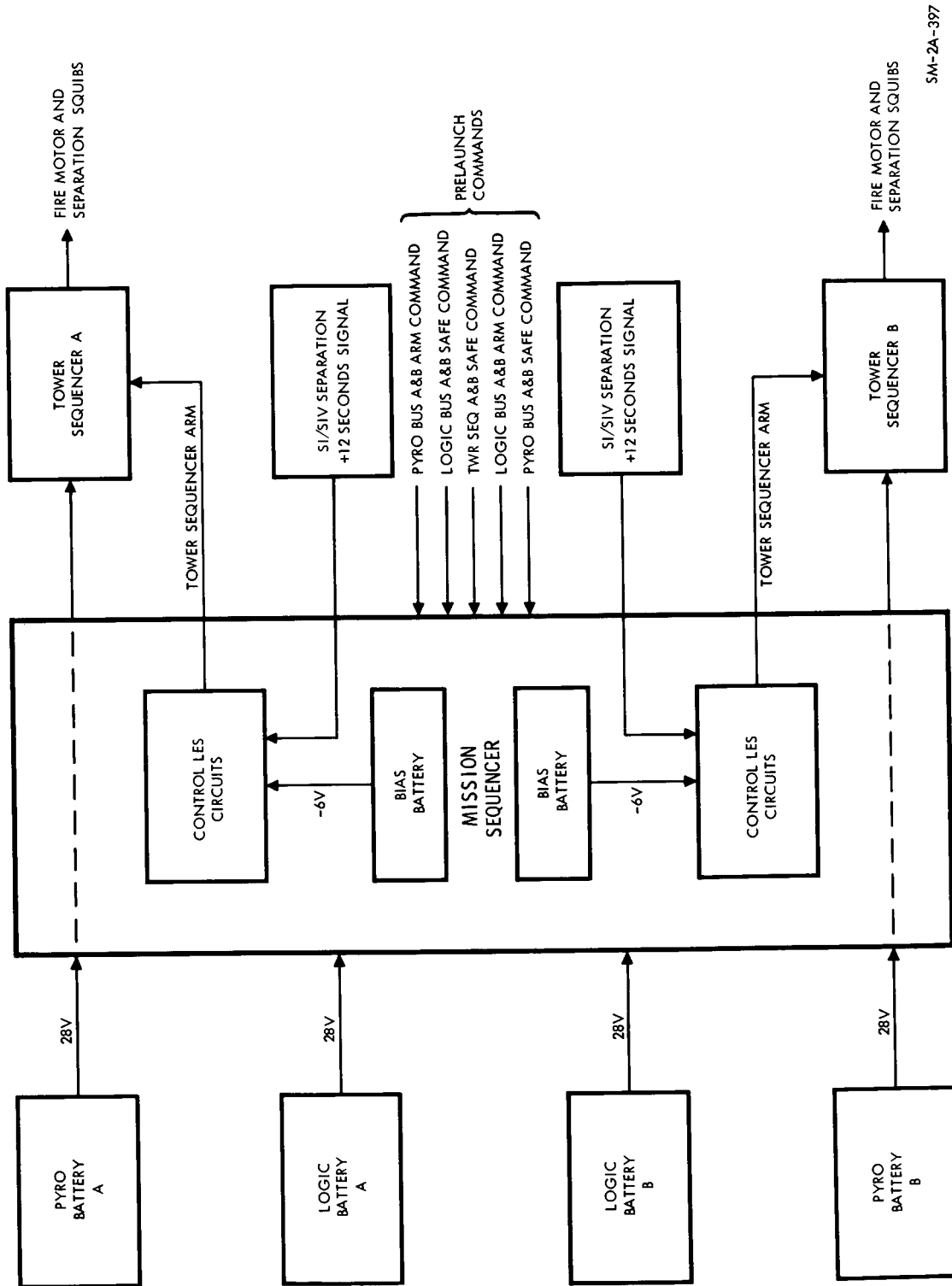
Table 3-1. Time History of Events Leading to Tower Jettison

Time (Seconds from Ignition)	Event	Velocity (Feet/ Second)	Altitude (Feet)	Dynamic Pressure (Pounds/ Foot <sup>2</sup> )	Flight Path Angle (Deg)	Range (KM)	Mach No.
T - 3.42	S-I ignition	0	0	0	90	0	0
T + 0	Lift-off		0	0	90		0
T + 69.5	Max Q	1481	38,770	720	58.7		1.5
T + 141.7	S-I inboard Eng. cutoff	8212	198,187	28.3	25.8		7.9
T + 147.7	S-I burnout	8718.3	219,886	11.0	24.8	50	8.9
T + 150.7	S-IV ignition	8678.4	230,750	7.0	24.4	55	9.1
T + 161.7	Escape tower	8752.5	265,581	1.3	22.8	67	10.3

#### 3-5. MOTOR IGNITION.

3-6. Each motor ignition system contains two electrical hot wire initiators threaded into pyrotechnic cartridges which fire the igniter of the motor. Redundant initiators are employed for increased reliability. Current passing through low resistance wires detonates the cartridge, which ignites the rocket motor igniter. The initiator body is 1 inch long with a 3/4-inch flange, 0.45 inch from the threaded end. The electrical header contains two independent hot wire circuits and four pins. The initiator ignites within 10 milliseconds when one bridgewire is subjected to a firing current of 3.5 amperes. The pressure level of the explosive charge is produced within 12 milliseconds after application of current. The igniter for the tower jettison motor is installed in the aft dome of the rocket motor. The propellant grain is an 8-point configuration of boron potassium nitrate.





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Figure 3-1. Launch Escape System Functional Block Diagram

### 3-7. TOWER SEPARATION.

3-8. The tower separation system consists of four explosive bolts (figure 2-2) that secure the tower to the command module. Each bolt contains two charges, the explosive bolt charge and the shaped charge. The explosive bolt charge is contained in the center of the bolt and the shaped charge is just below the bolt head. Both charges are fired simultaneously. Release of the tower is accomplished by simultaneous detonation of the four explosive bolts. The hot wire initiators for the bolts are ignited by 28-volt d-c signals received from the mission sequencer through the tower sequencers. The initiators will detonate to fire the explosive bolts within 5 milliseconds. To accomplish tower jettison, the mission sequencer simultaneously initiates detonating signals to the explosive bolts and to the tower jettison motor hot wire initiators. The entire launch escape assembly is released and pulled clear of the spacecraft trajectory. The tower to command module umbilical connections are disconnected automatically when tower separates from the command module.

### 3-9. LAUNCH ESCAPE MOTOR.

3-10. The launch escape motor is a solid-propellant motor with four nozzles nominally canted 35 degrees from the mean motor centerline. The resultant thrust vector of 2.3 degrees is obtained by a difference in exhaust nozzle throat area. The propellant capacity is approximately 3000 pounds, giving the motor a gross weight of approximately 4800 pounds. Effective thrust developed is approximately 155,000 pounds at 36,000 feet altitude, at 70 degrees Fahrenheit grain temperature. Burning time is 3 seconds at nominal thrust with burnout at 8 seconds.

### 3-11. PITCH CONTROL MOTOR.

3-12. The pitch control motor is a solid-propellant reaction motor. The motor provides up to 3400 pounds of thrust for 0.5 second in the minus Z-direction, producing a positive pitch rate about the Y-axis to provide displacement.

### 3-13. LAUNCH ESCAPE TOWER JETTISON MOTOR.

3-14. The tower jettison motor is a solid-propellant motor that provides the thrust for separation of the launch escape tower and related equipment from the command module. The jettison motor is mounted on top of the inert escape motor. Passive thrust vector control in the form of offset exhaust nozzles provides a trajectory that arcs slightly in the pitch-up direction. For operational characteristics of the jettison motor, refer to table 3-2.

Table 3-2. Operational Characteristics of Launch Escape Tower Jettison Motor

Thrust	33,000 pounds
Duration	1 second
Time required to reach 90-percent maximum thrust	75 to 125 milliseconds
Angles between resultant thrust axis and motor:	
Pitch plane	2 degrees $\pm$ 30 minutes
Yaw plane	0 degrees $\pm$ 30 minutes

3-15. MISSION SEQUENCER. (See figure 2-7, sheet 5, view E, and figure 3-2.)

3-16. The mission sequencer located in the command module controls the sequence of events that are necessary to execute a successful launch escape tower jettison operation. The sequencer contains the logic circuits to direct the timing and order of the electrically initiated steps of the mission. Complete redundancy of the entire sequential network is provided for reliability. The mission sequencer logic circuits send electrical signals to operate the motor switches in the tower sequencer for firing the explosive bolt squibs and igniting the tower jettison motor. Table 3-3 gives mission sequencer functions. In addition, the mission sequencer provides compatibility for monitoring critical events as they occur, thus providing an input to the instrumentation system.

3-17. TOWER SEQUENCERS. (See figures 2-3 and 3-3.)

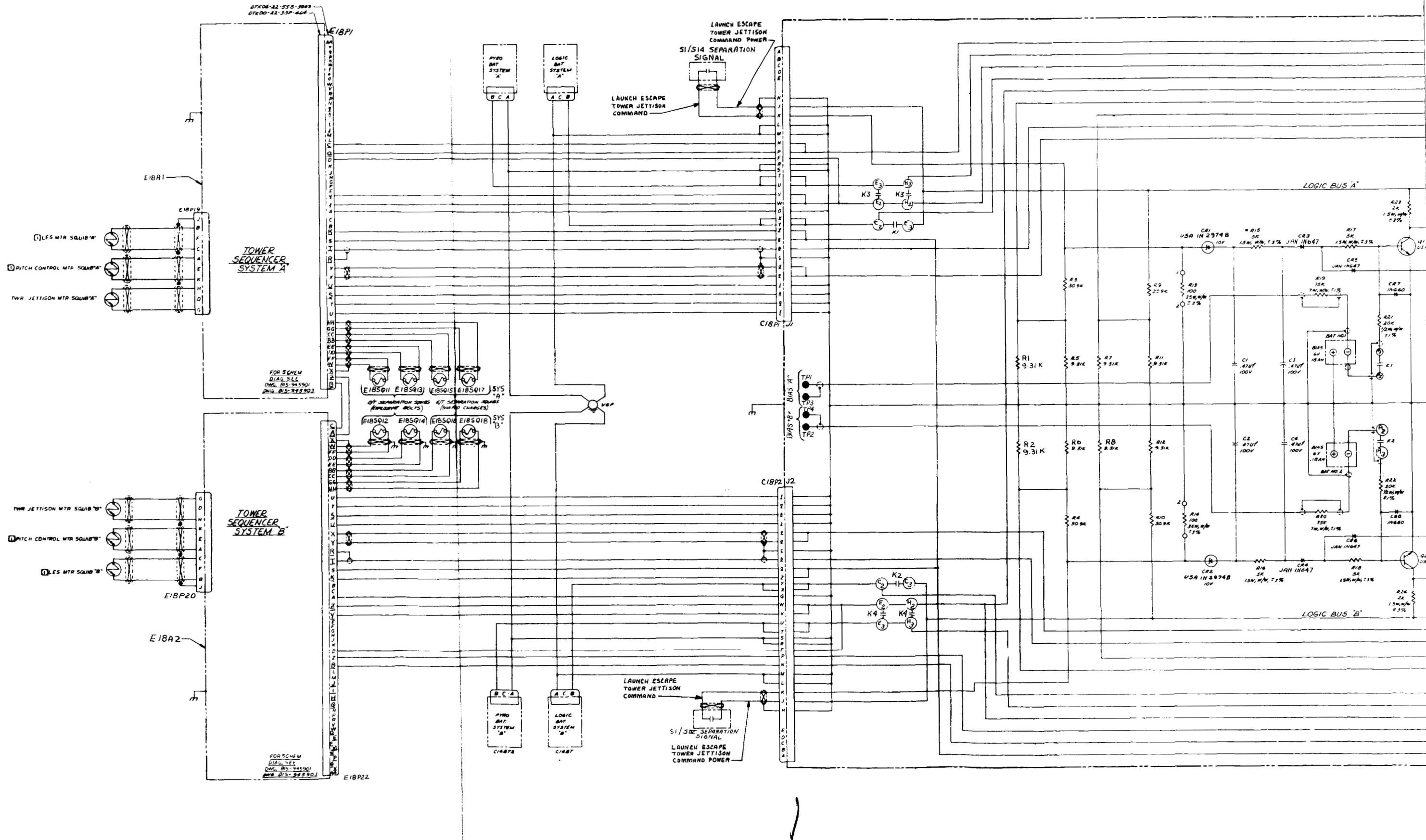
3-18. Two tower sequencers are attached to the underside of the structural skirt. Each sequencer has one motor-driven switch. An output voltage from the mission sequencer drives each motor-driven switch to the ARM position. The switches then allow electrical power from the pyro bus to simultaneously fire the tower separation explosive bolts, shaped charges, and jettison motor igniter. The sequencer provides circuits for monitoring the functional status of the control circuits via GSE during checkout operations. Use of two sequencers provides total redundancy for reliability.

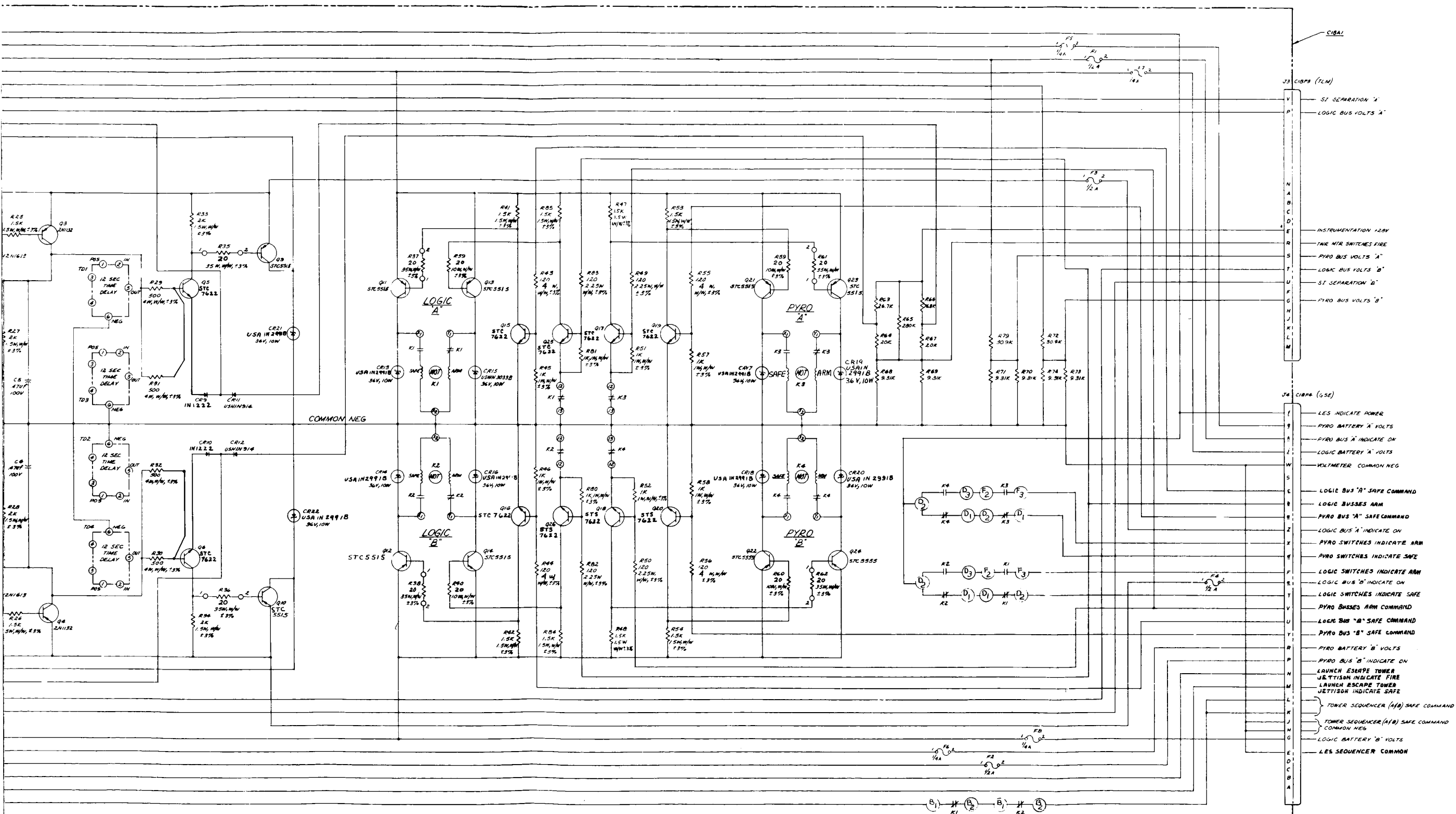
Table 3-3. Mission Sequencer Functions

Signal	Function	Time	Controlling Components	Signal Source
Logic bus A & B arm command	Supplies base voltage for transistorized switching network to energize coils of motor-driven switches C18K1 and C18K2.	Prelaunch	C18J4-b	GSE
Logic bus A & B	Supplies collector voltage to transistorized switching network to energize coils of motor-driven switches E18K1 and E18K2 and to arm contacts of S-I separation signal.	Prelaunch	C18K1 and C18K2, C18J4-X, C18J4-Y, C18J2-X, and C18J2-Y	Logic batteries A and B
Pyro bus A & B arm command	Supplies base voltage for transistorized switching network to energize coils of motor-driven switches C18K3 and C18K4.	Prelaunch	C18J4-V	GSE
Pyro bus A & B	Supplies voltage to firing contacts of E18K1 and E18K2.	Prelaunch	C18K3 and C18K4, C18J1-T, C18J1-U, C18J2-T, and C18J2-U	Pyro battery A

Table 3-3. Mission Sequencer Functions (Cont)

Signal	Function	Time	Controlling Components	Signal Source
S-I separation	Supplies base voltage to transistorized switching network to energize coils of motor-driven switches E18K1 and E18K2.	S-I separation plus 12 seconds	IV programmer C18J1-J, C18J1-K, C18J2-J, and C18J2-K	Logic bus A and B
Launch escape tower jettison	Supplies firing voltage to tower jettison motor and launch escape tower separation squib initiators.	S-I separation plus 12 seconds	E18K1 and E18K2	Pyro bus A and B





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Figure 3-2. Mission Sequencer Schematic Diagram

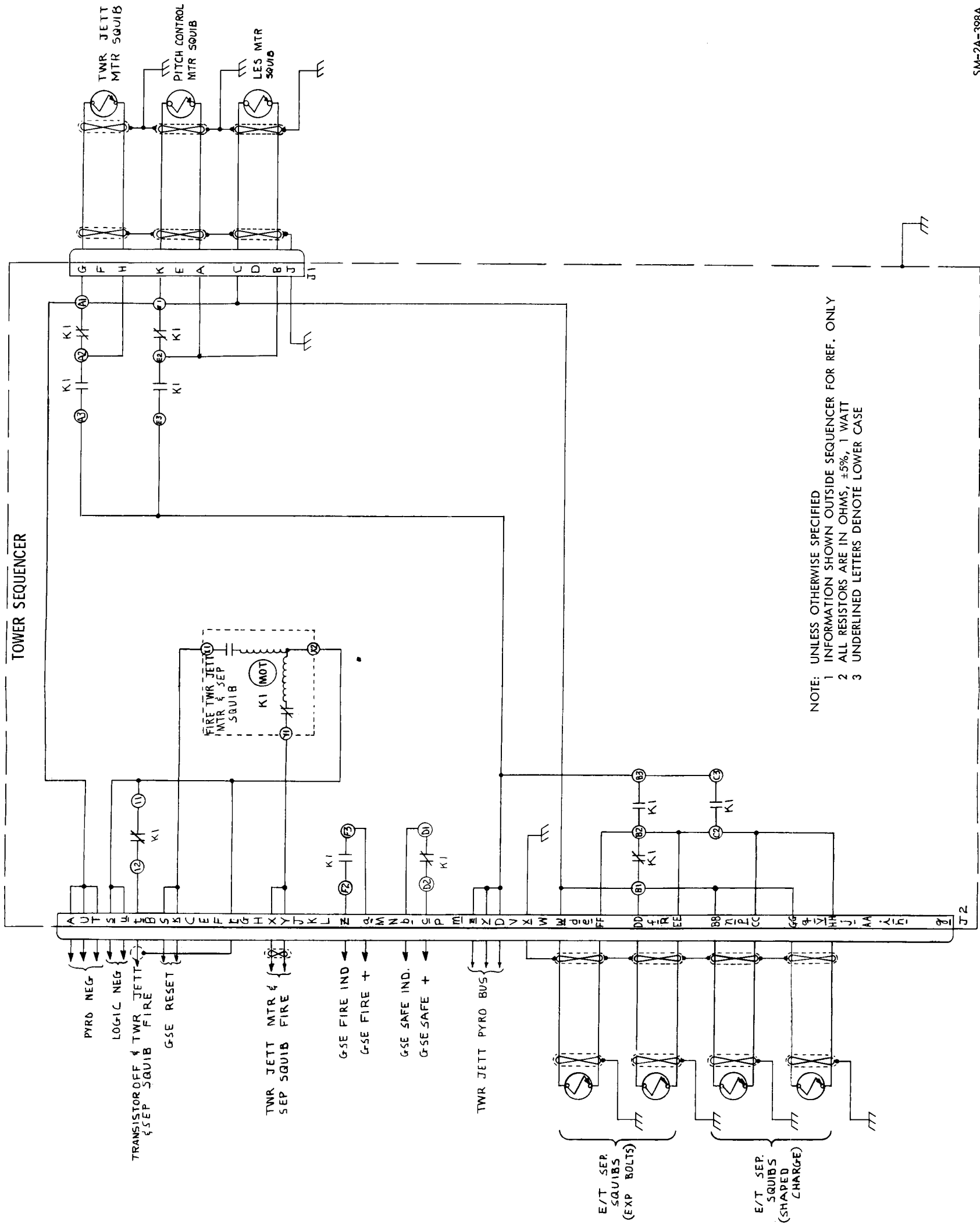


Figure 3-3. Tower Sequencer Schematic Diagram

## SECTION IV

## COMMUNICATIONS AND INSTRUMENTATION

4-1. PURPOSE.

4-2. The communications and instrumentation system provides a means of acquiring and conditioning preselected information and of transmitting this information to earth monitoring equipment. (Refer to table 4-1 for measurement list.) The system also provides for tracking of the spacecraft during the mission. The Q-ball contains some instrumentation equipment, the information being used for booster guidance system performance evaluation. The Q-ball system is not connected functionally with the Apollo communications and instrumentation system but is described in this section.

4-3. DESCRIPTION. (See figure 4-1.)

## NOTE

For detailed descriptive and checkout information for the R&D electronic equipment furnished by NASA, refer to applicable NASA document.

## 4-4. COMMUNICATIONS EQUIPMENT.

4-5. Communications R&D equipment consists of the telemetry system and radar transponders.

4-6. **TELEMETRY SYSTEM.** The telemetry system consists of three FM/FM telemetry subsystems, one system containing two PAM channels, the transmitters of each operating into the antenna system. Besides the transmitter, each telemetry subsystem includes sub-carrier oscillators and, in addition, subsystem A contains a 90 x 10 and a 90 x 1-1/4 commutator used for temperature measurements.

4-7. Transmitting frequencies of the three systems are as follows:

Telemetry system A	237.8 mc
Telemetry system B	247.3 mc
Telemetry system C	257.3 mc.

4-8. The antenna system consists of a multiplexer, a filter, and a VHF omni-antenna. The antenna is located under a radome in the nose of the command module.

4-9. **RADAR TRANSPONDERS.** The two radar transponders operate in the C-band, receiving at 5690 mc and transmitting at 5765 mc. The transponders are interrogated by a 2-pulse code spaced at intervals of 3.5 microseconds between leading edges and followed by a 2.0-microsecond delay. The repetition rate will be consistent with range tracking requirements.



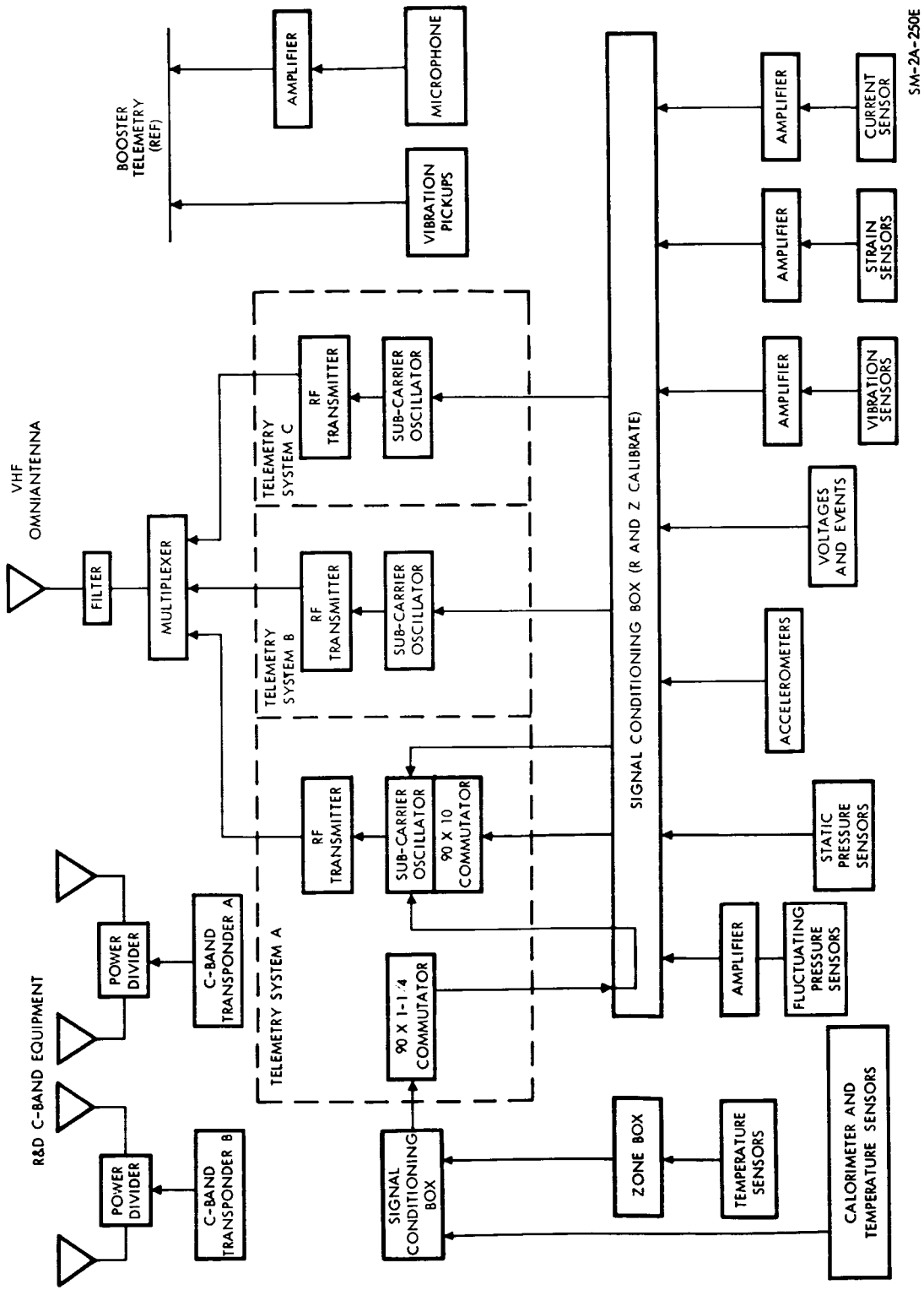


Figure 4-1. R&D Instrumentation Block Diagram

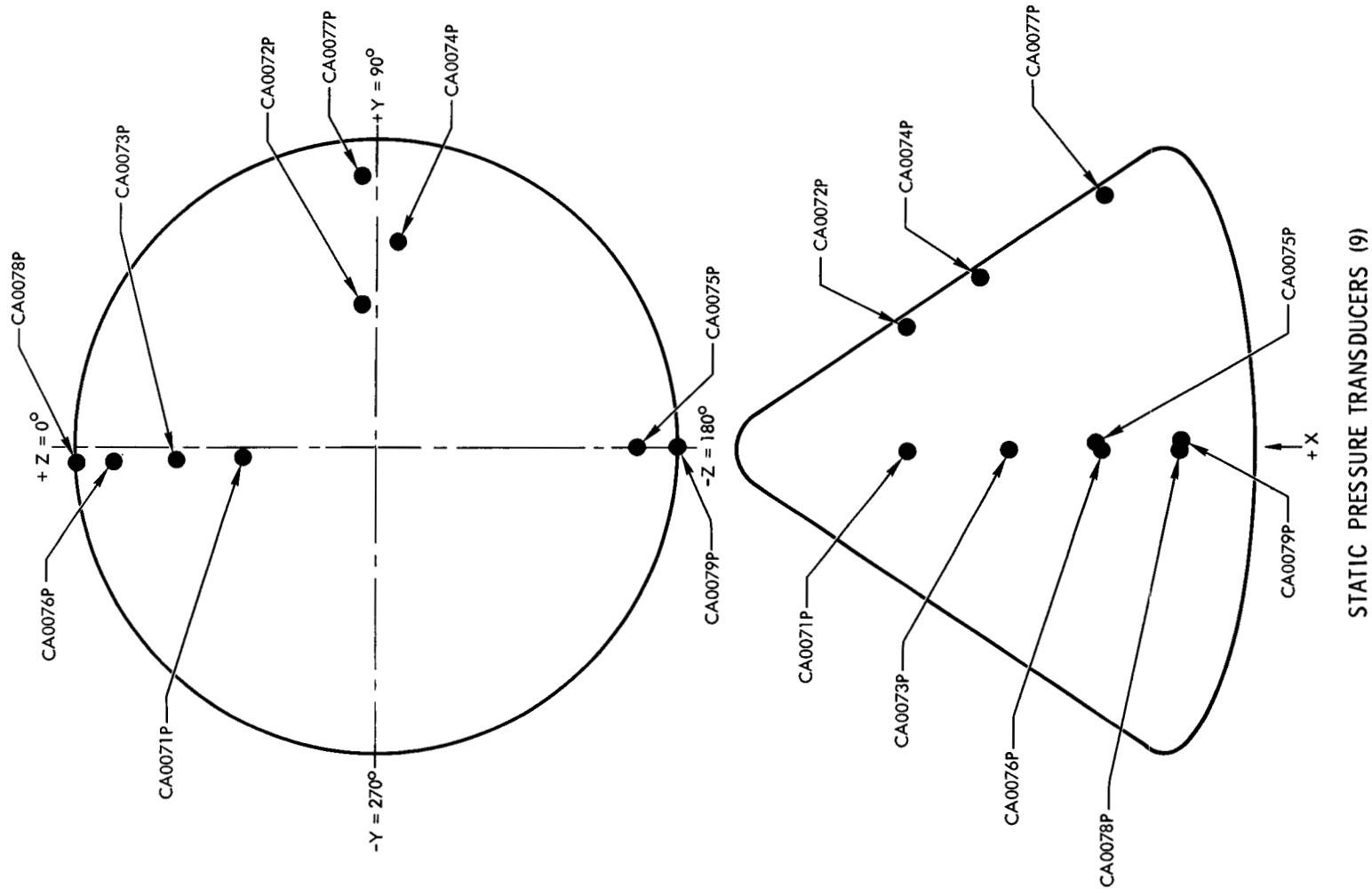
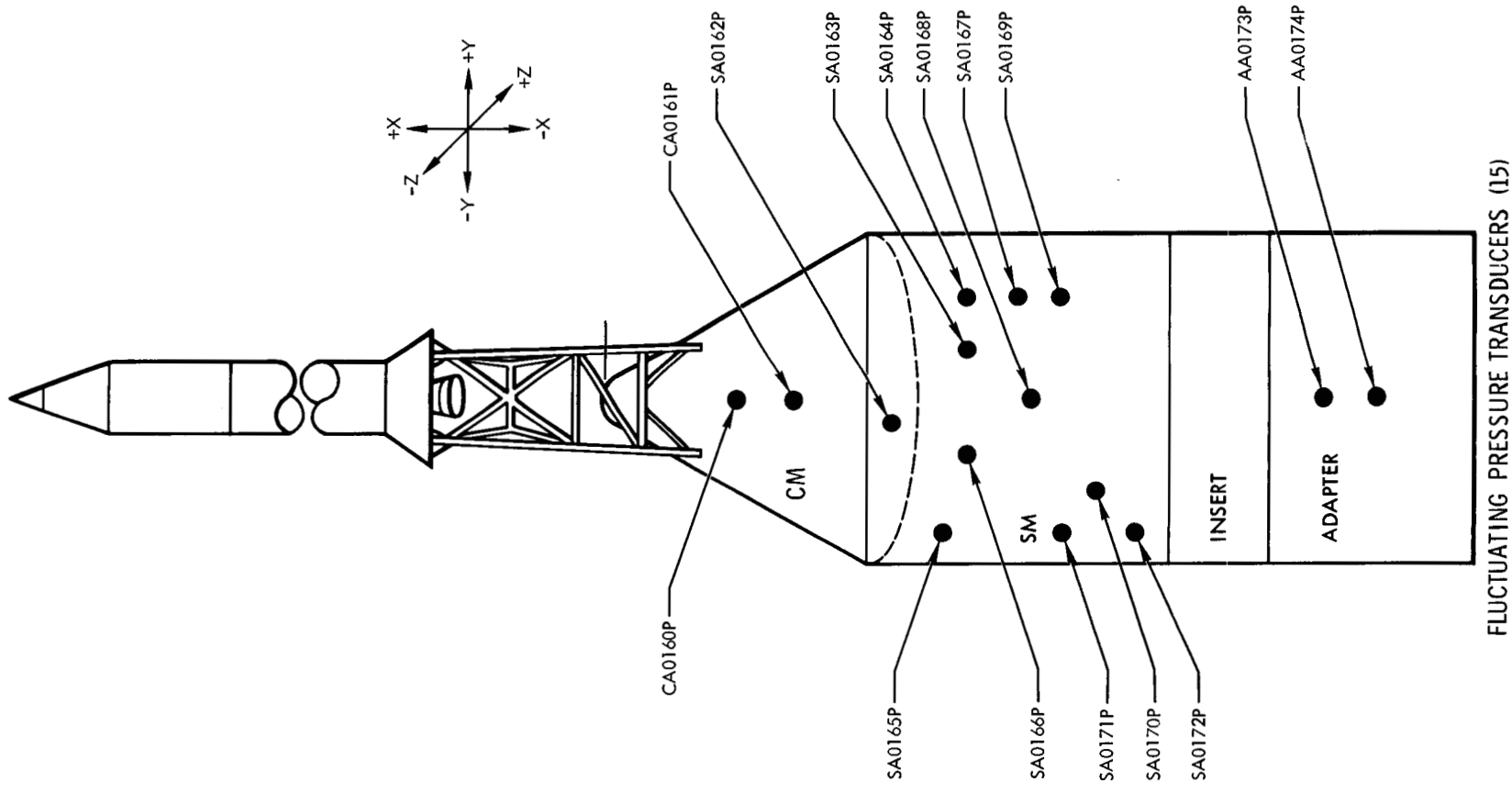


Figure 4-2. R&D Instrumentation Locations (Sheet 4 of 6)

4-10. The radar transponder antenna system includes two power dividers and four cavity helical, flush-mounted antennas. The antennas are mounted 90 degrees apart around the upper section of the service module.

#### 4-11. INSTRUMENTATION EQUIPMENT.

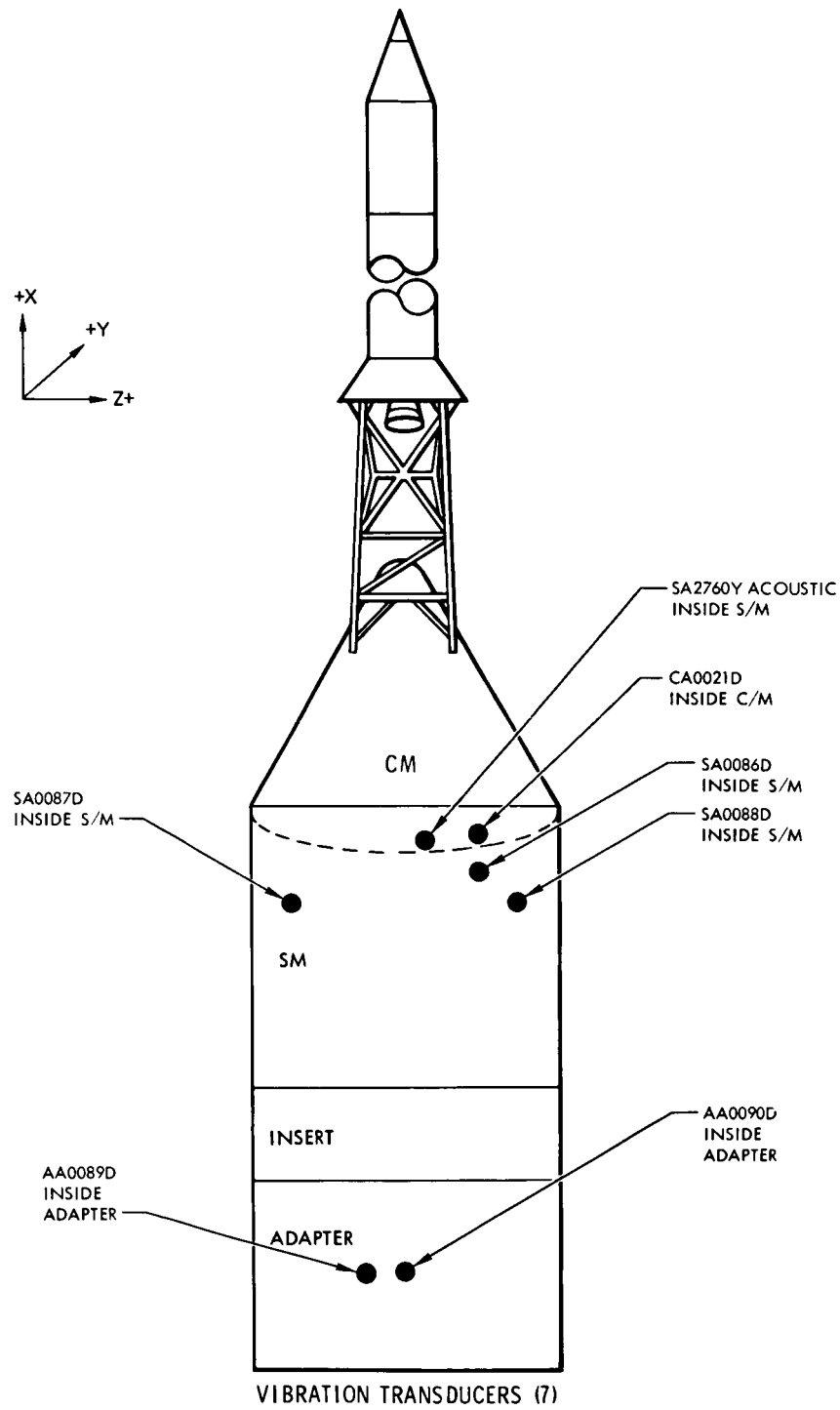
4-12. Instrumentation equipment includes the necessary transducers, sensors, and other devices to monitor physical and thermal effects of flight upon the spacecraft and to convert them into electrical signals suitable for telemetering. The devices are located in and on the spacecraft as shown in figure 4-2. Table 4-1 pertains to identification number, measurement description, channel, data range, priority, response, and device location. Subheadings in the channel columns indicate the following: LK (link) designates the telemetry (r-f carrier) package A, B, or C; SC No. (subcarrier number) designates telemetry channels 1 through 18, and Com Seg (commutator segment) designates the telemetry commutator segment assigned to the measurement for that vehicle. LV TM (launch vehicle telemetry), which appears in the channel LK and SC No. columns, designates a measurement to be telemetered by launch vehicle telemetry. The data range columns denote minimum and maximum values for a parameter in engineering units. The following letters in the PR (priority) column indicate how critical the measurements are: P (primary) denotes measurements that must be available at launch for mission success and to meet the flight objectives; S (secondary) denotes measurements that are highly desirable, but will not abort or delay the mission if inoperative, and M (multiple) designates a group of measurements of which only a specified percentage may be inoperative. The response column denotes the rate and unit required to provide satisfactory data resolution to time or waveform. Response for continuous data monitoring (telemetry or recorder) is specified in cycles per second (cps), and sampled-data monitoring (PCM or PACE) is specified in samples per second (S/S). The location column refers to the coordinates which denote the physical location within the spacecraft where measurement is taken.

4-13. SIGNAL CONDITIONER. The signal conditioner adapts all signals received from the measurement sensors to the telemetry signal input requirements and also directs the conditioned signal to the proper telemetry system. All R and Z calibration command circuitry is included in the signal conditioner unit. Z (zero) is equal to 15 percent of full-scale signal and R (range) is equal to 85 percent of full-scale signal.

4-14. VIBRATION SENSORS. Spacecraft radial vibrations are monitored by six vibration transducers located in the command module (1), service module (3), and adapter (2). The sensor circuitry includes an amplifier which raises the signal to a level compatible with the required signal input of the signal conditioner. Two additional sensors and an acoustical device (microphone) are located on the service module surface to determine structural response and aerodynamic and engine noises during boost and staging phases. These signals are routed through the booster instrument unit.

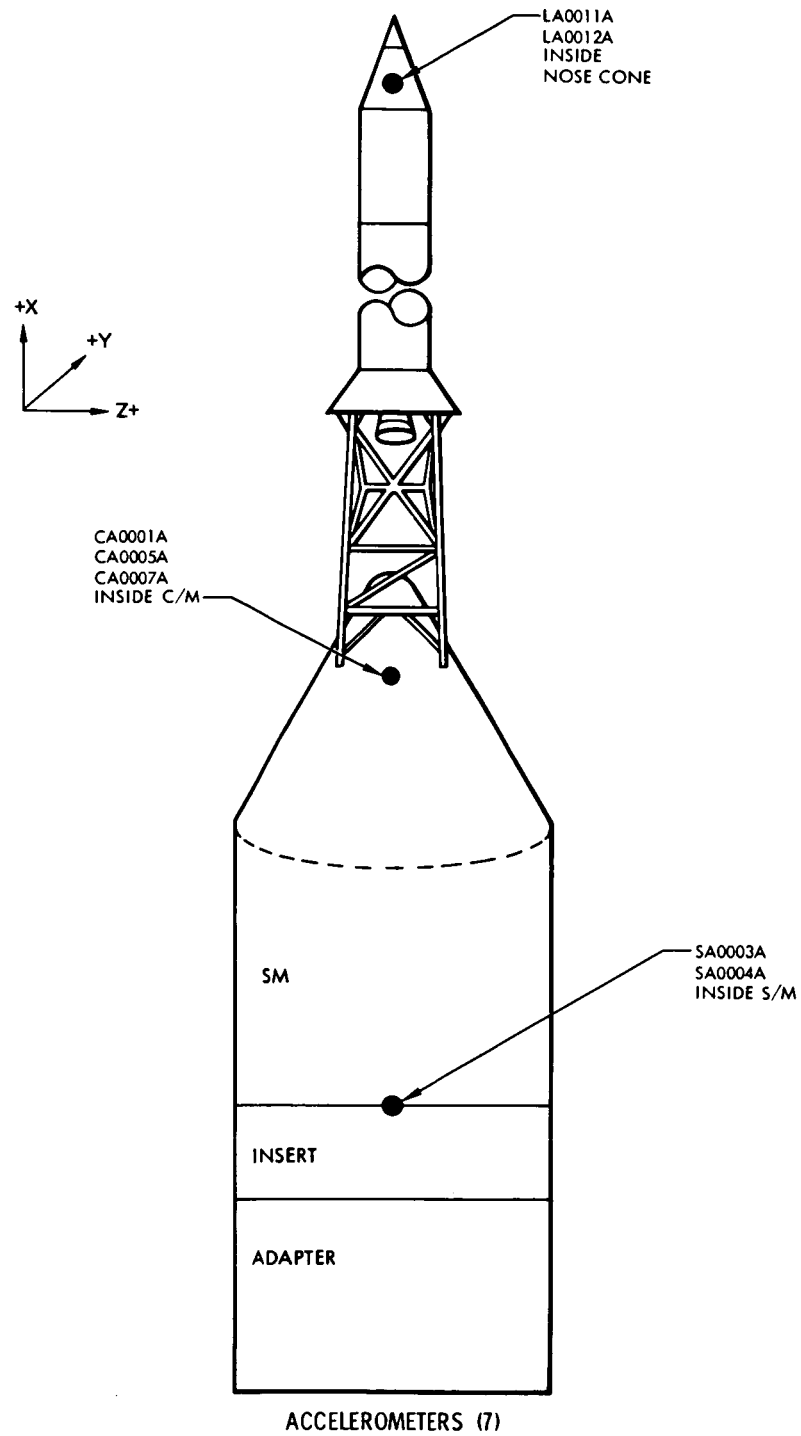
4-15. STRAIN SENSORS. Four strain gages are mounted on the adapter stringer frame and two on the service module ring frame to determine spacecraft structural integrity under dynamic loads. The circuitry includes an amplifier which raises the signal to a level compatible with the required signal input of the signal conditioner.

4-16. PRESSURE TRANSDUCERS. There are 26 pressure-sensing devices located in the spacecraft as follows: one transducer in the command module and one in the service module. The transducers monitor static internal pressures. Nine conical surface pressure sensors are mounted about the command module exterior, to determine the aerodynamic effects on the spacecraft to verify stability and loads. Fifteen fluctuating pressure transducers are located on the spacecraft, two in the command module and eleven in the service



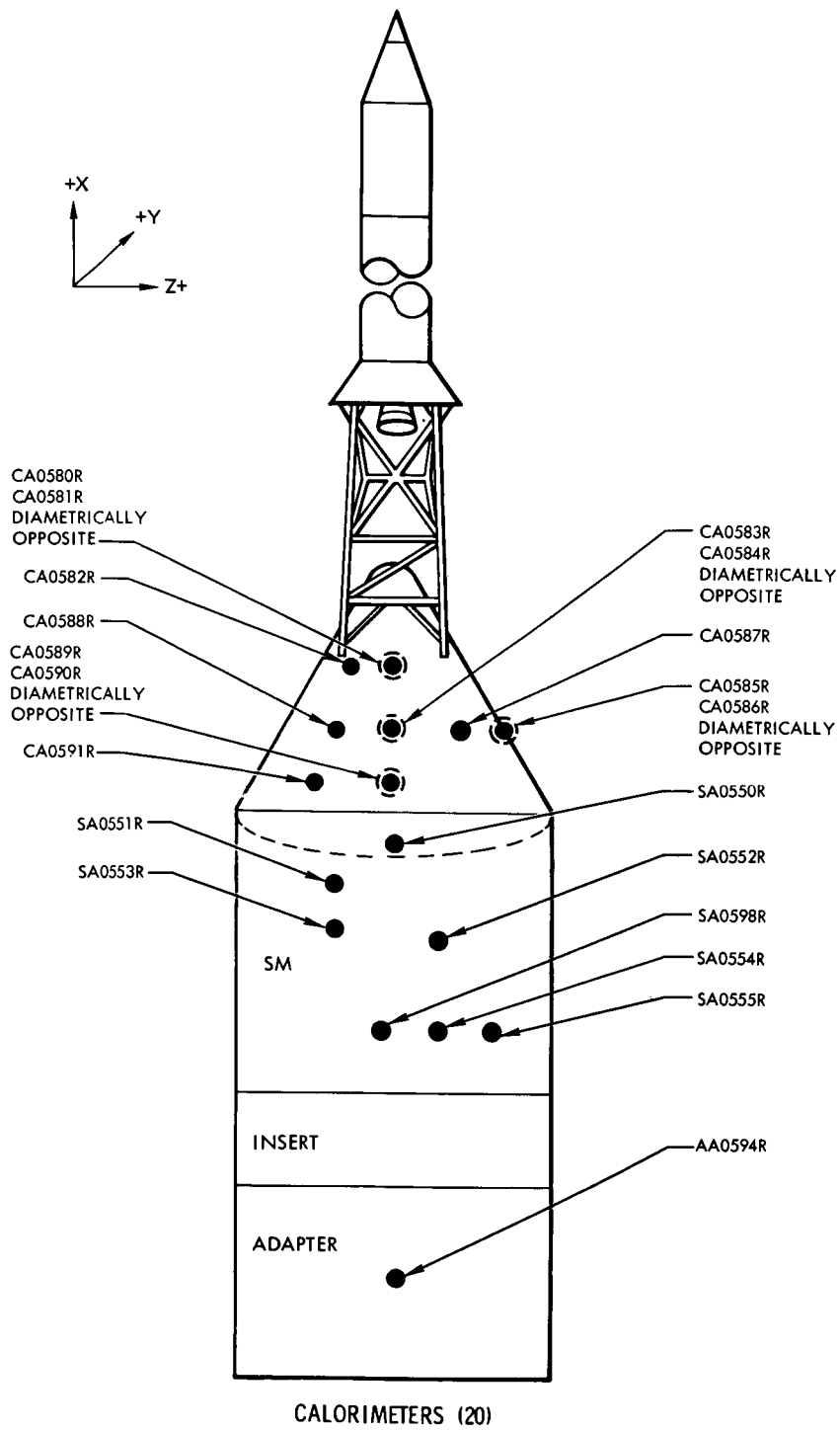
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Figure 4-2. R&D Instrumentation Locations (Sheet 1 of 6)



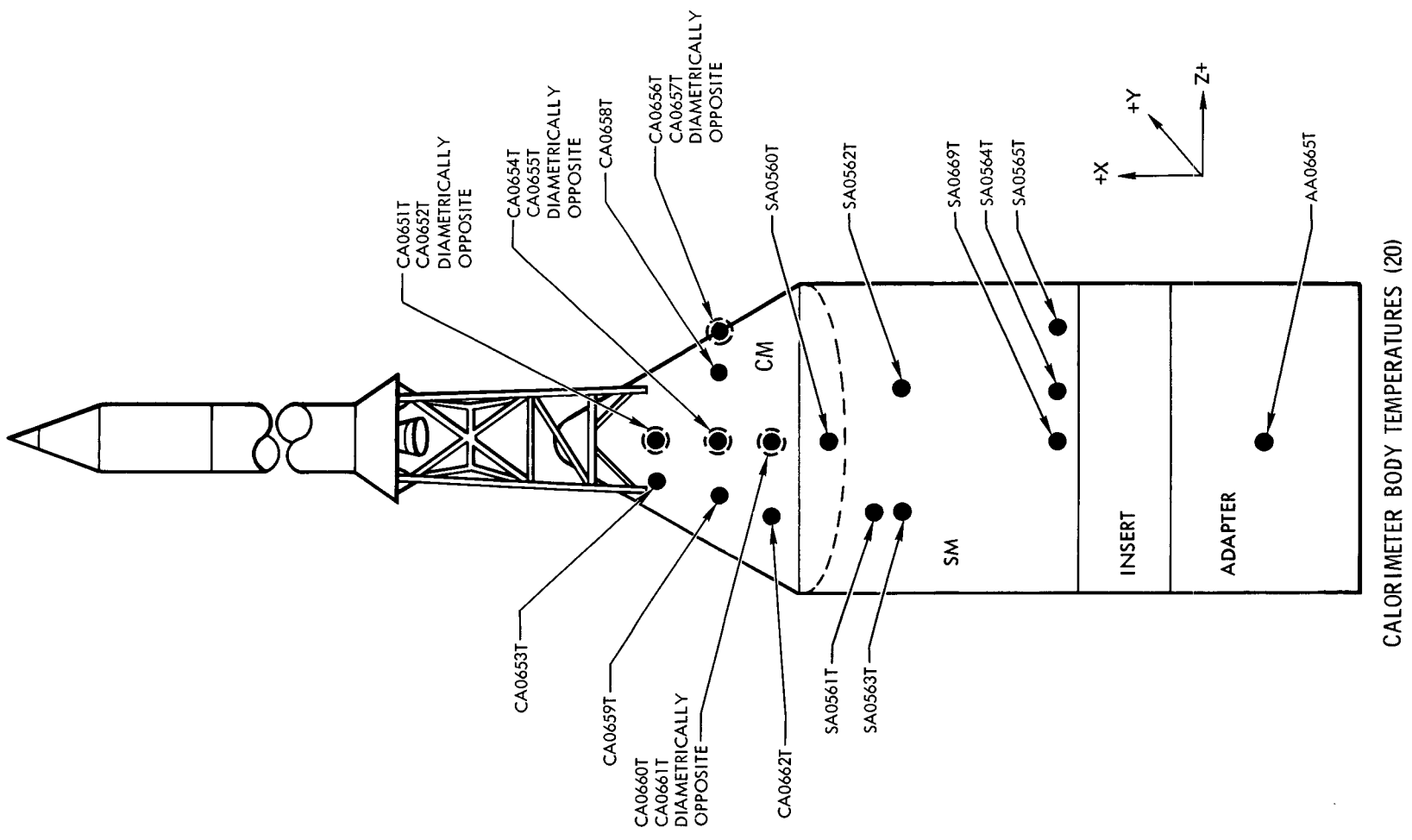
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Figure 4-2. R&D Instrumentation Locations (Sheet 2 of 6)

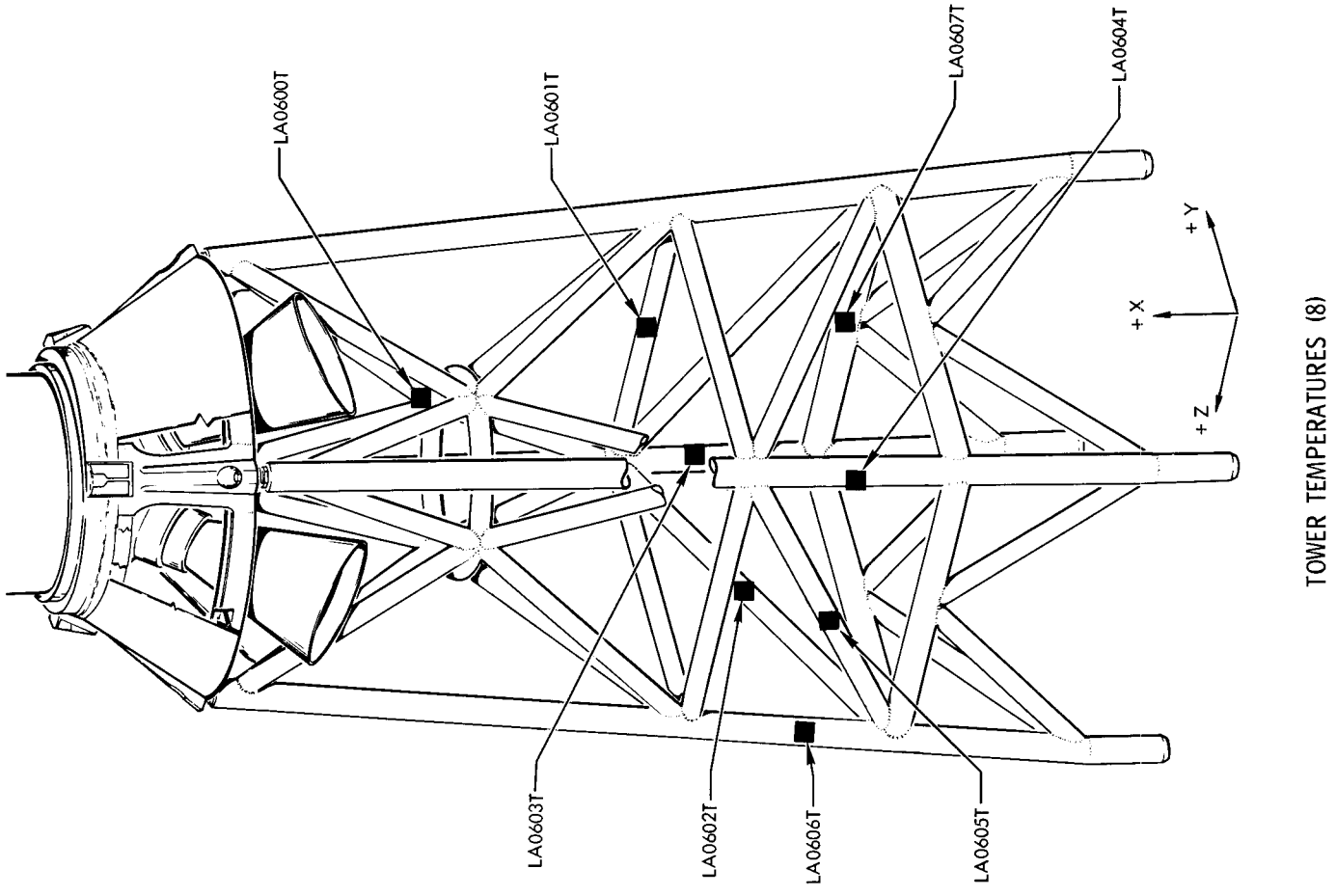


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Figure 4-2. R&D Instrumentation Locations (Sheet 3 of 6)

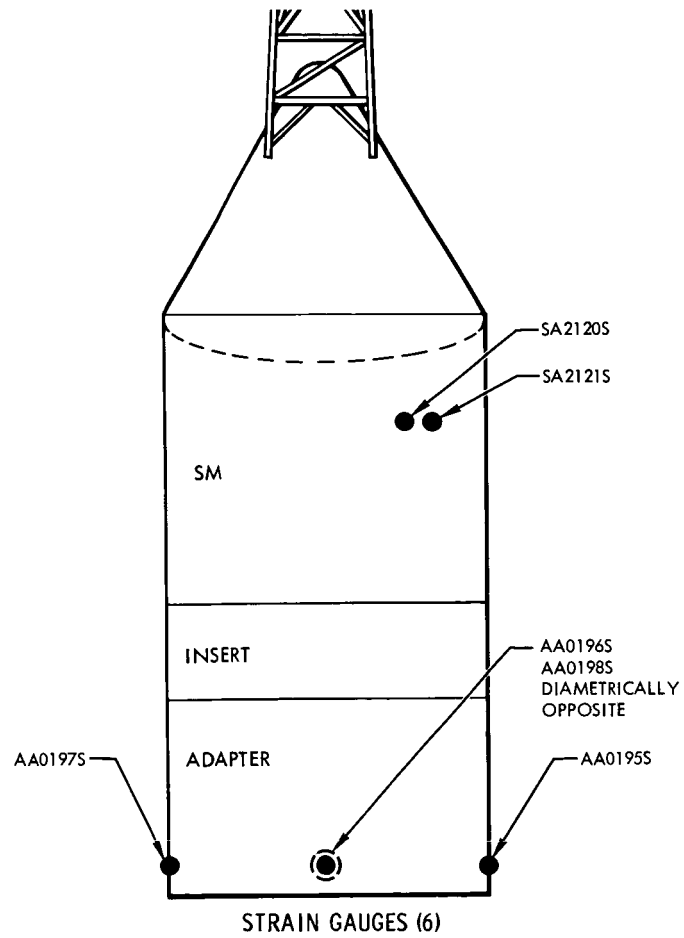


CALORIMETER BODY TEMPERATURES (20)



TOWER TEMPERATURES (8)

Figure 4-2. R&D Instrumentation Locations (Sheet 5 of 6)



SM-2A-403

Figure 4-2. R&D Instrumentation Locations (Sheet 6 of 6)



module. These measurements help to define boundary layer noise, confirm environmental predictions, and determine sonic-induced vibration response of the service module panels.

4-17. **ACCELEROMETERS.** Spacecraft acceleration measurements in all three planes are required to determine flight parameters and tower structure flight loads. Two accelerometers are mounted in the nose cone of the launch escape motor. One is assembled to measure acceleration along the Y-axis and the other is assembled to measure acceleration along the Z-axis. Three accelerometers are mounted in the command module to measure acceleration in all three axes and two are mounted in the service module to measure accelerations along the Y- and Z-axes.

4-18. **VOLTAGE DIVIDER NETWORKS.** Two voltage divider networks provide the means to monitor the main bus d-c voltage. The voltage levels of the two logic and two pyro buses can also be monitored by means of the voltage divider networks. This also provides events sequence information as to the time of arming the buses. Other events, which are sensed through relay closure, are jettison motor ignition commands and resultant tower separation, and tower-command module separation command from the booster guidance system. The purpose of monitoring the voltage levels is to determine the electrical capability of the electrical power system and the mission sequencer during flight loading conditions. The purpose of the events signals is to demonstrate tower jettison sequencing.

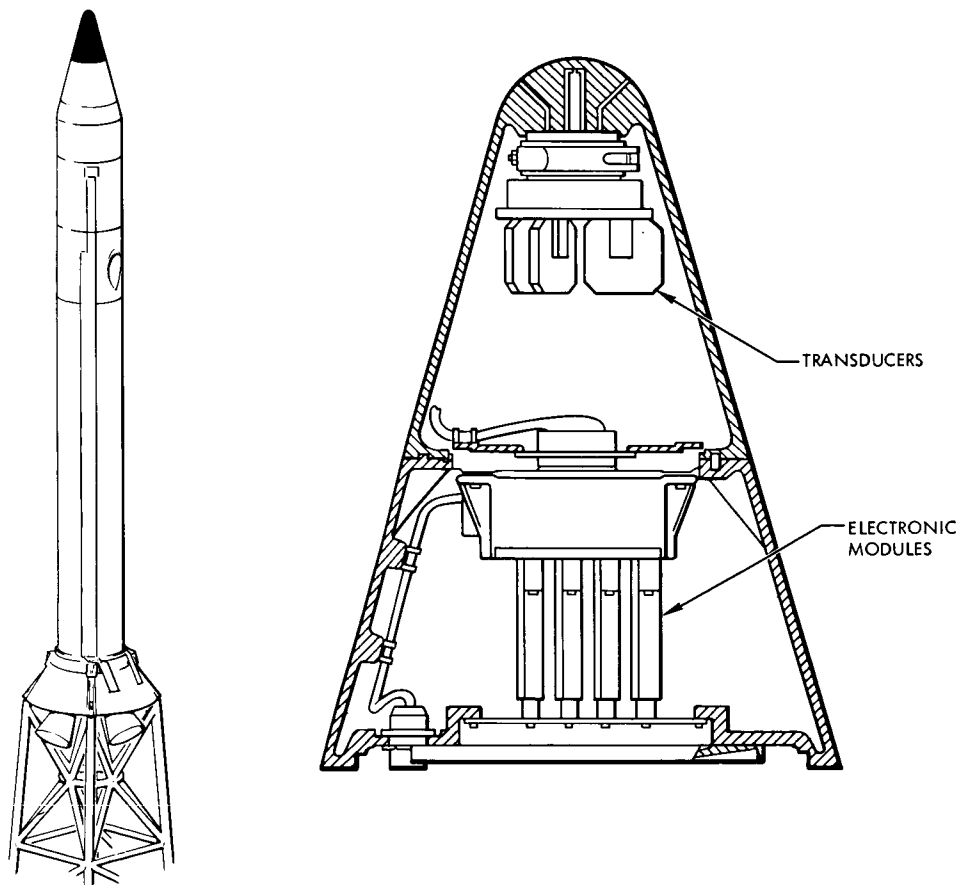
4-19. Sensors are also provided to monitor the sequencer control S-I lift-off signal from the booster instrument unit and to monitor transponder trigger signals.

4-20. **TEMPERATURE SENSORS.** A temperature sensor is mounted in the interior of both the command module and service module to determine interior temperatures during flight loading conditions. Eight resistance thermometers are mounted on the launch escape system tower structure members to determine aerodynamic heating. A thermocouple is mounted on each calorimeter to sense calorimeter body temperature for use in computing heat flow from the data provided by the 20 calorimeters. Telemetry transmitter and r-f amplifier environmental temperatures are monitored for abnormal heating by six sensors mounted in the telemetry packages.

4-21. **CALORIMETERS.** Twenty calorimeters are located in the spacecraft to measure heating rates of various areas in order to adequately define aerodynamic heating of the spacecraft. Twelve are located about the command module surface, seven on the service module surface, and one on the adapter surface.

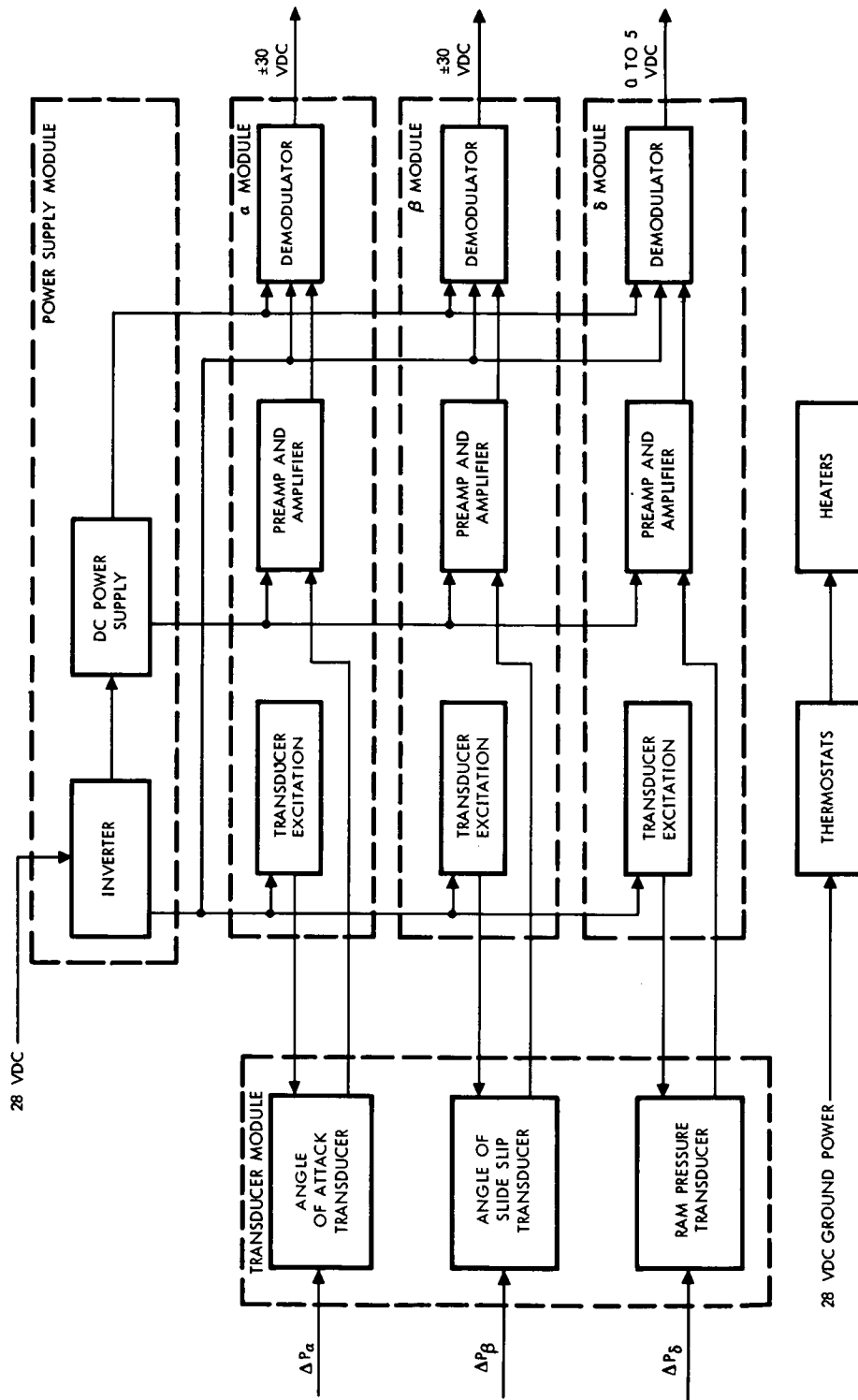
4-22. **CURRENT SENSOR.** A current sensor is located in the power control box. It monitors the total main power direct current flow during system operation to assist in determining the electrical capability and operation of the electrical power system.

4-23. **Q-BALL.** (See figures 4-3 and 4-4.) Three pressure transducers with associated electronics and wiring form the MSFC-furnished Q-ball system. Data acquired by the Q-ball includes angle of attack, angle of sideslip, and dynamic ram pressures. The transducers are located in the LES nose cone and sense airflow direction and pressure through ports in the nose cone surface. The input voltage is 28 volts dc. The transducers are capacitance-balanced with conversion of input power to 8 kilocycles. The output of the transducers is proportional to the three differential pressures measured. The transducer outputs are routed to the booster instrumentation unit control computer and conditioned for booster telemetry, but are not used functionally.



SM-2A-454

Figure 4-3. Q-Ball



SM-2A-169

Figure 4-4. Q-Ball Block Diagram

Table 4-1. Apollo CM/SM Measurement List

Meas. ID	Measurement Description	Channel			Data Range			PR	Response		Location
		L K	SC No.	Com Seg	Low	High	Unit		Rate	Unit	
Structures											
CA0001A	X-axis spacecraft accel high	C	8		-2	+10	G	P	0-30	cps	XC78, YC0, ZC21
SA0003A	Z-axis spacecraft accel S/M	C	7		-0.5	+0.5	G	P	0-20	cps	XA866, YA0, ZA73
SA0004A	Y-axis spacecraft accel S/M	A	6		-0.5	+0.5	G	P	0-20	cps	XA866, YA0, ZA73
CA0005A	Y-axis spacecraft accel	C	6		-0.5	+0.5	G	P	0-20	cps	XC78, YC0, ZC21
CA0007A	Z-axis spacecraft accel	B	6		-0.5	+0.5	G	P	0-20	cps	XC78, YC0, ZC21
LA0011A	Y-axis tower accel	B	7		-2	+2	G	P	0-30	cps	XL380, YL0, ZL6
LA0012A	Z-axis tower accel	B	8		-2	+2	G	P	0-30	cps	XL380, YL6, ZL0
CA0021D	C/M radial vibration 1	A	16		-50	+50	G	P	20-1000	C	XC14, YC40.4 ZC37.3
CA0071P	Conical surface pressure 1	A	E	66	+0	+15	psia	M	10	S/S	XC76, 357 DEG
CA0072P	Conical surface pressure 2	A	E	67	+0	+15	psia	M	10	S/S	XC76, 87 DEG
CA0073P	Conical surface pressure 3	A	E	68	+0	+15	psia	M	10	S/S	SC36, 357 DEG

Table 4-1. Apollo CM/SM Measurement List (Cont)

Meas. ID	Measurement Description	Channel			Data Range			PR	Response		Location
		L K	SC No.	Com Seg	Low	High	Unit		Rate	Unit	
Structures											
CA0074P	Conical surface pressure 4	A	E	69	+0	+15	psia	M	10	S/S	XC36, 93 DEG
CA0075P	Conical surface pressure 5	A	E	70	+0	+15	psia	M	10	S/S	XC29, 180 DEG
CA0076P	Conical surface pressure 6	A	E	71	+0	+15	psia	M	10	S/S	XC27, 357 DEG
CA0077P	Conical surface pressure 7	A	E	72	+0	+15	psia	M	10	S/S	XC27, 87 DEG
CA0078P	Conical surface pressure 8	A	E	73	+0	+15	psia	M	10	S/S	XC20, 357 DEG
CA0079P	Conical surface pressure 9	A	E	74	+0	+15	psia	M	10	S/S	XC20, 180 DEG
SA0086D	S/M radial vibration 2	C	18		-50	+50	G	P	20-1000	C	XA965.2, YA42.8, ZA58
SA0087D	S/M radial vibration 3	C	17		-50	+50	G	P	20-1000	C	XA953, YA53.9, ZA47.7
SA0088D	S/M radial vibration 4	B	17		-50	+50	G	P	20-1000	C	XA940.4, YA-68.3, ZA22.8
AA0089D	Adapter radial vibration 5	LV	TM		-50	+50	G	P	25-2000	C	XA777.7, YA0, ZA72
AA0090D	Adapter radial vibration 6	LV	TM		-50	+50	G	P	25-2000	C	XA777.7, YA-15.5, ZA71

CA0160P	Fluctuating pressure 1	B	18	+0	+15	psia	M	1000	cps	XC70, 357 DEG
CA0161P	Fluctuating pressure 2	B	15	+0	+15	psia	M	300	cps	XC40.4, 180 DEG
SA0162P	Fluctuating pressure 3	A	15	+0	+15	psia	M	300	cps	XA1000, 329.25 DEG
SA0163P	Fluctuating pressure 4	C	14	+0	+15	psia	M	300	cps	XA959, 24.1 DEG
SA0164P	Fluctuating pressure 5	A	14	+0	+15	psia	M	300	cps	XA959, 58.9 DEG
SA0165P	Fluctuating pressure 6	B	14	+0	+15	psia	M	300	cps	XA973, 277.5 DEG
SA0166P	Fluctuating pressure 7	C	13	+0	+15	psia	M	300	cps	XA959, 215.3 DEG
SA0167P	Fluctuating pressure 8	C	15	+0	+15	psia	M	300	cps	XA938, 147.9 DEG
SA0168P	Fluctuating pressure 9	B	12	+0	+15	psia	M	300	cps	XA932, 187.25 DEG
SA0169P	Fluctuating pressure 10	A	11	+0	+15	psia	M	300	cps	XA919, 58.9 DEG
SA0170P	Fluctuating pressure 11	A	12	+0	+15	psia	M	300	cps	XC893.5, 316.6 DEG
SA0171P	Fluctuating pressure 12	A	13	+0	+15	psia	M	300	cps	XA906, 277.25 DEG
SA0172P	Fluctuating pressure 13	C	11	+0	+15	psia	M	300	cps	XA881, 277.25 DEG
SA0173P	Fluctuating pressure 14	C	12	+0	+15	psia	M	300	cps	XA764, 183 DEG
SA0174P	Fluctuating pressure 15	B	11	+0	+15	psia	M	300	cps	XA737, 3 DEG
AA0195S	Strain 1 adapter	A	9	-1000	+1000	UI/IN	M	100	cps	XA736, YA76, ZA0
AA0196S	Strain 2 adapter	A	10	-1000	+1000	UI/IN	M	100	cps	XA736, YA0, ZA76
AA0197S	Strain 3 adapter	B	10	-1000	+1000	UI/IN	M	100	cps	XA736, YA76, ZA0
AA0198S	Strain 4 adapter	C	10	-1000	+1000	UI/IN	M	100	cps	XA736, YA0, ZA76

Table 4-1. Apollo CM/SM Measurement List (Cont)

Meas. ID	Measurement Description	Channel			Data Range			PR	Response		Location
		L K	SC No.	Com Seg	Low	High	Unit		Rate	Unit	
Structures											
SA0550R	Heat flux (calorimeter) 17	B	13	28	+0	+5	B/F/S	M	1.25	S/S	XS338, 183 DEG
SA0551R	Heat flux (calorimeter) 18	B	13	29	+0	+5	B/F/S	M	1.25	S/S	XS315, 187.2 DEG
SA0552R	Heat flux (calorimeter) 20	B	13	31	+0	+5	B/F/S	M	1.25	S/S	XS305, 177 DEG
SA0553R	Heat flux (calorimeter) 13	B	13	24	+0	+5	B/F/S	M	1.25	S/S	XS305, 187.2 DEG
SA0554R	Heat flux (calorimeter) 14	B	13	25	+0	+5	B/F/S	M	1.25	S/S	XS267, 160 DEG
SA0555R	Heat flux (calorimeter) 16	B	13	27	+0	+5	B/F/S	M	1.25	S/S	XS267, 145 DEG
SA0560T	Calorimeter body temp 17	B	13	48	+0	+300	Deg C	S	1.25	S/S	XS338, 183 DEG
SA0561T	Calorimeter body temp 18	B	13	49	+0	+300	Deg C	S	1.25	S/S	XS315, 187.2 DEG
SA0562T	Calorimeter body temp 20	B	13	51	+0	+300	Deg C	S	1.25	S/S	XS305, 177 DEG
SA0563T	Calorimeter body temp 13	B	13	44	+0	+300	Deg C	S	1.25	S/S	XS305, 187.2 DEG
SA0564T	Calorimeter body temp 14	B	13	45	+0	+300	Deg C	S	1.25	S/S	XS267, 160 DEG

SA0565T	Calorimeter body temp 16	B	13	47	+0	+300	Deg C	S	1.25	S/S	XS267, 145 DEG
CA0580R	Heat flux (calorimeter) 1	B	13	12	+0	+25	B/F/S	M	1.25	S/S	XC74, 3 DEG
CA0581R	Heat flux (calorimeter) 2	B	13	13	+0	+25	B/F/S	M	1.25	S/S	XC74, 180 DEG
CA0582R	Heat flux (calorimeter) 3	B	13	14	+0	+25	B/F/S	M	1.25	S/S	XC74, 319 DEG
CA0583R	Heat flux (calorimeter) 4	B	13	15	+0	+25	B/F/S	M	1.25	S/S	XC53, 180 DEG
CA0584R	Heat flux (calorimeter) 5	B	13	16	+0	+25	B/F/S	M	1.25	S/S	XC52, 3 DEG
CA0585R	Heat flux (calorimeter) 6	B	13	17	+0	+25	B/F/S	M	1.25	S/S	XC52, 80 DEG
CA0586R	Heat flux (calorimeter) 7	B	13	18	+0	+25	B/F/S	M	1.25	S/S	XC52, 85 DEG
CA0587R	Heat flux (calorimeter) 8	B	13	19	+0	+25	B/F/S	M	1.25	S/S	XC52, 95 DEG
CA0588R	Heat flux (calorimeter) 9	B	13	20	+0	+25	B/F/S	M	1.25	S/S	XC52, 319 DEG
CA0589R	Heat flux (calorimeter) 10	B	13	21	+0	+25	B/F/S	M	1.25	S/S	XC42.65, 3 DEG
CA0590R	Heat flux (calorimeter) 11	B	13	22	+0	+25	B/F/S	M	1.25	S/S	XC27, 180 DEG
CA0591R	Heat flux (calorimeter) 12	B	13	23	+0	+25	B/F/S	M	1.25	S/S	XC27, 319 DEG
AA0594R	Heat flux (calorimeter) 19	B	13	30	+0	+5	B/F/S	M	1.25	S/S	XA770, 183 DEG
SA0598R	Heat flux (calorimeter) 15	B	13	26	+0	+5	B/F/S	M	1.25	S/S	XA933, 183 DEG
LA0600T	Tower temperature 1	B	13	52	+0	+150	Deg C	M	1.25	S/S	XL90, YL12, ZL0
LA0601T	Tower temperature 2	B	13	53	+0	+150	Deg C	M	1.25	S/S	XL61, YL22, ZL0
LA0602T	Tower temperature 3	B	13	54	+0	+150	Deg C	M	1.25	S/S	XL47, YL0, ZL23



Table 4-1. Apollo CM/SM Measurement List (Cont)

Meas. ID	Measurement Description	Channel			Data Range			PR	Response		Location
		L K	SC No.	Com Seg	Low	High	Unit		Rate	Unit	
Structures											
LA0603T	Tower temperature 4	B	13	55	+0	+150	Deg C	M	1.25	S/S	XL47, YL24, ZL23
LA0604T	Tower temperature 5	B	13	56	+0	+150	Deg C	M	1.25	S/S	XL47, YL24, ZL23
LA0605T	Tower temperature 6	B	13	57	+0	+150	Deg C	M	1.25	S/S	XL47, YL24, ZL0
LA0606T	Tower temperature 7	B	13	58	+0	+150	Deg C	M	1.25	S/S	XL47, YL24, ZL23
LA0607T	Tower temperature 8	B	13	59	+0	+150	Deg C	M	1.25	S/S	XL36, YL24, ZL0
CA0610T	C/M interior temp	B	13	4	+0	+150	Deg C	S	1.25	S/S	C/M interior
CA0611P	C/M interior press	A	E	88	+0	+15	psia	S	10	S/S	C/M interior
SA0612T	S/M interior temp	B	13	5	+0	+150	Deg C	S	1.25	S/S	S/M interior
SA0613P	S/M interior press	A	E	87	+0	+15	psia	S	10	S/S	S/M interior
CA0651T	Calorimeter body temp 1	B	13	32	+0	+300	Deg C	S	1.25	S/S	XC74, 3 DEG
CA0652T	Calorimeter body temp 2	B	13	33	+0	+300	Deg C	S	1.25	S/S	XC74, 180 DEG
CA0653T	Calorimeter body temp 3	B	13	34	+0	+300	Deg C	S	1.25	S/S	XC74, 319.DEG
CA0654T	Calorimeter body temp 4	B	13	35	+0	+300	Deg C	S	1.25	S/S	XC53, 180 DEG
CA0655T	Calorimeter body temp 5	B	13	36	+0	+300	Deg C	S	1.25	S/S	XC52, 3 DEG

CA0656T	Calorimeter body temp 6	B	13	37	+0	+300	Deg C	S	1.25	S/S	XC52, 80 DEG
CA0657T	Calorimeter body temp 7	B	13	38	+0	+300	Deg C	S	1.25	S/S	XC52, 85 DEG
CA0658T	Calorimeter body temp 8	B	13	39	+0	+300	Deg C	S	1.25	S/S	XC52, 95 DEG
CA0659T	Calorimeter body temp 9	B	13	40	+0	+300	Deg C	S	1.25	S/S	XC52, 319 DEG
CA0660T	Calorimeter body temp 10	B	13	41	+0	+300	Deg C	S	1.25	S/S	XC42.65, 3 DEG
CA0661T	Calorimeter body temp 11	B	13	42	+0	+300	Deg C	S	1.25	S/S	XC27, 180 DEG
CA0662T	Calorimeter body temp 12	B	13	43	+0	+300	Deg C	S	1.25	S/S	XC27, 319 DEG
AA0665T	Calorimeter body temp 19	B	13	50	+0	+300	Deg C	S	1.25	S/S	XA770, 183 DEG
SA0669T	Calorimeter body temp 15	B	13	46	+0	+300	Deg C	S	1.25	S/S	XA933, 183 DEG
SA2120S	Strain 1 service module	C	16		-4000	+4000	UI/IN	M	250	cps	XA940.4, 62.25 DEG
SA2121S	Strain 2 service module	B	16		-4000	+4000	UI/IN	M	250	cps	XA940.4, 77.25 DEG
SA2760Y	Service module acoustic	LV	TM		+150	+170	DB	S	25-3000	C	XS339, 0 DEG
CC0001V	D-C voltage main bus A	A	E	24	+22	+32	VDC	P	10	S/S	Pwr control box
CC0002V	D-C voltage main bus B	A	E	25	+22	+32	VDC	P	10	S/S	Pwr control box

Table 4-1. Apollo CM/SM Measurement List (Cont)

Meas. ID	Measurement Description	Channel			Data Range			PR	Response		Location
		L K	SC No.	Com Seg	Low	High	Unit		Rate	Unit	
Electrical											
CC0003V	D-C voltage logic bus A	A	E	22	+0	+36	VDC	P	10	S/S	LES sequencer
CC0004V	D-C voltage logic bus B	A	E	23	+0	+36	VDC	P	10	S/S	LES sequencer
CC0005C	Total D-C current	A	E	26	+0	+50	AMPS	P	10	S/S	Pwr control box
Launch Escape											
BD0001X	S-I lift-off signal	A9	A10				Step	M	100	cps	Sig cond box
LD0033X	Twr jett and sep relay close A	A	E	29			Step	P	10	S/S	Twr LES sequencer
LD0034X	Twr jett and sep relay close B	A	E	29			Step	P	10	S/S	Twr LES sequencer
CD0039V	Twr jett sep signal A	A	E	37	+0	+36	VDC	P	10	S/S	LES sequencer
CD0040V	Twr jett sep signal B	A	E	38	+0	+36	VDC	P	10	S/S	LES sequencer
CD0185V	D-C voltage twr pyro bus A	A	E	28	+0	+36	VDC	P	10	S/S	LES sequencer
CD0186V	D-C voltage twr pyro bus B	A	E	35	+0	+36	VDC	P	10	S/S	LES sequencer
Communications and Instrumentation											
CT0002V	Transponder A trigger	A	E	57	+0	+5	VDC	S	10	S/S	Transponder A
CT0003V	Transponder B trigger	A	E	58	+0	+5	VDC	S	10	S/S	Transponder B
CT0007X	R&Z calibration monitor	A	E	59			STEP	P	10	S/S	Sig cond box
CT0201T	TM RF XMTR A temp	B	13	6	+0	+150	Deg C	S	1.25	S/S	TM RF XMTR A
CT0202T	TM RF AMP A temp	B	13	7	+0	+150	Deg C	S	1.25	S/S	TM RF AMP A

CT0203T	TM RF XMTR B temp	B	13	8	+0	+150	Deg C	S	1.25	S/S	TM RF XMTR B
CT0204T	TM RF AMP B temp	B	13	9	+0	+150	Deg C	S	1.25	S/S	TM RF AMP B
CT0205T	TM RF XMTR C temp	B	13	10	+0	+150	Deg C	S	1.25	S/S	TM RF XMTR C
CT0207T	TM RF AMP C temp	B	13	11	+0	+150	Deg C	S	1.25	S/S	TM RF AMP C
Environmental Control System											
CF0400T	R/D ECS CM interior temp	GSE			+0	+150	Deg F				CM interior
CF0401T	R/D ECS coldplate inlet temp	GSE			+0	+100	Deg F				Coldplate inlet
CF0402T	R/D ECS coldplate outlet temp	GSE			+0	+100	Deg F				Coldplate outlet
CF0403P	R/D ECS tank inlet press	GSE			+0	+50	PSID				Cool tank inlet
CF0404T	R/D ECS tank outlet temp	GSE			+0	+100	Deg F				Cool tank outlet
CF0405P	R/D ECS pump outlet press	GSE			+0	+50	PSID				Cool pump outlet

## SECTION V

## EQUIPMENT COOLING SYSTEM

5-1. PURPOSE.

5-2. The equipment cooling system is a specially designed water-glycol system which provides a coolant for five coldplates (three telemetry r-f packages and two C-band transponders). It also provides a continuous flow of air in the crew compartment for compartment cooling during ground operations and during the initial boost phase of the flight.

5-3. SYSTEM DESCRIPTION. (See figure 5-1.)

5-4. The complete cooling system for boilerplate 15 is located in the command module. The major components of the system are the supply tank, coolant pump, coldplates, heat exchanger with fan, accumulator, thermal control valve, and temperature and pressure transducers.

5-5. PRINCIPLES OF OPERATION. (See figure 5-2.)

5-6. OPERATION DURING MISSION. Coolant flow through the equipment cooling system is maintained by the pump assembly. The 250-pound capacity water-glycol tank operates in a standby condition to supply low-temperature coolant, when required, through the thermal control valve into the instrumentation cooling system. The thermal control valve is an automatic bypass valve which regulates the flow of coolant out of the tank into the closed cooling circuit. The thermal control valve is set to control the system temperature at  $40 \pm 5^\circ\text{F}$  for any inlet temperature encountered during the mission. The coolant continues from the thermal control valve to the coldplates of modulation packages A, B, and C and C-band transponders 1 and 2. The coldplates are connected in series. The heat exchanger receives the fluid from the coldplates and removes the ambient air heat load given off by the R&D instruments. Ambient air is circulated by the fan around the coiled tubing of the heat exchanger for crew compartment cooling.

5-7. Electrical power for equipment cooling system operation is supplied by the main batteries. Power from the batteries is routed through relay contacts to bus B in the power control box. Power from bus B is routed through relay contacts and fuses to a three-phase inverter and to two series-connected baroswitches. The three-phase inverter supplies power to operate the three-phase water-glycol pump motor. Power through the two baroswitches operate the heat exchanger control and the single-phase inverter which powers the fan motor. At a command module cabin pressure of 5 psi, the two baroswitches open, shutting down operation of the heat exchanger control, single-phase inverter, and fan motor. (See figure 5-3 for electrical schematic.)

5-8. OPERATION ON THE LAUNCH PAD. Ground support equipment furnishes water-glycol at  $20^\circ\text{F}$  to the spacecraft umbilical disconnect. The coolant flows into the tank continually, exciting the fluid in the tank, and flows out, returning to the GSE. The supply line and return line to the ground support equipment is disconnected by an umbilical disconnect on the service module. Pressure transducers are installed between the pump outlet and the thermal control valve, and between the glycol tank inlet and the GSE supply umbilical disconnect for checking system pressure. Temperature sensors are installed in the lines at the inlet side of the modulation package coldplates, at the inlet side of the heat exchanger, and at the outlet side of the glycol tank. This instrumentation is provided for ground monitoring only.

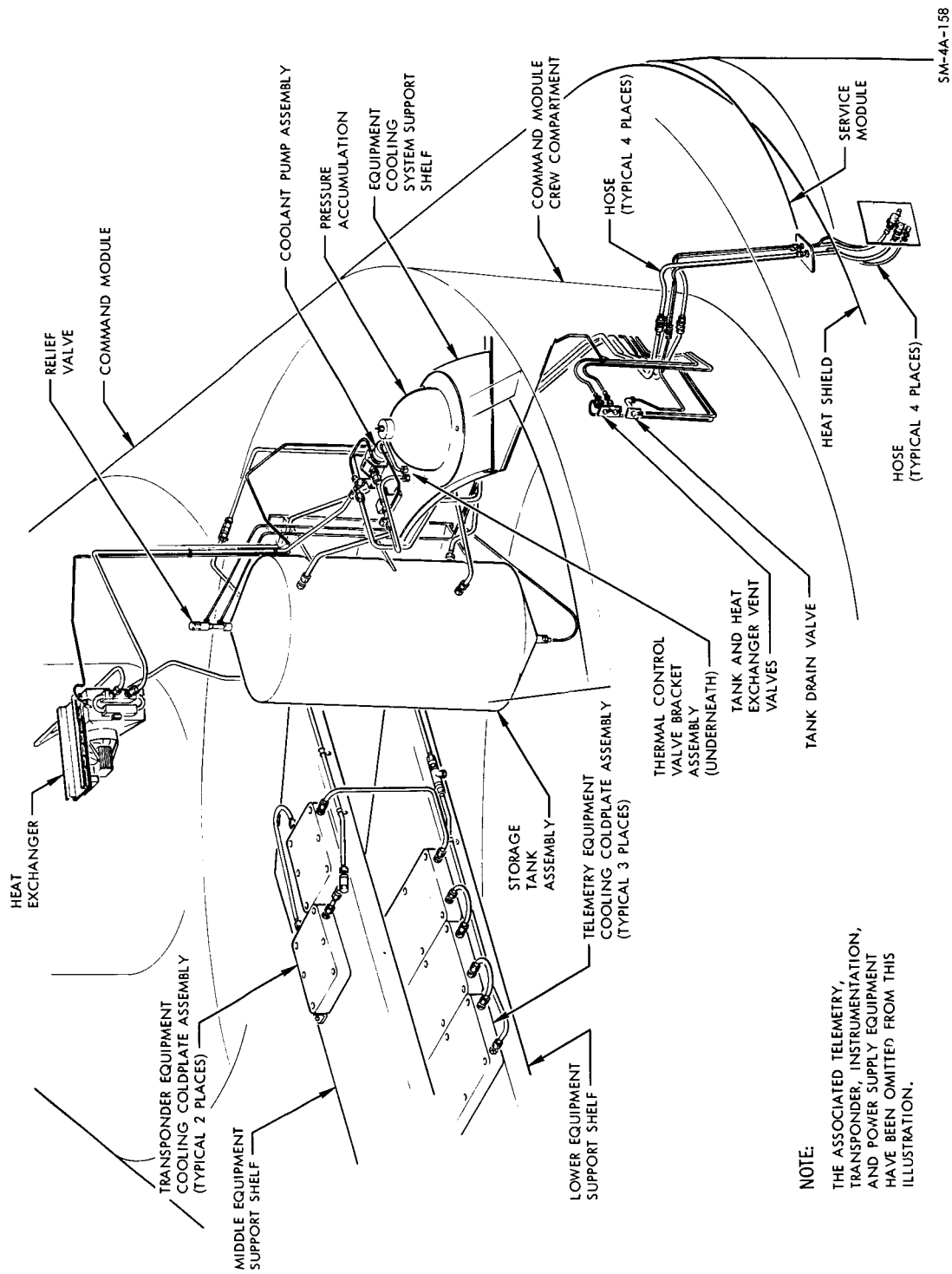
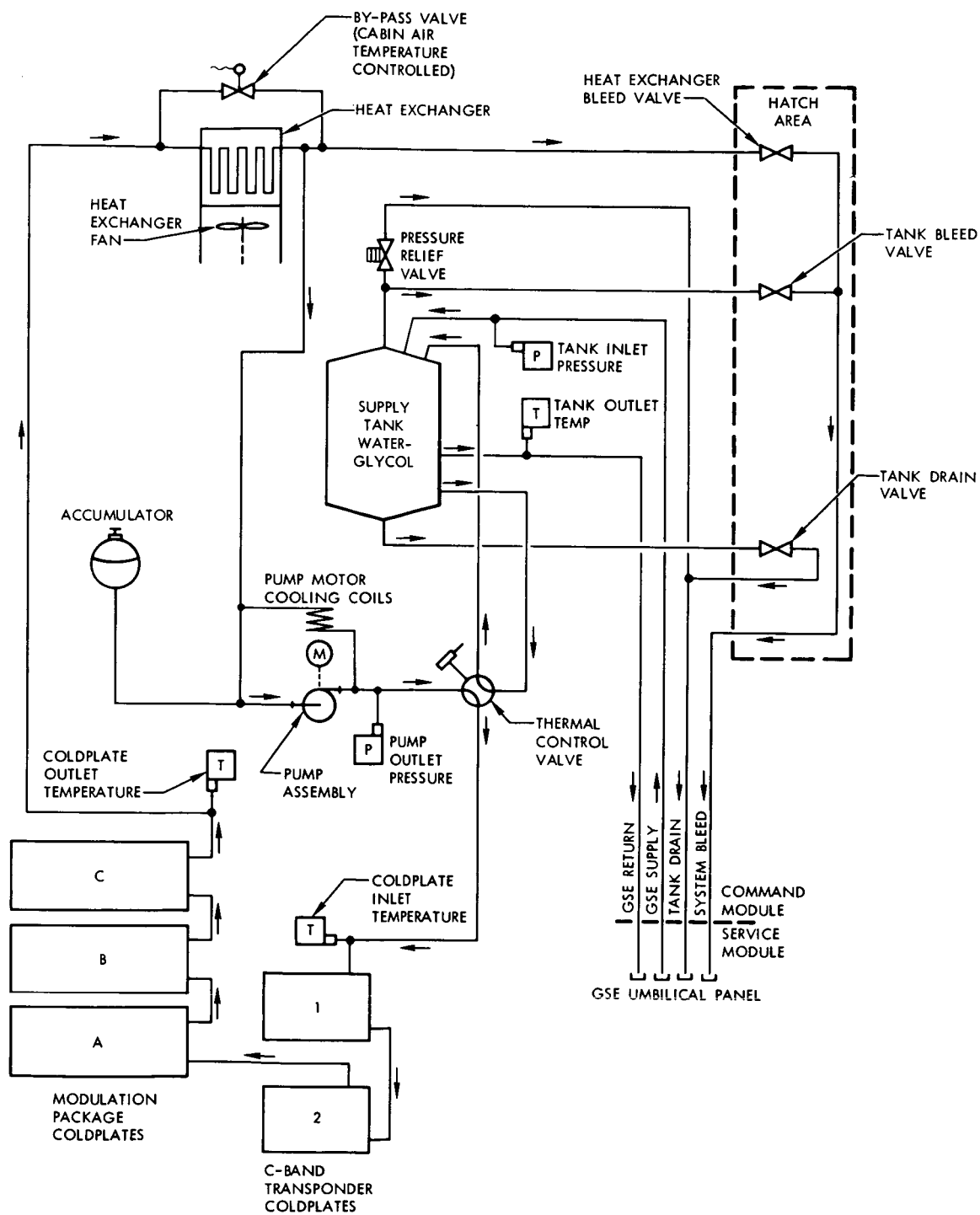


Figure 5-1. Equipment Cooling System



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Figure 5-2. Equipment Cooling System Functional Diagram

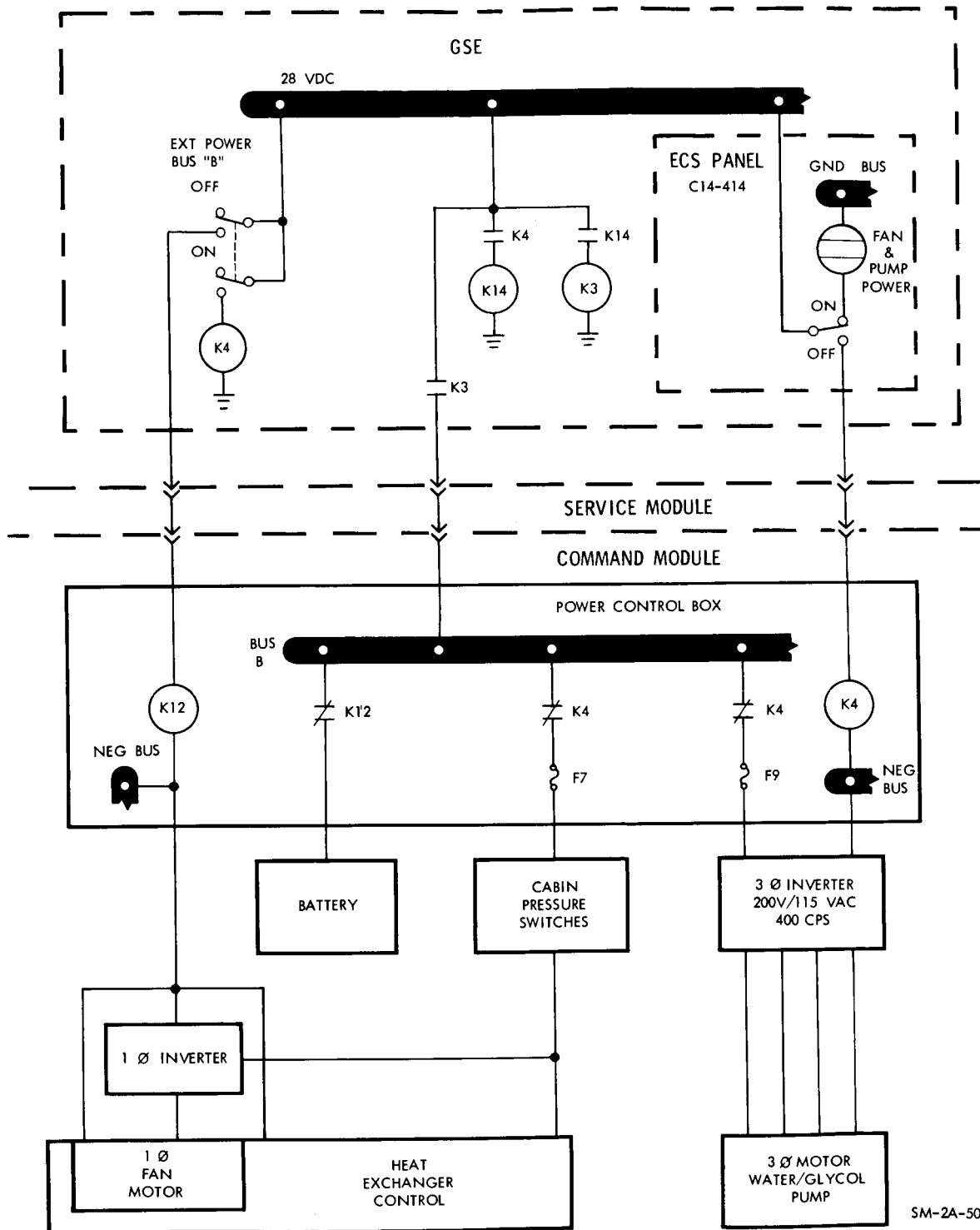


Figure 5-3. Equipment Cooling System Simplified Electrical Schematic  
(Sheet 1 of 2)





## SECTION VI

## ELECTRICAL POWER SYSTEM

6-1. PURPOSE.

6-2. The electrical power system supplies the power to the environmental control system and to all operational units of the communications and instrumentation system for switching and distribution of events that occur during a mission. It also provides the switching arrangement for event distribution to the signal conditioning unit and operating and monitoring power for launch escape system functions.

6-3. SYSTEM EQUIPMENT.

6-4. The electrical power system consists of six multi-cell, zinc-silver oxide batteries, a power control box, a junction box, and associated wire harnesses. These units are located on the equipment racks of the command module. Physical characteristics of the batteries are listed in table 6-1.

6-5. PRINCIPLES OF OPERATION. (See figure 6-1.)

6-6. The main batteries (NASA-furnished) provide the electrical power required to energize the instrumentation devices such as sensors, amplifiers, and telemetry equipment. The main batteries supply power to buses A and B of the power control box through normally closed contacts of the internal A and B power control relays. These relays can only be energized by GSE action. The power control relays remain open when power is being supplied by GSE to preserve the battery power prior to umbilical disconnect. Power transfer is accomplished manually. When power from GSE is discontinued, the power control relays close and system power is supplied by the on-board batteries.

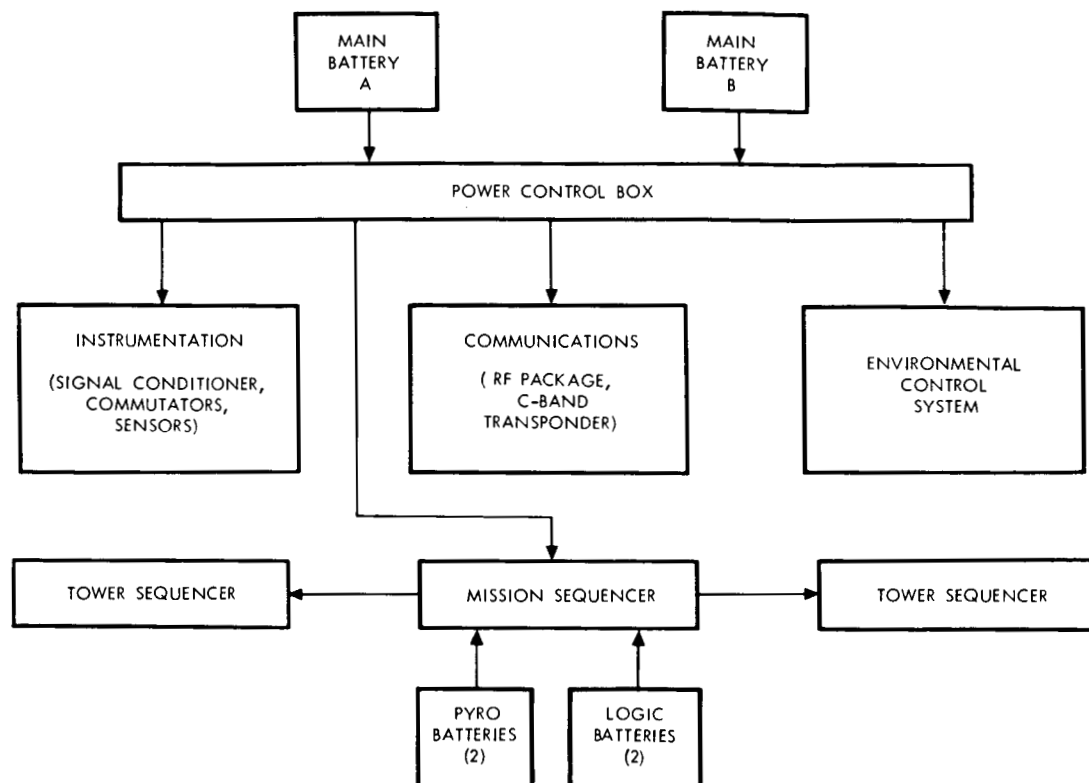
6-7. The pyro batteries provide the electrical power to energize the tower separation system components. Redundant circuits provide the high reliability required to assure a successful mission.

6-8. The logic batteries provide the electrical power to energize control circuitry of the mission and tower sequencers. Redundant circuits provide the high reliability required to assure a successful mission.

6-9. POWER CONSUMPTION.

6-10. Optimum power requirements by system are as follows:

Equipment cooling system	396 watts (mission)
Communications and instrumentation system	924 watts (mission)
Launch escape system	
Tower jettison motor squibs	18 watts (for 20 milliseconds)
Tower leg separation squibs	72 watts (for 20 milliseconds).



SM-2A-279A

Figure 6-1. Electrical Power System Block Diagram

Table 6-1. Battery Physical Characteristics

## Main batteries (instrumentation)

Height	9.50 inches
Width	6.36 inches
Length	9.05 inches
Weight	52 pounds
Nominal voltage	28 volts
Capacity	120-ampere hours
Electrolyte	Potassium hydroxide.

## Pyro and logic batteries

Height	3.52 inches
Width	4.69 inches
Length	7.00 inches
Weight	7.6 pounds
Nominal voltage	28 volts
Capacity	5-ampere hours
Electrolyte	Potassium hydroxide.

## SECTION VII

## DOCUMENTATION AND SUPPORTING EQUIPMENT

7-1. PURPOSE.

7-2. This section contains a list of documentation (table 7-1) and lists ground support equipment (table 7-2) for boilerplate 15.

7-3. DOCUMENTATION.

7-4. Documents containing supplementary information for boilerplate 15 are listed in table 7-1.

Table 7-1. Boilerplate 15 Supplementary Documents

Document No.	Title	Contents
SM1A-1	Apollo Support Manual Index	This manual contains a complete listing of Apollo support manuals.
SM2A-02	Apollo Spacecraft Familiarization Handbook	Description of spacecraft with all systems in overall terms.
SM2A-05-BP15	Apollo Spacecraft Transportation and Handling Procedures	Instructions for handling, packaging, packing, shipping, transporting, and storing the Apollo spacecraft for boilerplate 15 and its associated ground support equipment.
SM3A-201	Apollo Transportation and Handling Equipment Data Sheets	Maintenance procedures for transportation and handling equipment.
SM3A-202	Apollo Auxiliary Checkout and Servicing Equipment Maintenance Data Sheets	Maintenance instructions covering inspection, cleaning, lubrication, trouble analysis, and maintenance of equipment.
SM3A-204	Apollo Support Equipment, Maintenance Signal Conditioner Console, Model C14-135, Part No. G16-852500-101	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-205	Apollo Support Equipment, Maintenance Radar Transponder and Recovery Beacon Checkout Unit, Model C14-112, Part No. G16-852900	Physical and functional description and maintenance procedures consisting of functional tests and repair.

Table 7-1. Boilerplate 15 Supplementary Documents (Cont)

Document No.	Title	Contents
SM3A-208	Apollo Support Equipment, Maintenance Data Distribution and Recording Console, Model C14-420, Part No. G16-850500-101	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-213	Apollo Support Equipment, Maintenance Antenna Checkout Group, Model C14-032, Part No. G16-850400-101	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-221	Apollo Support Equipment, Maintenance Ground Cooling Cart, Model A14-011	Maintenance instructions covering inspection, cleaning, lubrication, trouble analysis, and maintenance of equipment.
SM3A-222	Apollo Support Equipment, Maintenance Launch Escape Tower Substitute Unit, Model A14-001, Part No. G16-820301-201	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-226	Apollo Support Equipment, Maintenance Pyrotechnics Bench Maintenance Equipment, Model C14-051, Part No. G16-852700-101	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-227	Apollo Support Equipment, Maintenance Launch Escape Sequencer Bench Maintenance Equipment, Model C14-029, Part No. G16-853400-201	Physical and functional description of test, trouble analysis, repair, servicing, packaging, and diagrams as related to boilerplate 15 configuration.
SM3A-228	Apollo Support Equipment, Maintenance Launch Vehicle Substitute Unit, Model A14-021, Part No. G16-821300	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-229	Apollo Support Equipment, Maintenance Optical Alignment Set, Model A14-028, Part No. G17-824010	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-235	Apollo Support Equipment, Maintenance Launch Control Group, Model C14-414, Part No. G16-853950-101	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-263	Apollo Support Equipment, Maintenance Water-Glycol Cooling Unit, Model S14-052, Part No. G16-848020	Maintenance instructions covering inspection, cleaning, lubrication, trouble analysis, and maintenance of equipment.

Table 7-1. Boilerplate 15 Supplementary Documents (Cont)

Document No.	Title	Contents
SM3A-272	Apollo Support Equipment, Maintenance MSFC Patch and Logic Distribution Sub Unit, Model A14-075, Part No. G16-853060	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM3A-273	Apollo Support Equipment, Maintenance Umbilical Junction Box, Model C14-192, Part No. G16-852850	Physical and functional description and maintenance procedures consisting of functional tests and repair.
SM4A-200-BP15	Apollo Spacecraft Maintenance BP15	Maintenance procedures consisting of testing, trouble analysis, repair, removal and installation, and calibration and adjustment as related to boilerplate 15 configuration.

7-5. SUPPORTING EQUIPMENT.

7-6. Supporting equipment for boilerplate 15 is the ground support equipment GSE listed in table 7-2. All listed GSE has been shop-released and approved by NASA.

Table 7-2. Ground Support Equipment

Model No.	Nomenclature	Part No.	Description
A14-001	Launch escape tower substitute unit	G16-820301-201	Provides electrical interface normally presented by LES to the command module.
A14-007	LES optical alignment set	G15-824040	Consists of two pieces; a telescope adapter and a target. The set provides means of aligning thrust vector of LE motor in relation to gross CG of abort configuration.
A14-009	Spacecraft adapter cover	G18-828001	A lightweight, synthetic, impregnated, fabric raincoat to protect adapter from sand, dust, rain, and salt spray.
A14-011	Ground cooling cart	ME-362-0002-0001	The cart will filter, cool, dehumidify, or heat ambient air to suitable level for introduction into interior of command module.
A14-020	S/M cover	G17-828003	A lightweight, synthetic, impregnated fabric fitted to conform to shape of S/M and used to protect S/M from sand, rain, and salt spray during handling, transportation and storage.

Table 7-2. Ground Support Equipment (Cont)

Model No.	Nomenclature	Part No.	Description
A14-021	Launch vehicle substitute unit C1	G16-821300	Provides interface for power to Q-ball heater and Q-ball electronics. It also provides access to monitor signals that may be returned from Q-ball electronics package.
A14-024	Fluid and electrical umbilical disconnect set	G16-828010-101	Interconnects spacecraft automatic and manually activated fluid servicing connections with appropriate fluid distribution systems.
A14-026	Cap and plug set	G14-828012-301	Consists of covers, caps, and plugs for all electrical, hydraulic, and mechanical disconnects; duct, pipe, and interface openings; and areas to be protected from shipping and handling damage.
A14-027	Adapter cap and plug set	G18-828002	Consists of covers, caps, and plugs for all electrical, hydraulic, and mechanical disconnects; duct, pipe, and interface openings; and areas to be protected from shipping and handling damage.
A14-076	Spacecraft GSE crossover distributor	G16-853056	Junction box for electrical cables.
C14-112	Radar transponder and recovery beacon checkout unit	G16-852900	Rack-mounted drawers. Rack is mounted on wheels and is approximately five feet in height. Drawers contain the following equipment: electronic counter, frequency meter, coax panel, signal generator, power control panel, blower, power meter drawer, oscilloscope, pulse generator, and cable drawer.
C14-135	Signal conditioner console	G16-852500-101	Consists of a signal conditioner drawer, relay drawer, and panel terminal board. The signal conditioner will amplify very small signals from pressure and temperature transducers.
C14-186	Electrical cable set	G16-850065	Consists of 50 cables, the lengths varying from 6 to 70 feet. The cables are used to transfer electrical power, monitor and control signals to and from spacecraft and ground support equipment.

Table 7-2. Ground Support Equipment (Cont)

Model No.	Nomenclature	Part No.	Description
C14-191	Terminal distributor	G16-851300	Cabinet, mounted to floor in test area and providing connection points between the spacecraft and various GSE units. Cabinet contains fuses, terminal blocks, and a power distribution panel with circuit breakers.
C14-414	Launch control group	G16-853950	Group consists of five system panels on drawer assemblies mounted in a five-bay equipment rack. The panels are: test conductor panel, electrical power system panel, instrumentation and communication systems panel, environmental control system panel, and launch escape system panel.
C14-420	Data distribution and recording console	G16-850500	Provides means of integrating data signals from spacecraft, Marshall Space Flight Control Panel (MSFC), and NAA ground support equipment panels. The system also provides monitoring and/or recording capability for all signals routed through console.
H14-016	LES weight and balance fixture	G15-810029	Fixture consists of two welded square tubing structures bolted together and supported by short jacks. The upper surface of frame has six level mounting pads for mounting load cells and a laterally and vertically adjustable cradle to support and position LES components.
H14-018	Escape tower support	G15-810026	Welded tubular structure equipped with four clamps to secure tower and four roller assemblies to rails of the H14-011 alignment stand and H14-052 positioning trailer.
H14-021	GSE handling cart	G14-810050	Can be used to transport lightweight miscellaneous components such as load cell kits and removable pieces from equipment, tools, etc.



Table 7-2. Ground Support Equipment (Cont)

Model No.	Nomenclature	Part No.	Description
H14-074	Spacecraft sling (with LES)	G15-818001-101	Consists of lifting eye, galvanized cables, spreader bar, rocket motor clamp assembly, and tie rods running from this clamp to attach points on skirt of LES. The sling is used to assemble launch escape system on command module, and for lifting both to a position on top of service module.
H14-109	S/M external access stand	G17-810070	Square platform having a circular cutout to clear the S/M, mounted on a scaffolding erected to reach the topmost area of the S/M. The platform is constructed of reinforced wood and the scaffolding of tubular steel. The platform is ringed with a protective rail of tubular steel.
H14-111	Access ladder, command module hatch	G16-810162	A stepladder that may be positioned on H14-109 workstand platform and allowed to rest against command module for entrance to hatch.
H14-127	Cable and fitting set, weight and balance, service module adapter	G17-810220	Consists of conical-shaped buttons with shank for installation into aft interface of spacecraft adapter and/or extension. The set is used during weight and balance operations.
H14-139	Forward compartment heat shield retention bolt guide	G16-810245	The bolt guide is tapered, and screws over retention bolts for thread protection and acts as a guide during heat shield installation.
H14-9076	General-purpose dolly	G16-810033-101	Consists of a welded rectangular steel frame, four lateral support brackets, and necessary tie-down brackets. Unit has lockable casters bolted to each corner of frame and removable tow bar assembly with swivel-type brackets in front and back of frame.
S14-052	Water-glycol cooling unit	G16-848020	A steel enclosure mounted on skids and containing all necessary controls and instrumentation for local operation.

SECTION VIII  
ELECTRICAL SCHEMATICS

8-1. PURPOSE.

8-2. This section consists of the electrical wiring schematic for boilerplate 15.

8-3. SCHEMATIC DIAGRAMS.

8-4. The combined systems schematic diagram for boilerplate 15 and GSE hanger checkout equipment is shown in figure 8-1.

RANGE	50°F TO 120°F	30°F TO 100°F	0°F TO 150°F	0°F TO 200°F	0°F TO 350°F
R 6	842	763	778	806	806
R 8	12500	2500	3360	3600	8000
R 9	11200	15335	1350	16000	14000
R 12	30000	40000	40000	40000	40000
R 13	3600	4000	4000	4000	4000
R 14	279.5	111.6	300	43.7	558.5
R 15	2000	1000	1000	2000	2000

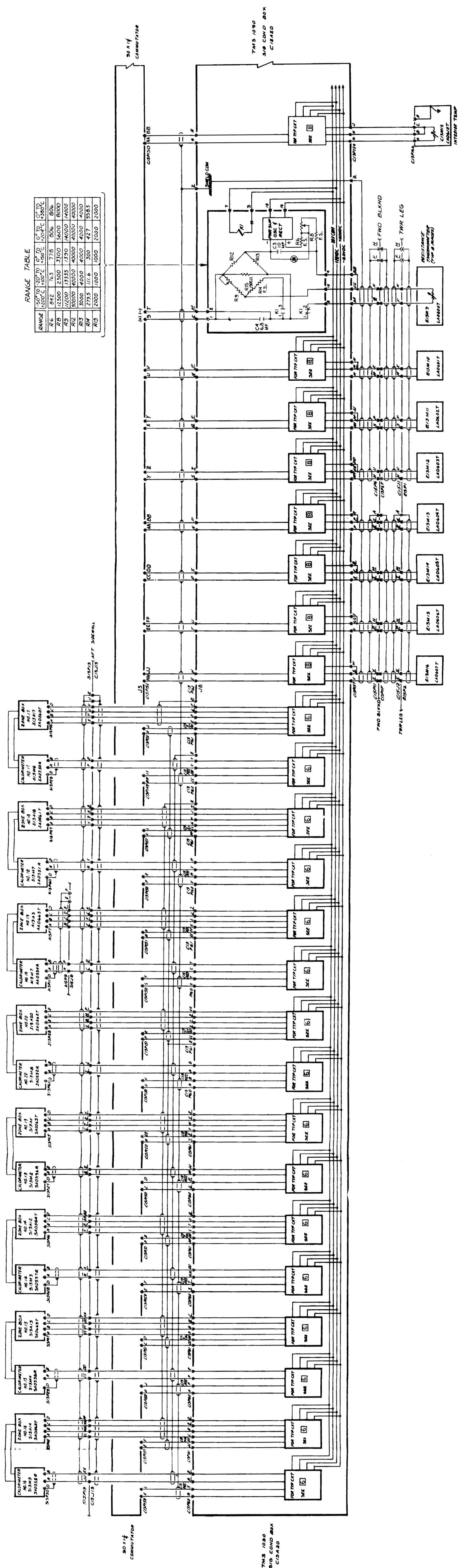
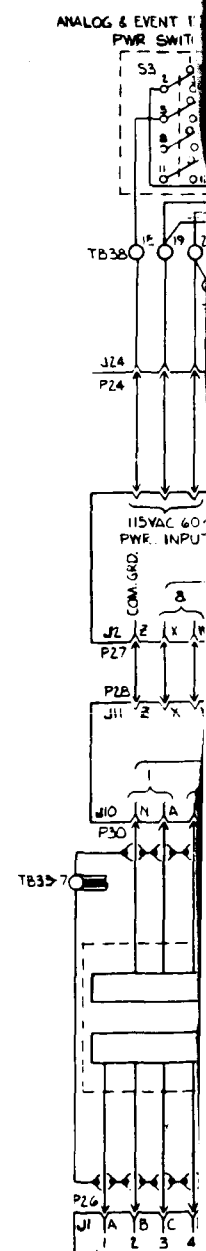


Figure 8-1. Boilerplate 15 and GSE Hangar Checkout Equipment Combined Systems Schematic (Sheet 1 of 5)

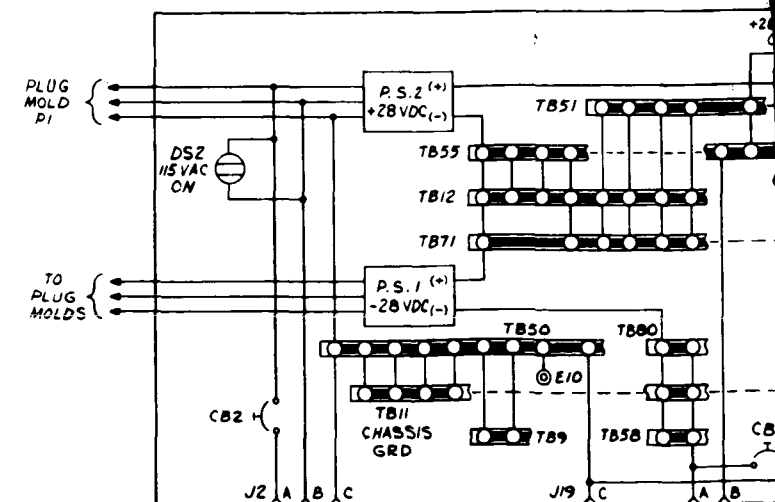
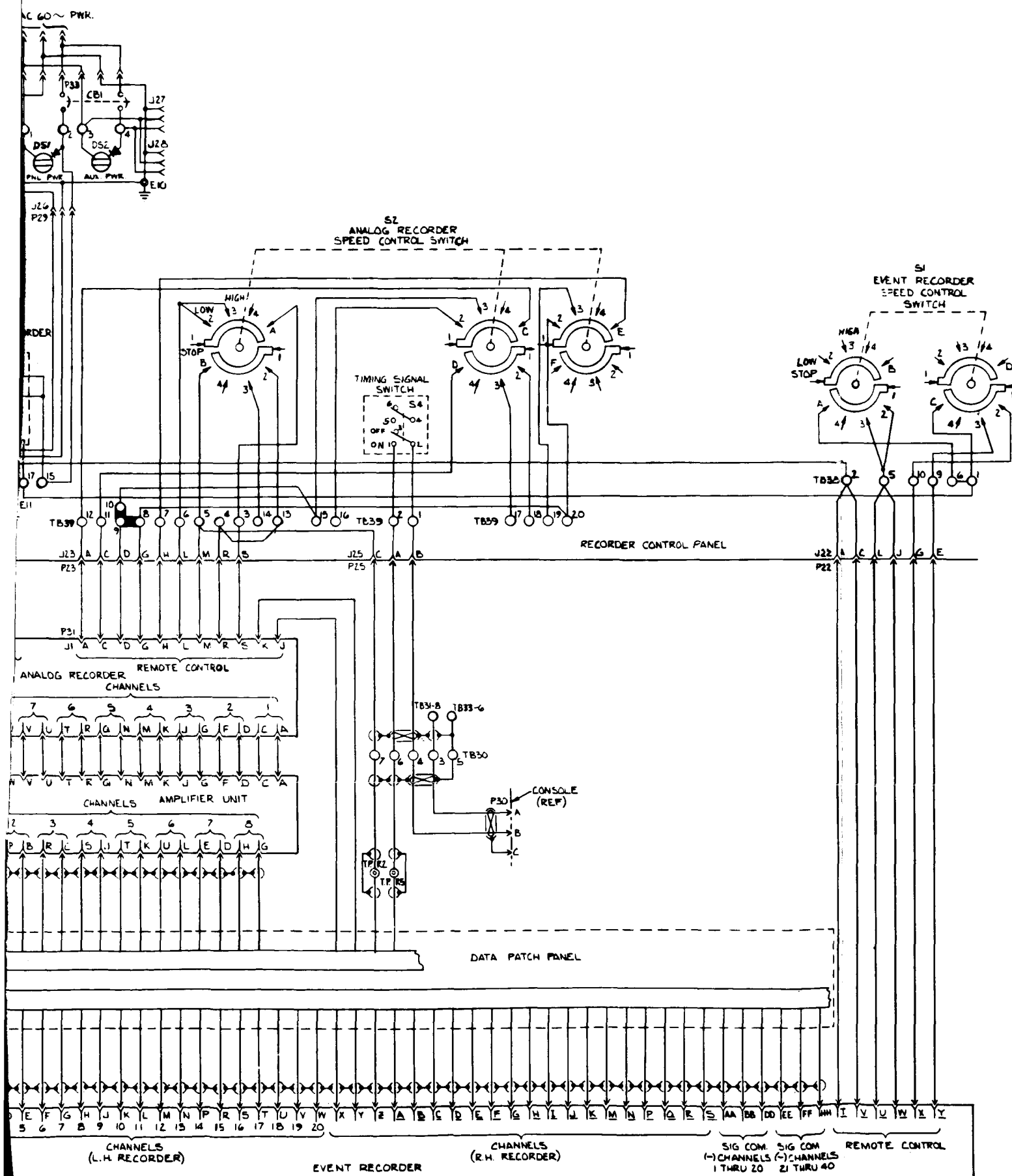
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CONSOLE  
PWR PANEL  
7B37

[illegible]

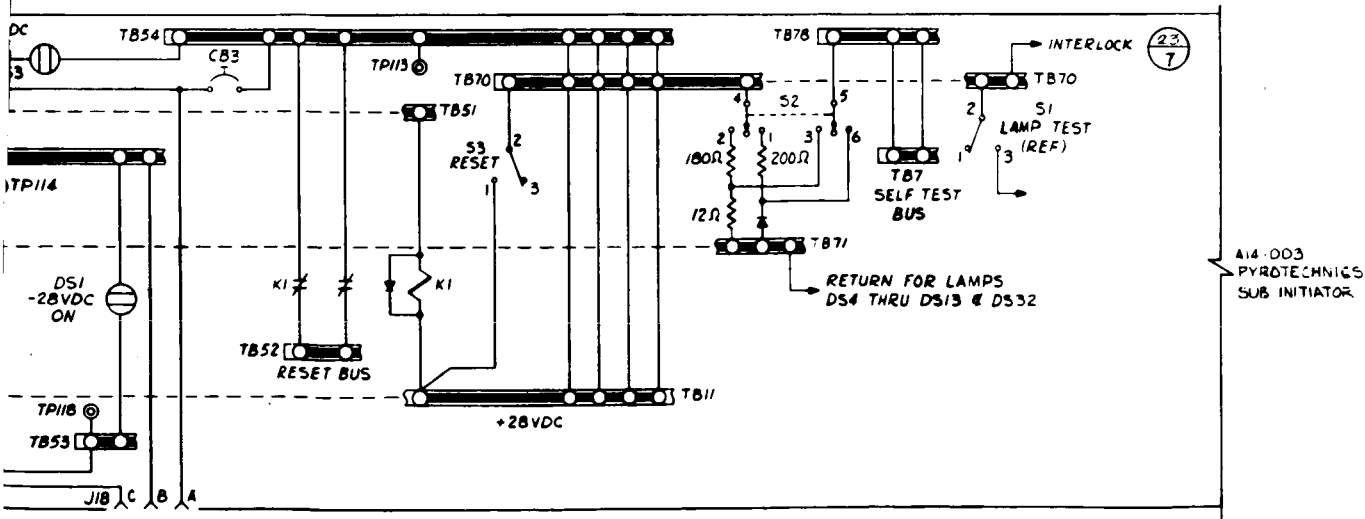
4

3



2

2



RELATED DRAWINGS

UNIT	SCHEMATIC	WIRING DIAGRAM
A14-003 (PYRO)	GSE G16-982108B	G16-820589A G16-820550 G16-820551 G16-820555

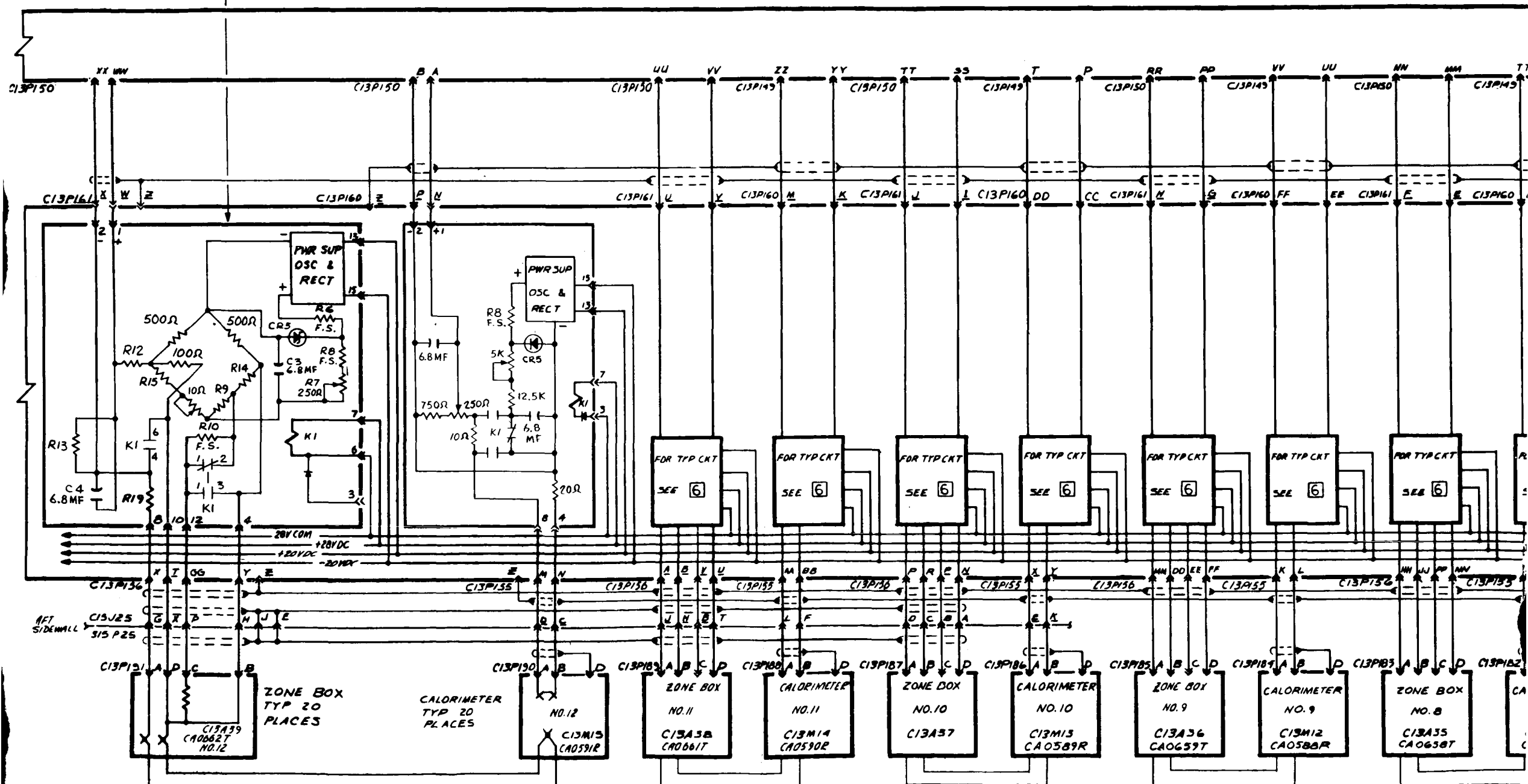
BOILERPLATE

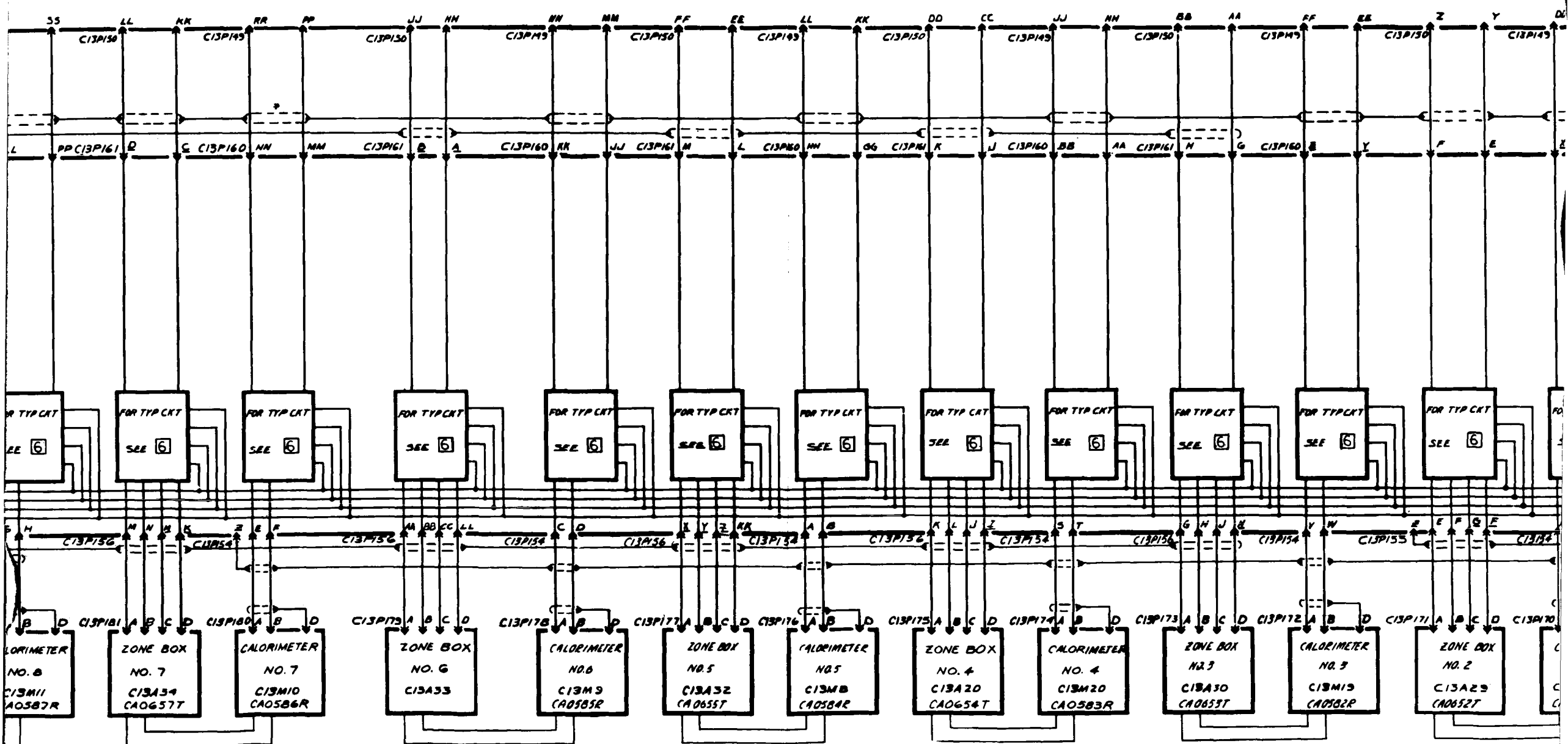
SIGNAL COND. BOX \_\_\_\_\_ SX 540,007 (NASA)

3

RANGE TABLE

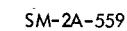
RANGE	C-A 0-300°	C-A 0-375°	C-A 0-550°	C-A 0-800°	C-A 0-1100°	C-A 0-1200°	C-C 0-250°
R6	555	540	555	545	555	655	668
R8	2150	2120	2120	2120	2090	2150	2430
R9	300	300	300	300			
R10	85.5	93.8	100.9	128.8	159.4	169.3	78.7
R12	16.66	62.66	95.86	167.2	298.7	335.0	147.5
R13	1000	500	400	250	250	250	500
R14	400	400	400	400	400	400	NOT USED
R15	335	335	335	335	335	335	240
R19	124	124	335	365	500	500.5	133





5

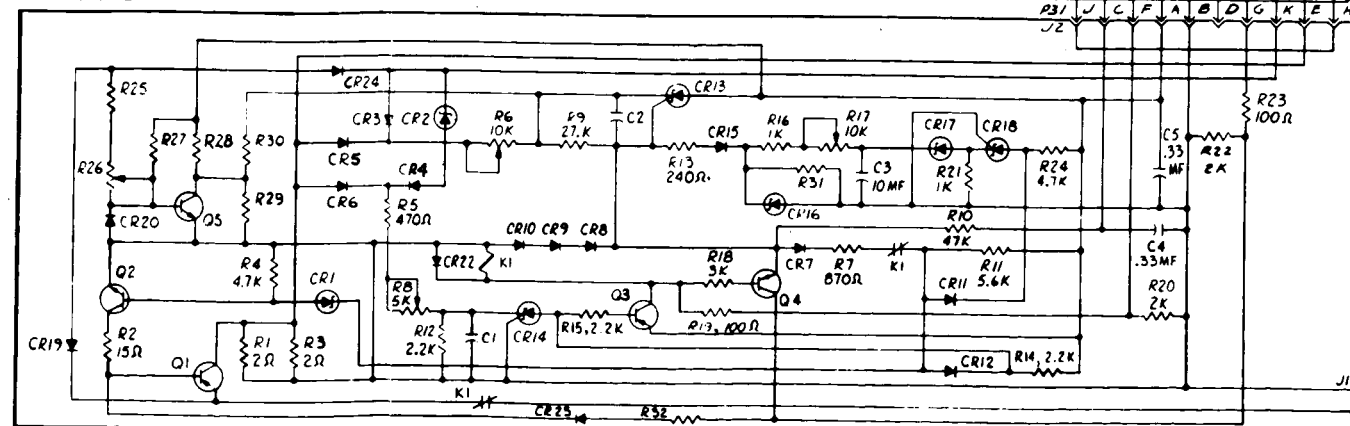




6

ELECTRONIC  
HOT BRIDGE  
WIRE SUB UNITS

SUB (TYP SCHEMATIC)  
PITCH CONTROL MOTOR  
SYS B

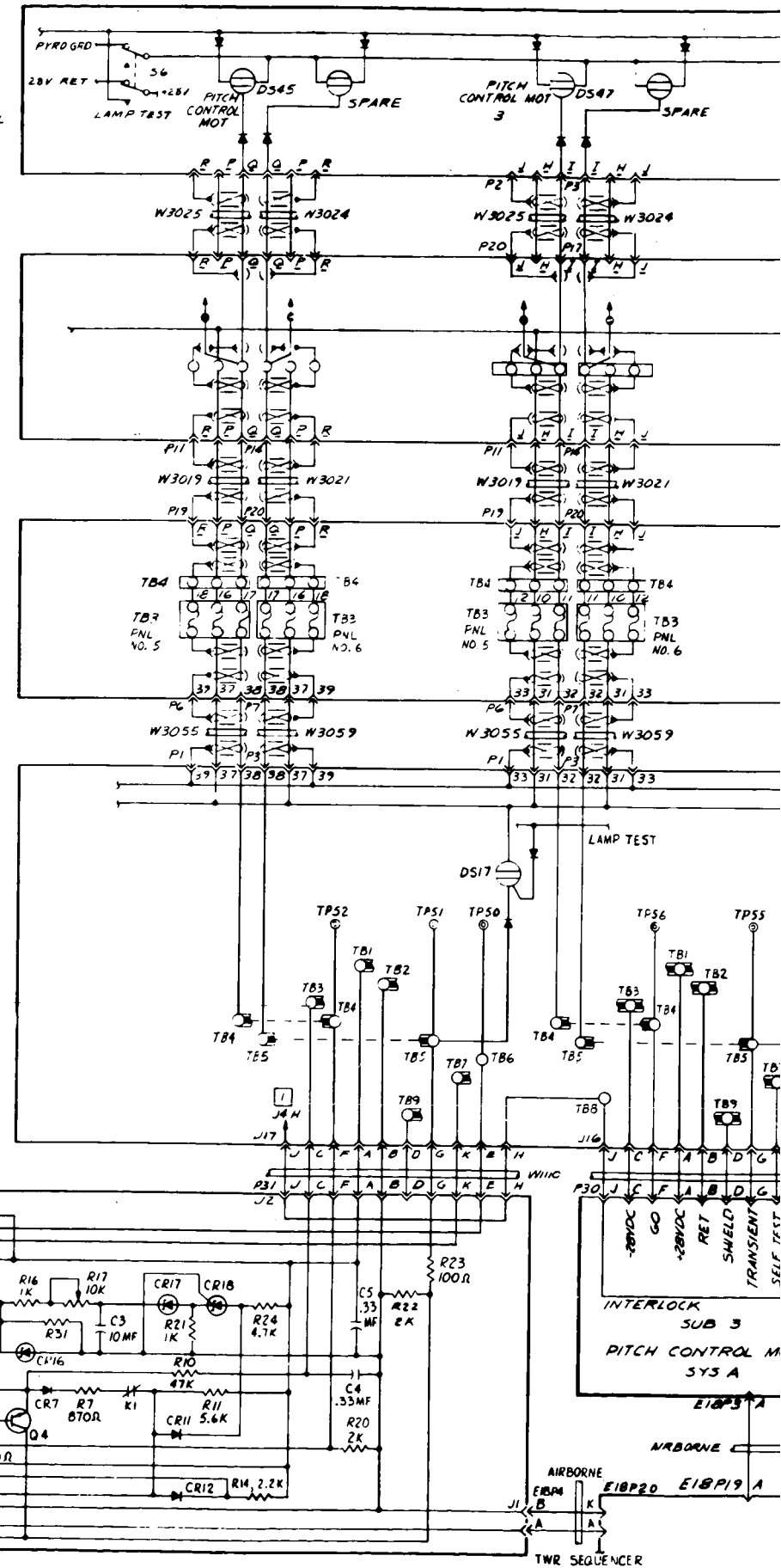


C14-914  
LES PANEL

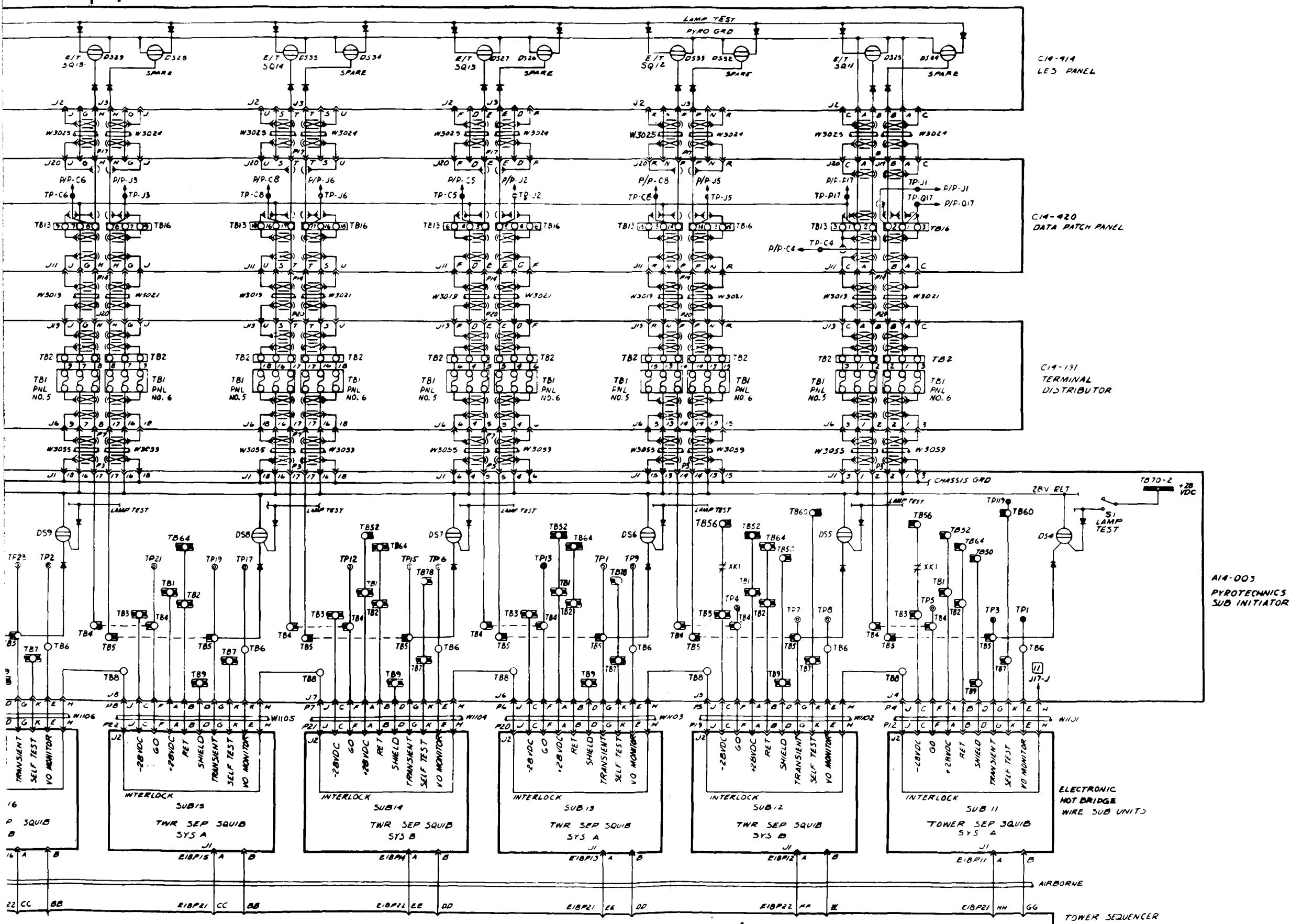
C14-420  
DATA PATCH  
PANEL

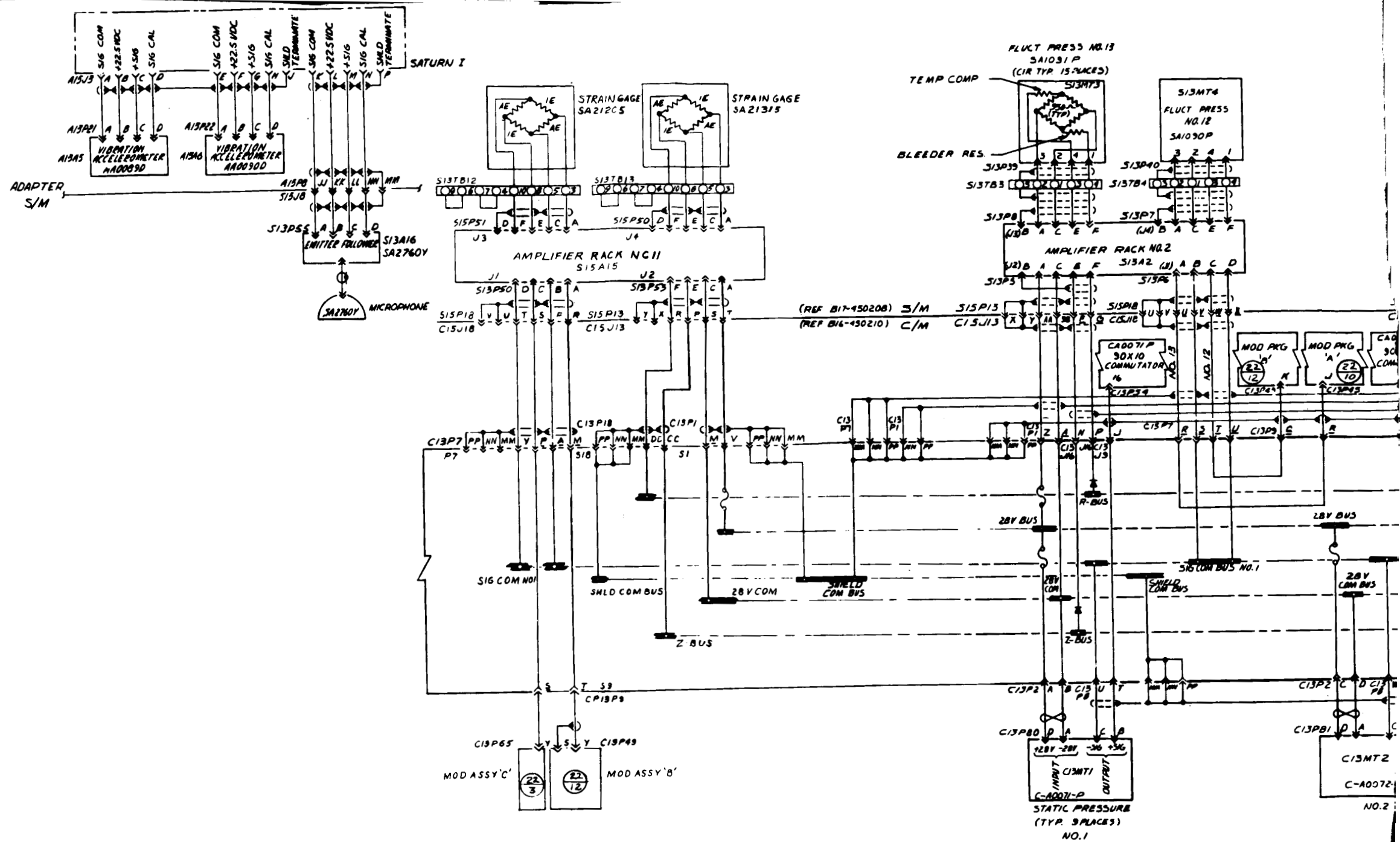
C14-191  
TERMINAL  
DISTRIBUTOR

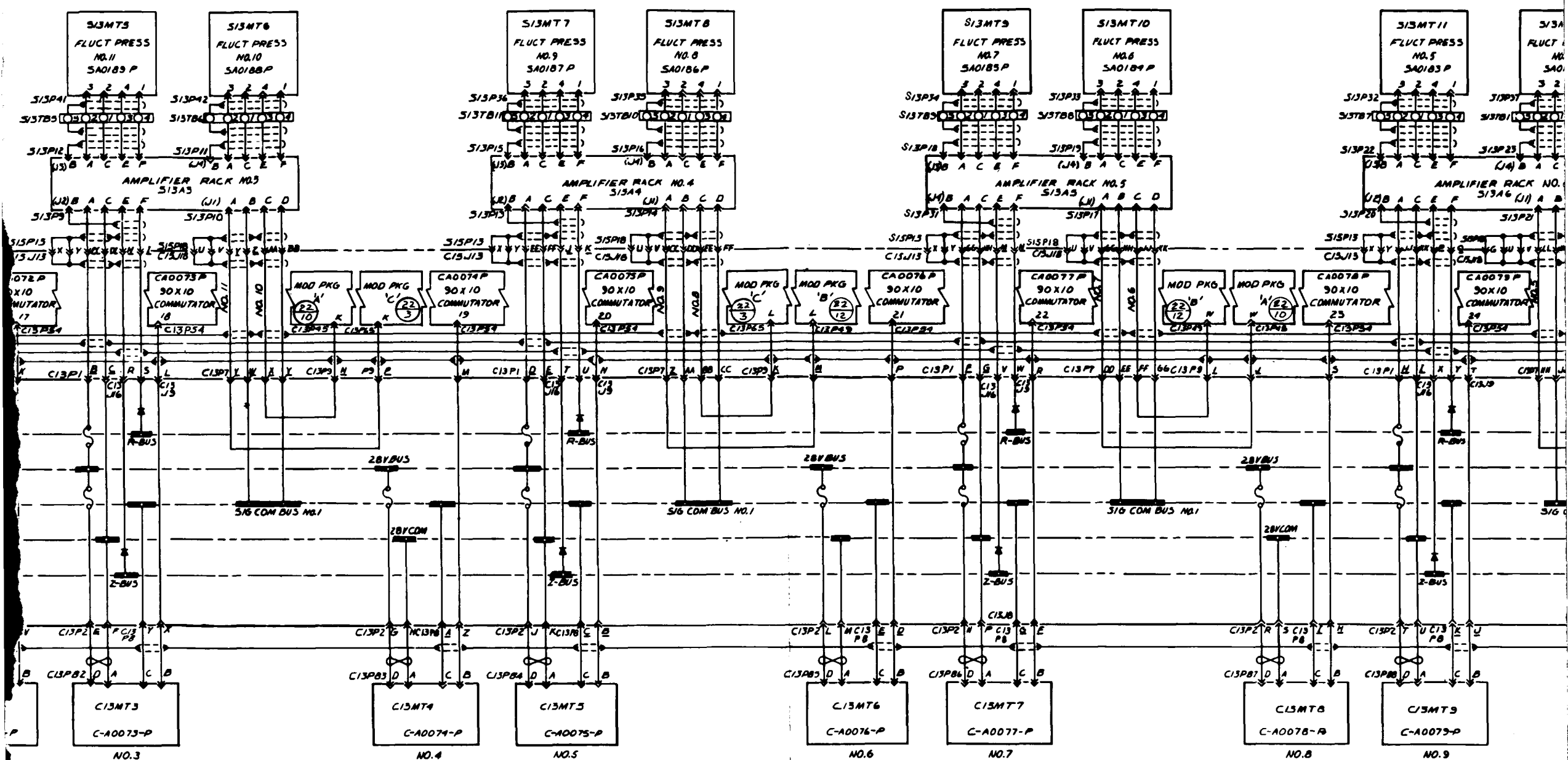
A14-003  
PYROTECHNICS  
SLB INITIATOR











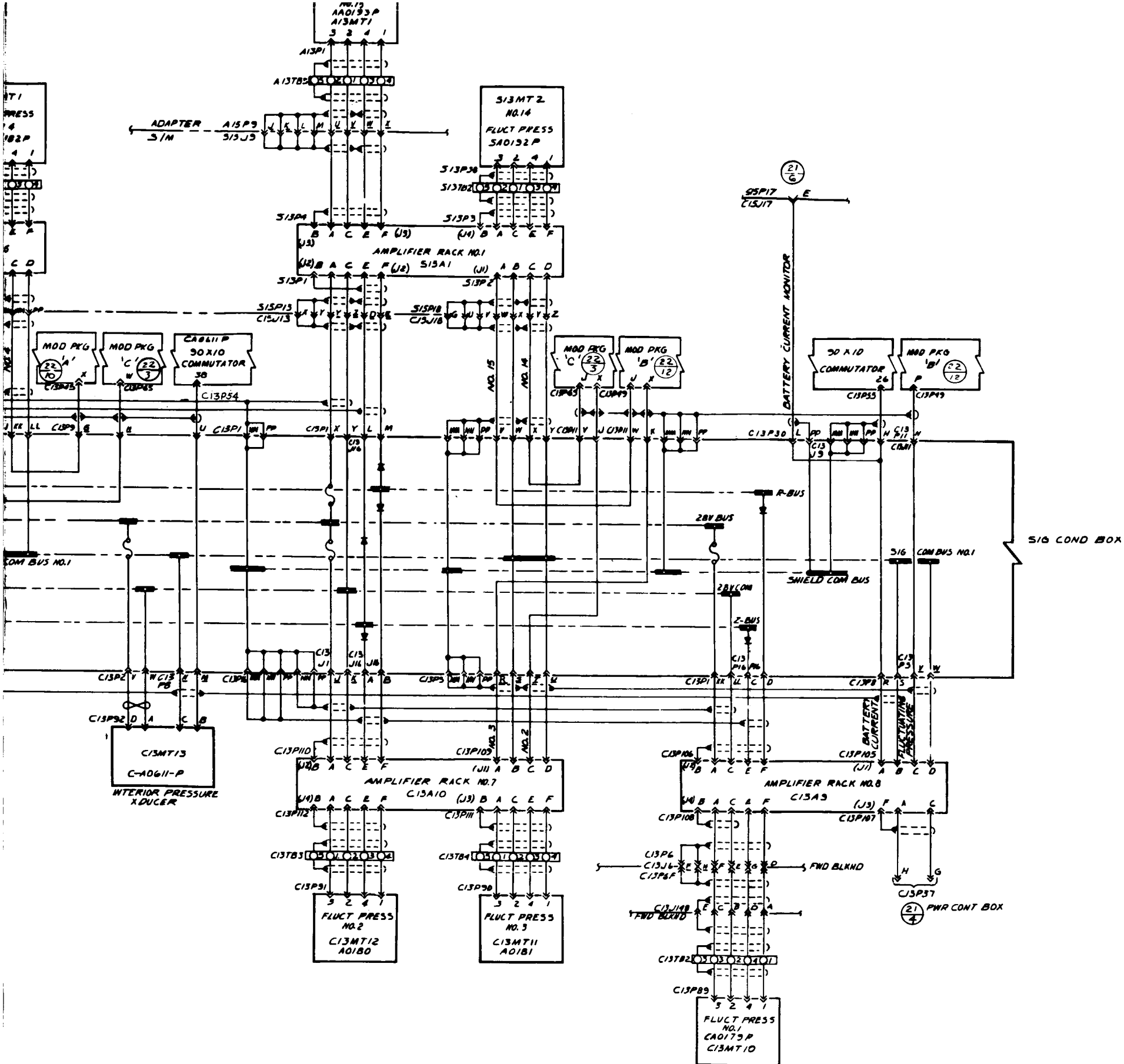
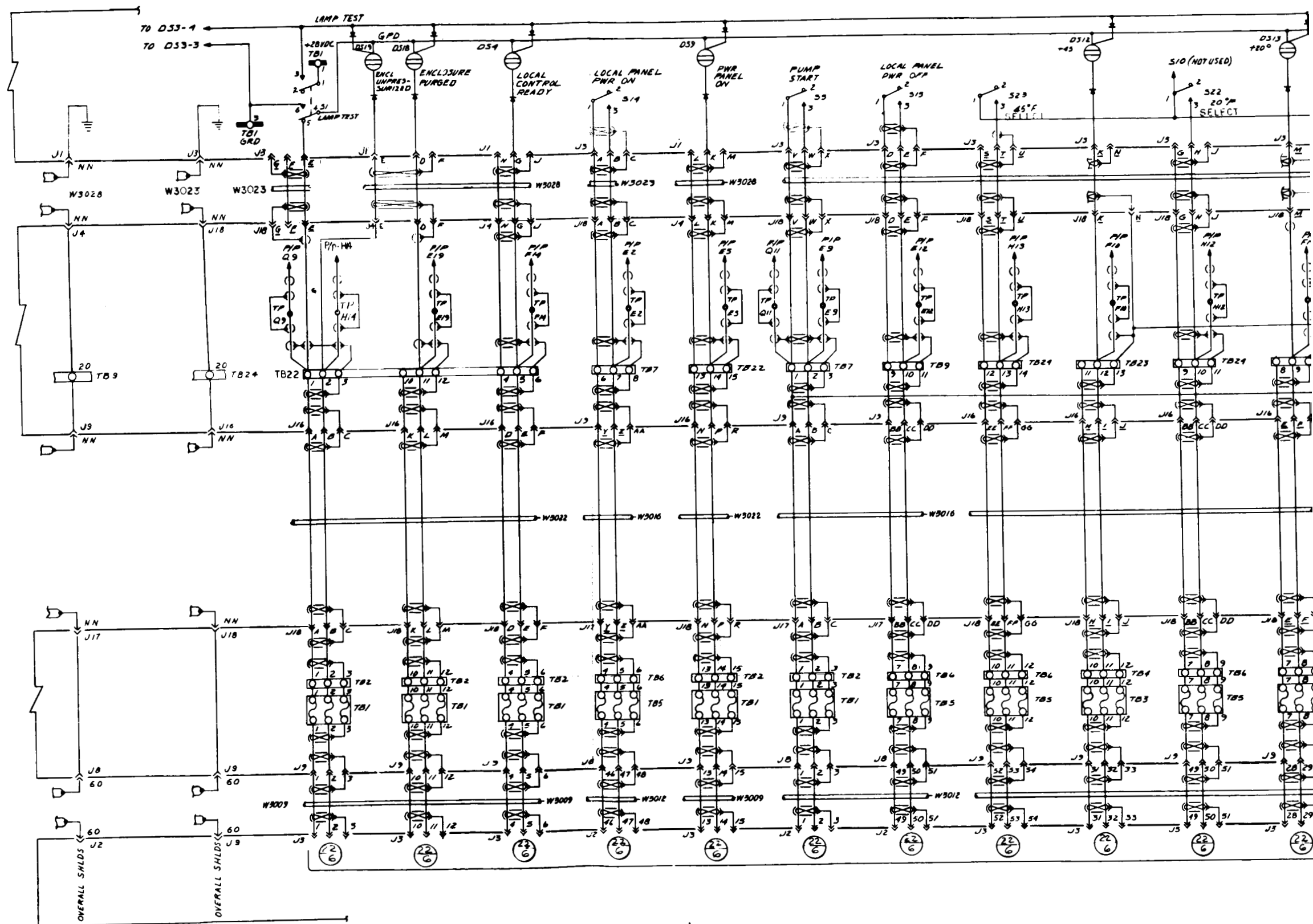
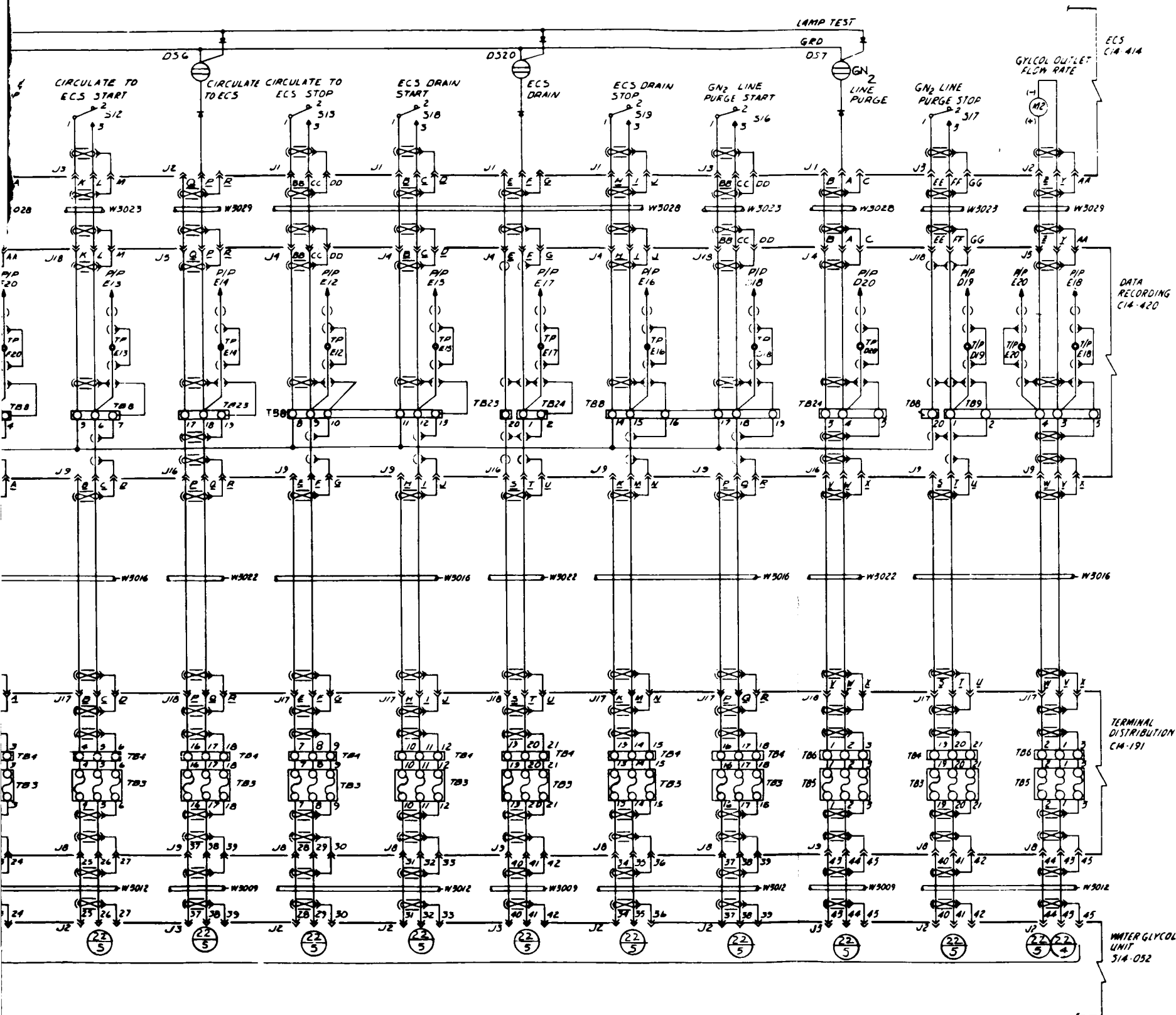


Figure 8-1. Boilerplate 15 and GSE Hangar Checkout Equipment Combined Systems Schematic (Sheet 3 of 5)





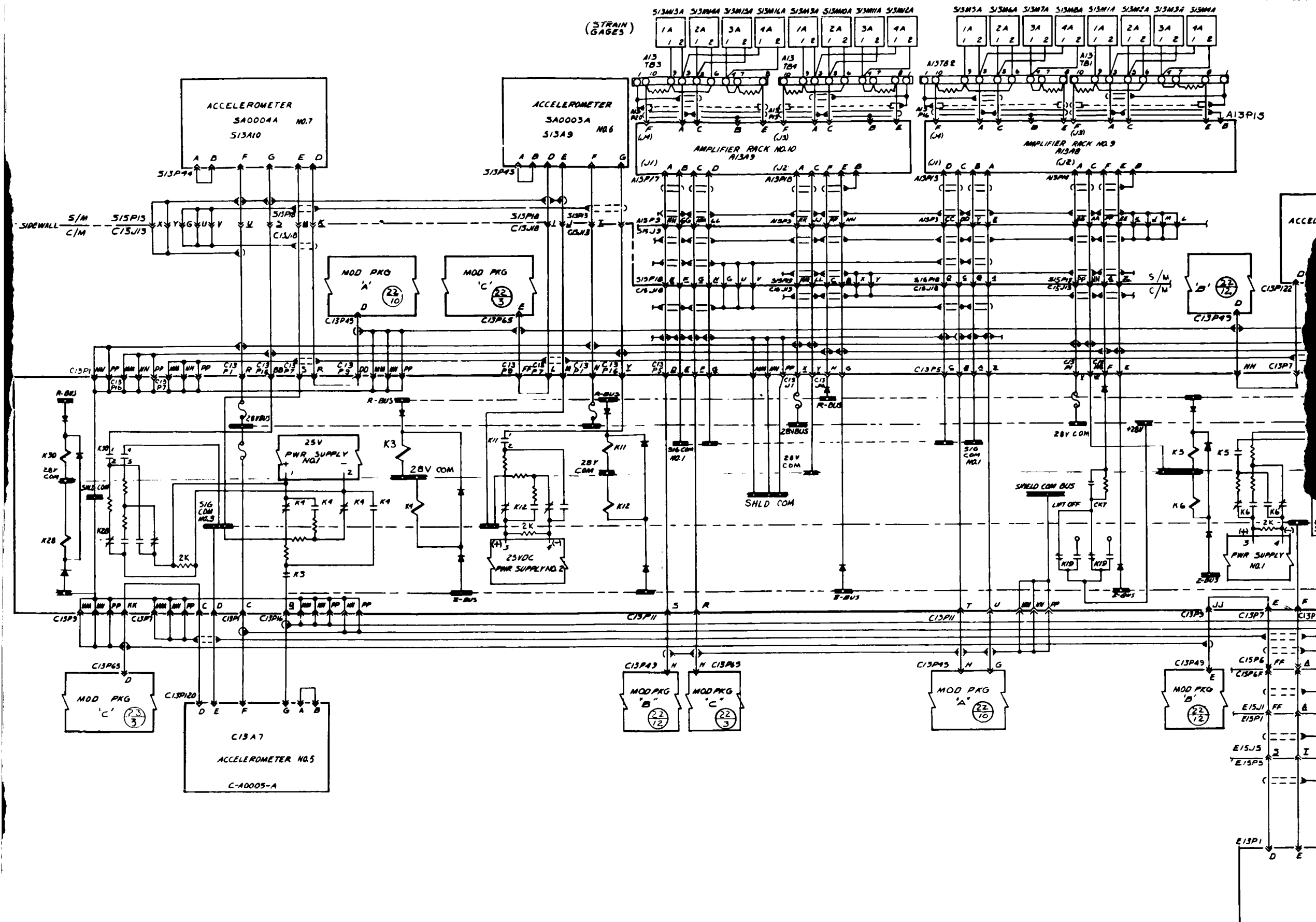




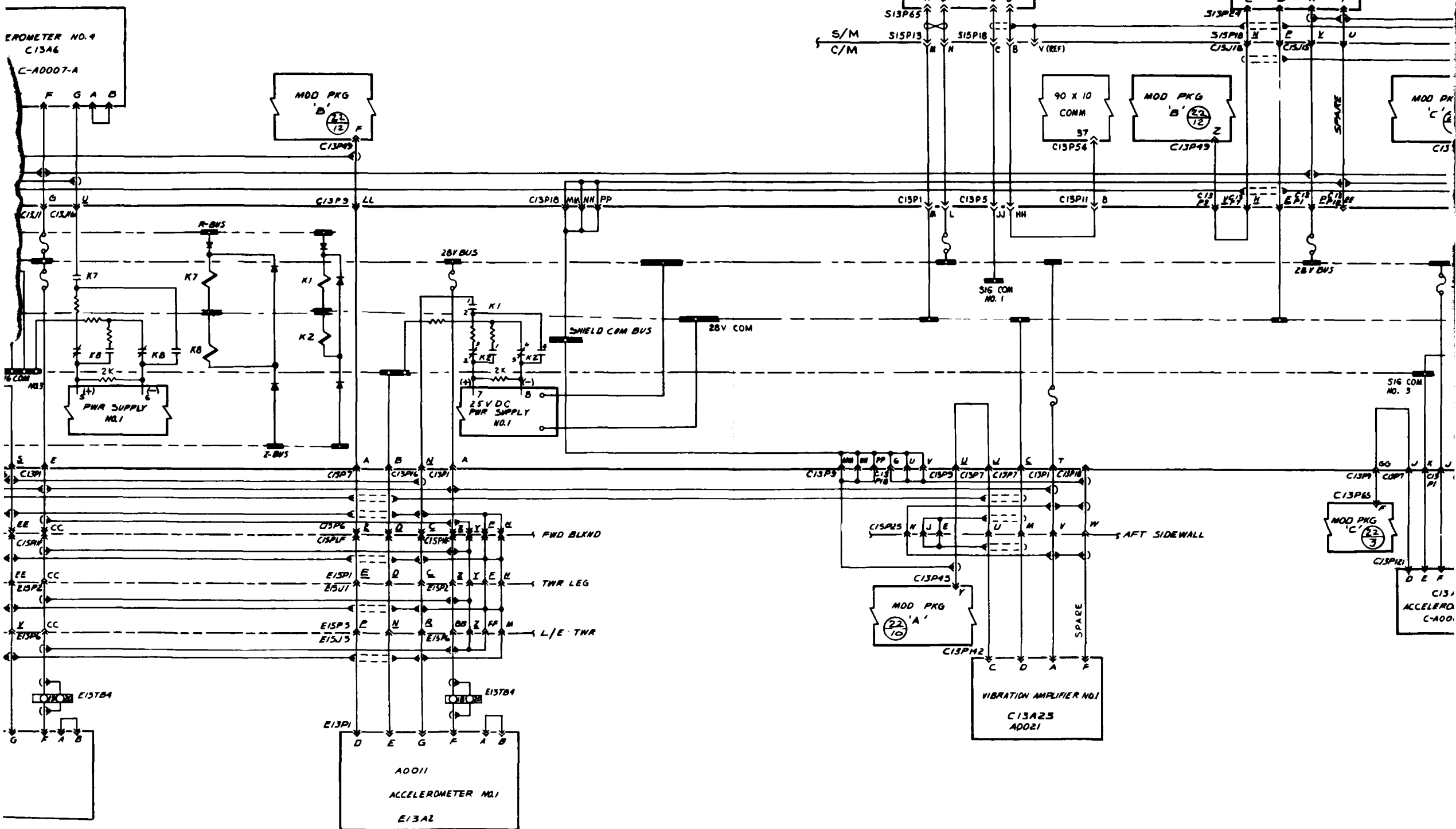
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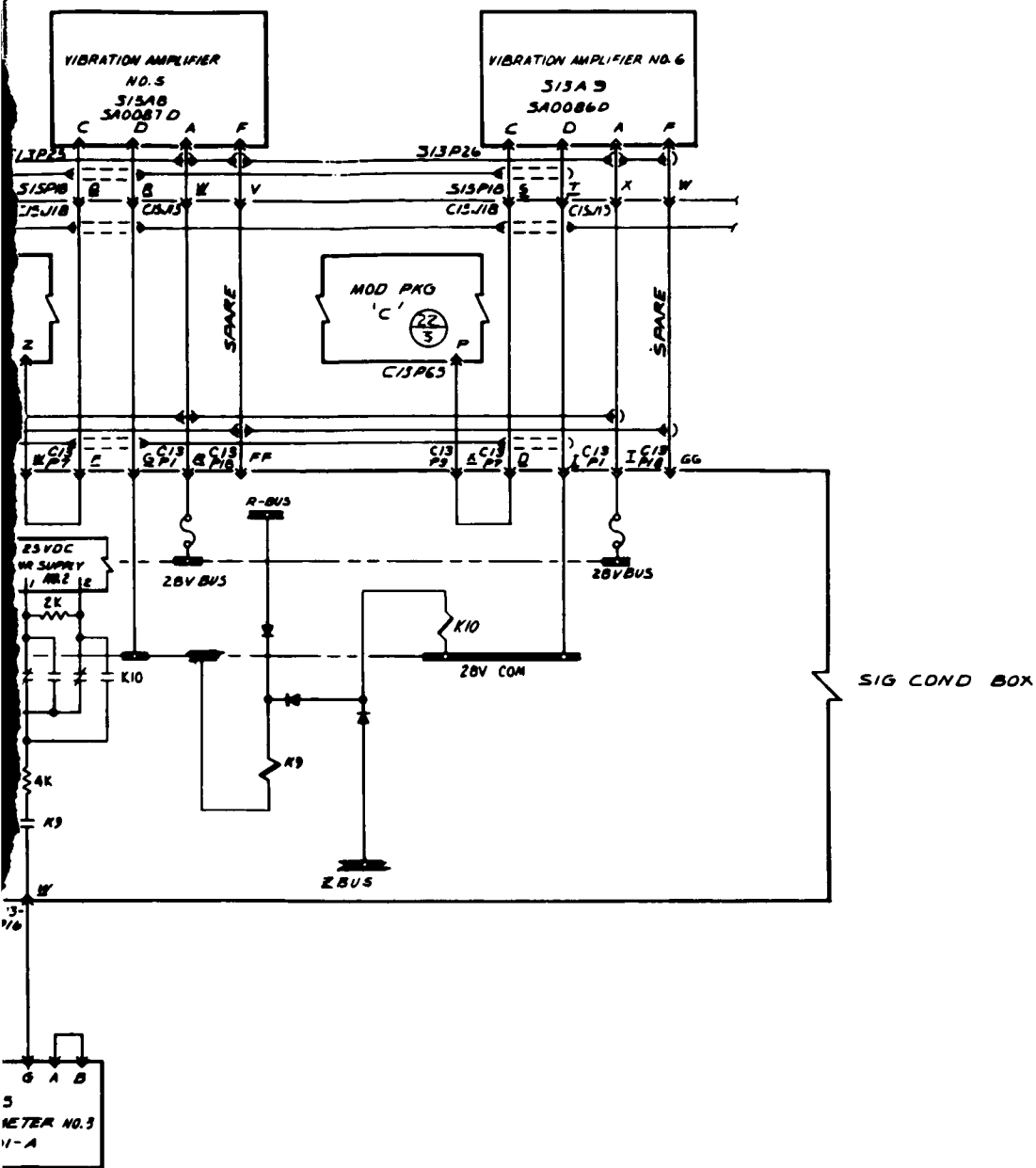
UNIT	SCHEMATIC GSE WIRING DIAGRAM	
C14-414 (ECS)	G16-985134B	G16-853973A
(LES)	G16-985130C	G16-853983B
C14-420 (DATA DLST)	G16-985158	G16-850533



4



5

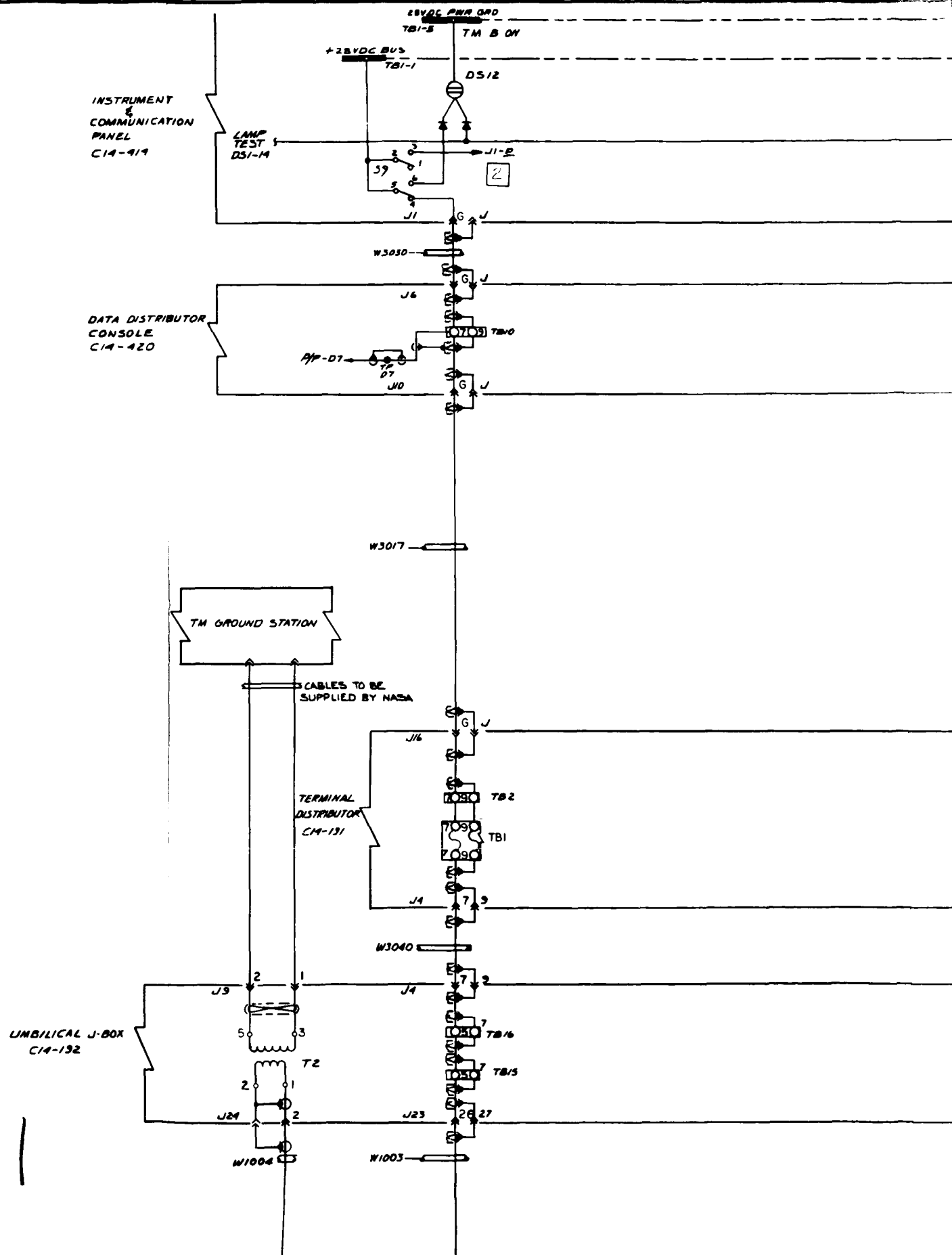


C14-191 (TERM. DIST.) G16-851308 T  
G16-851315 AND  
G16-851318A  
A14-003 (PYRO) G16-982108B G16-820589 A  
G16-820550  
G16-820551  
G16-820555  
ELECT HOT BRIDGE G16-982119 A  
BOILERPLATE  
SIG COND BOX SX530,106 (NASA)

SM-2A-561

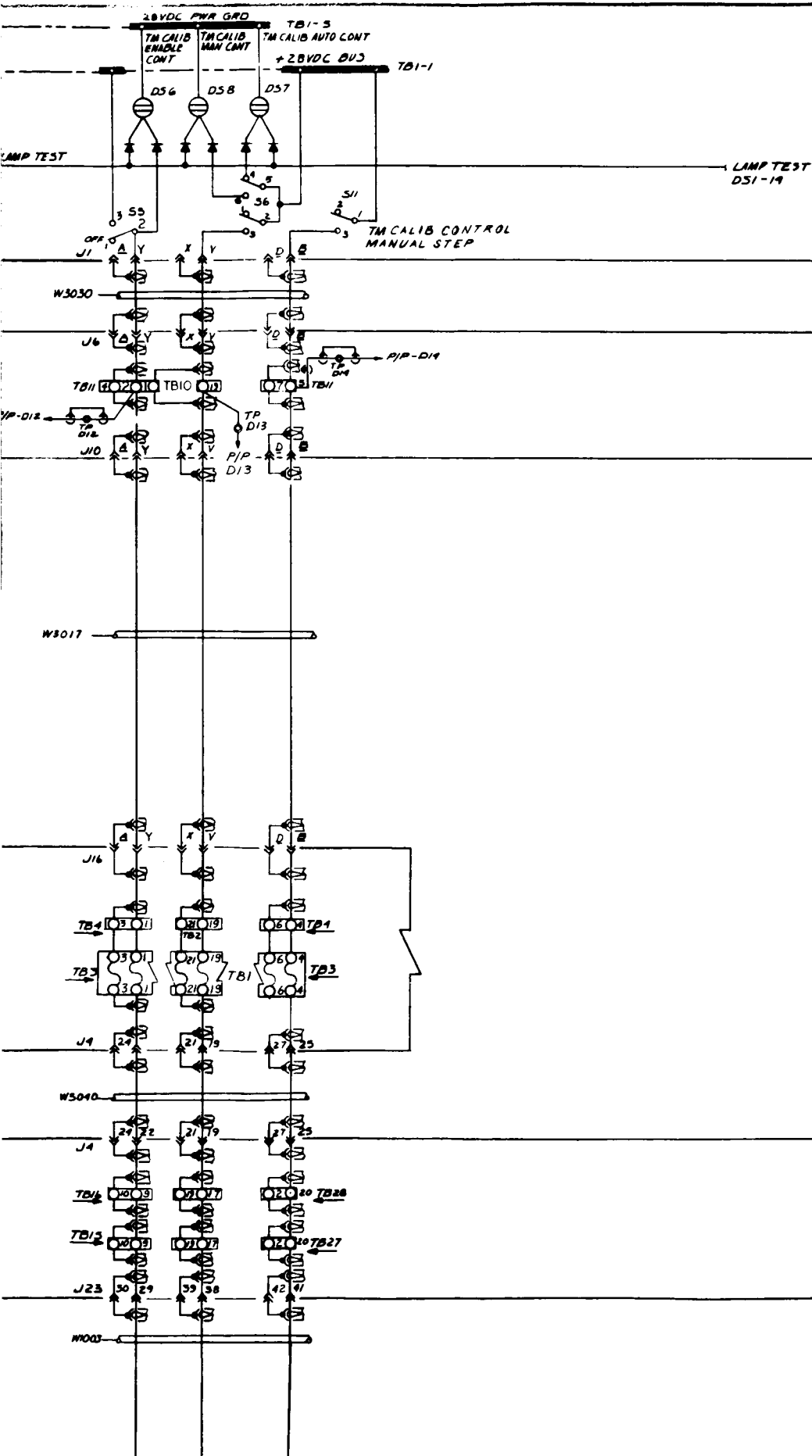
Figure 8-1. Boilerplate 15 and GSE Hangar Checkout Equipment  
Combined Systems Schematic (Sheet 4 of 5)

11

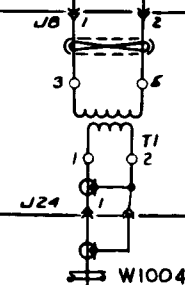


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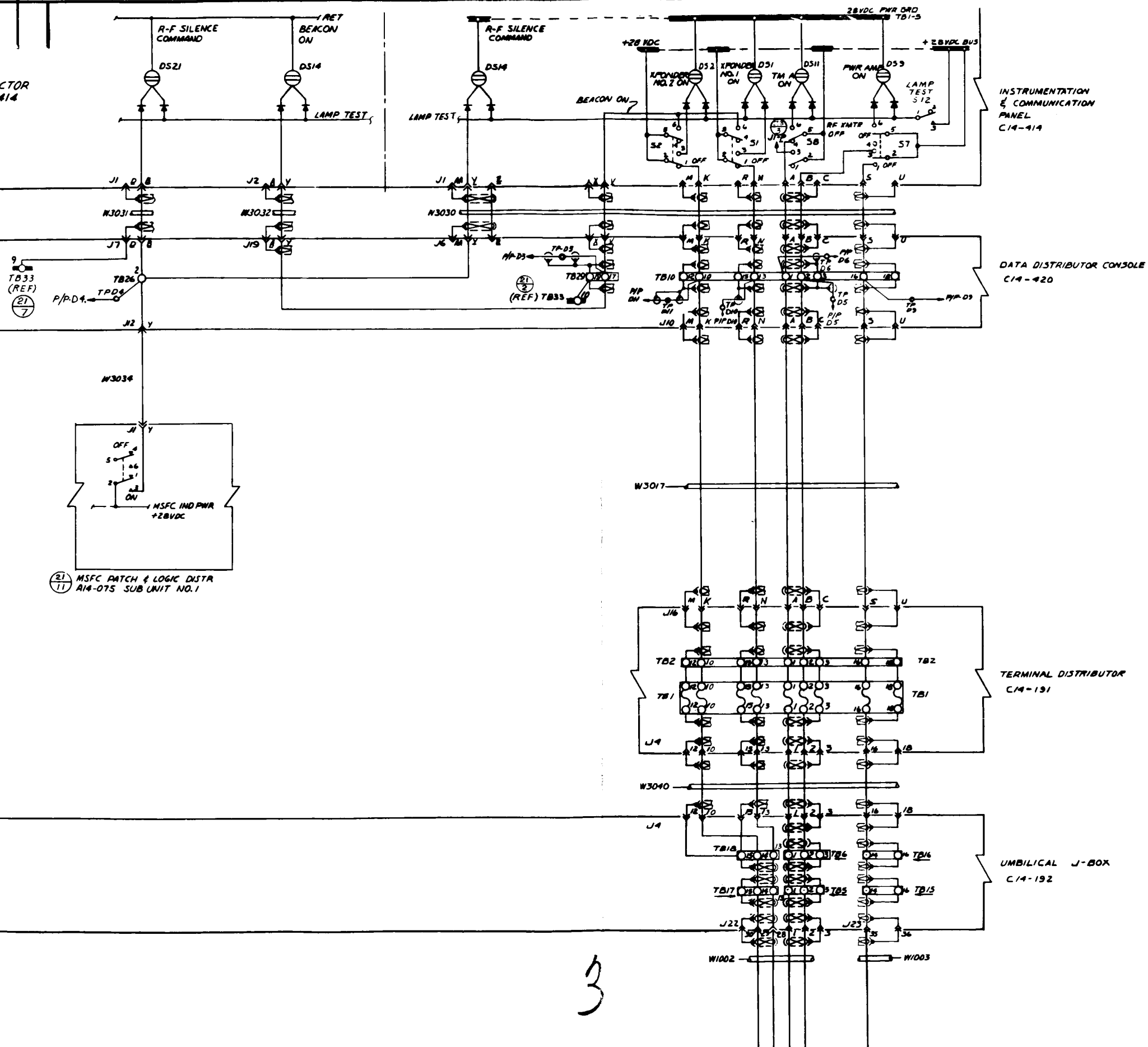
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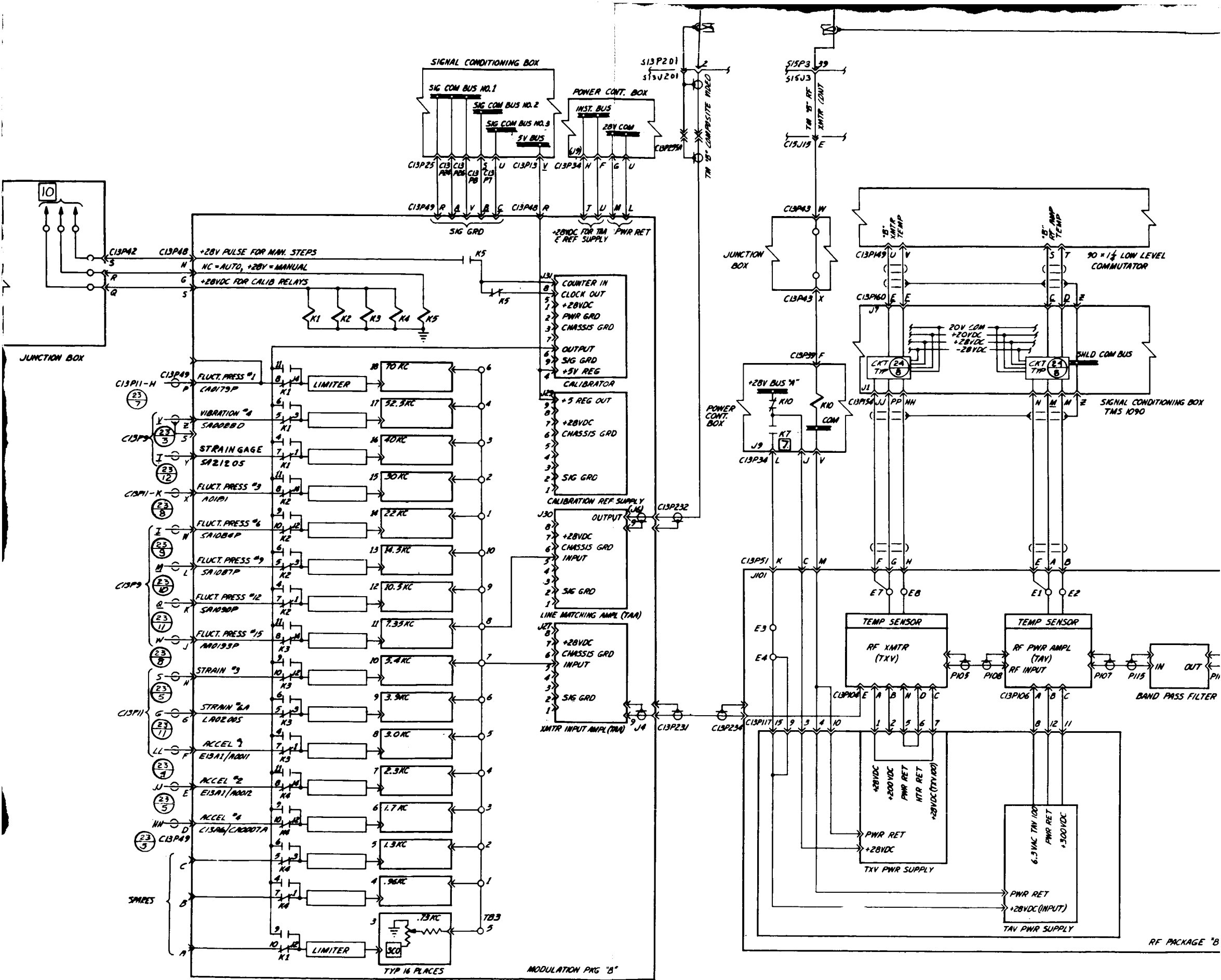
CABLES TO BE  
SUPPLIED BY NASA

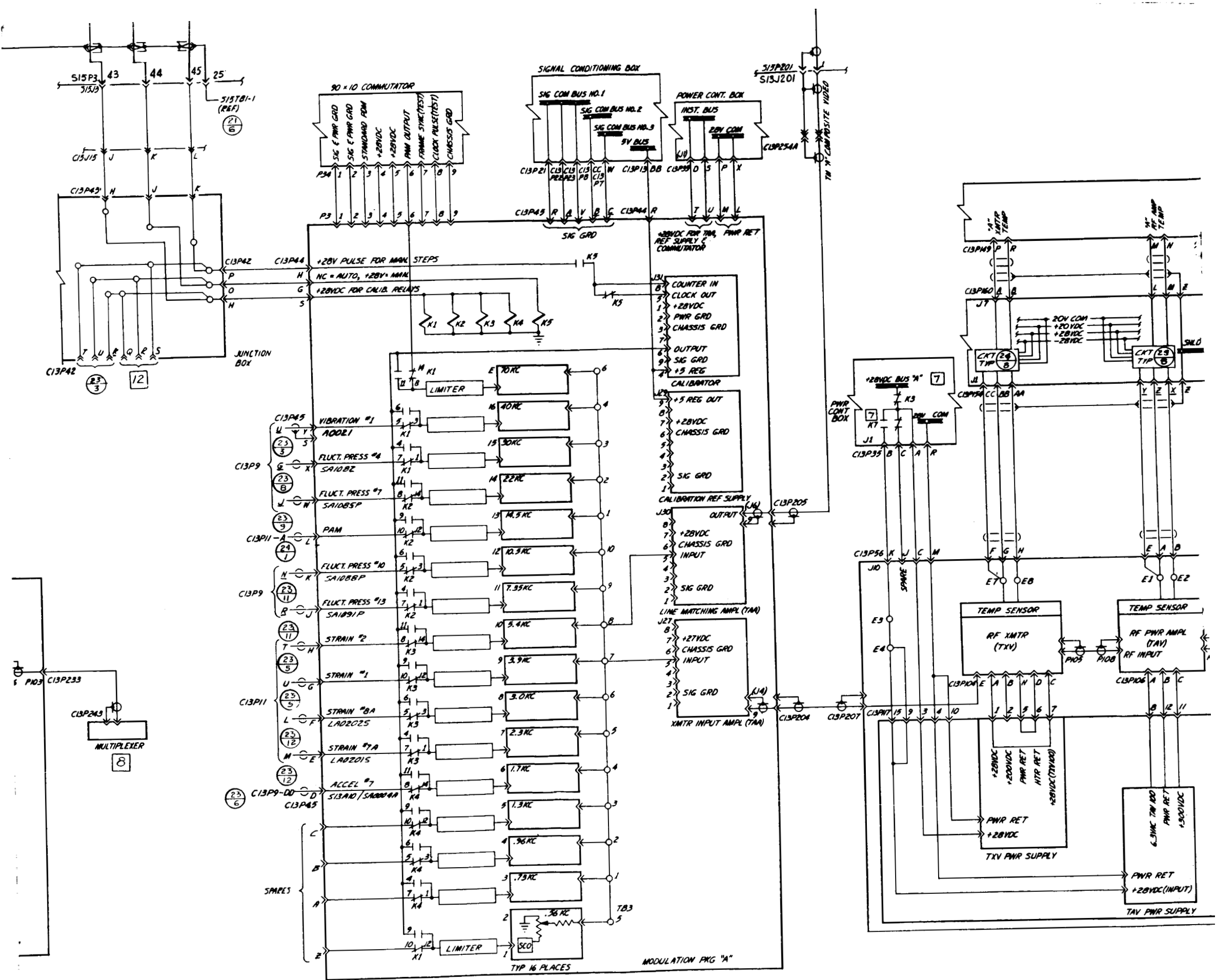


2

ST CONDUCTOR  
NEL C14-414







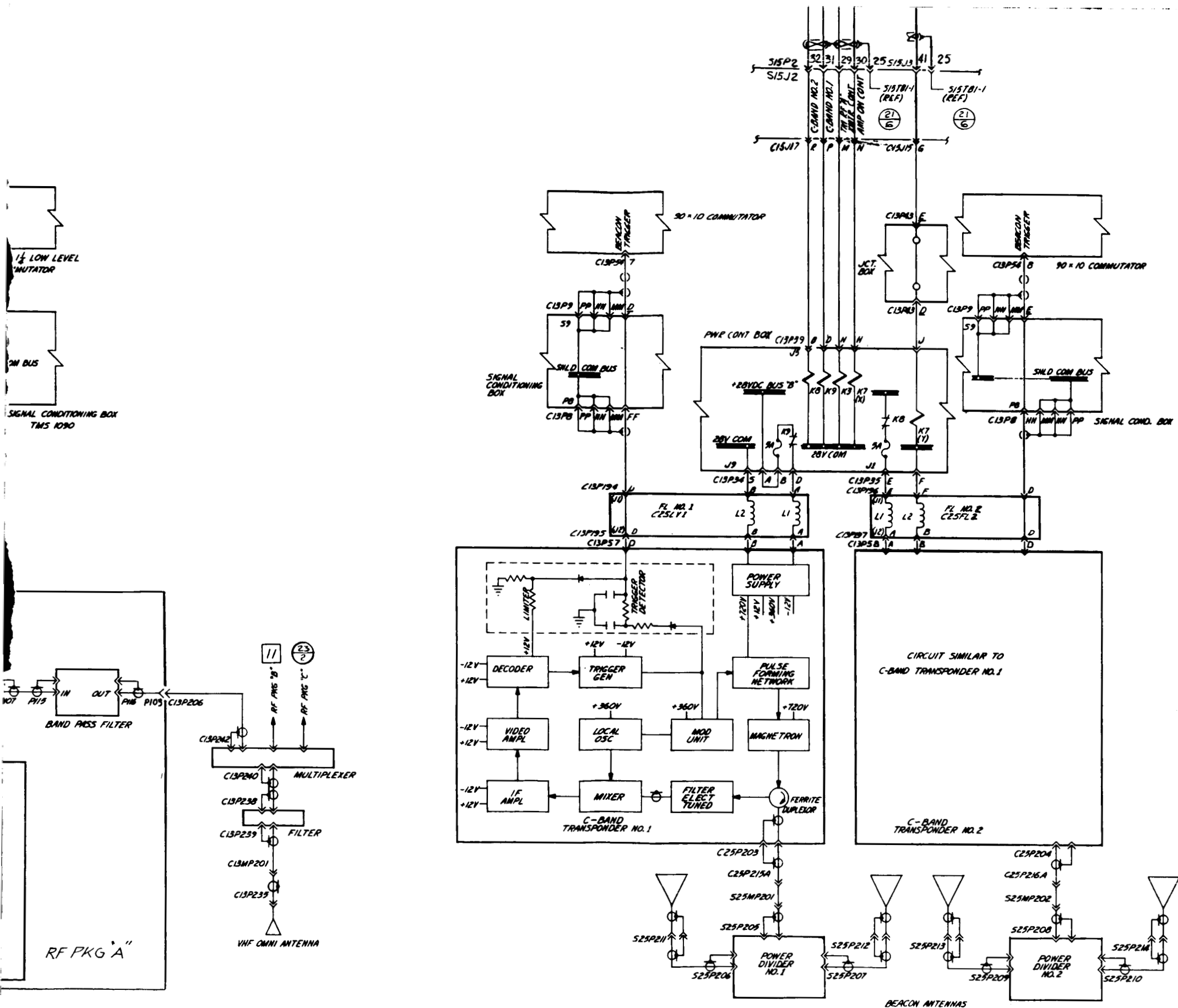
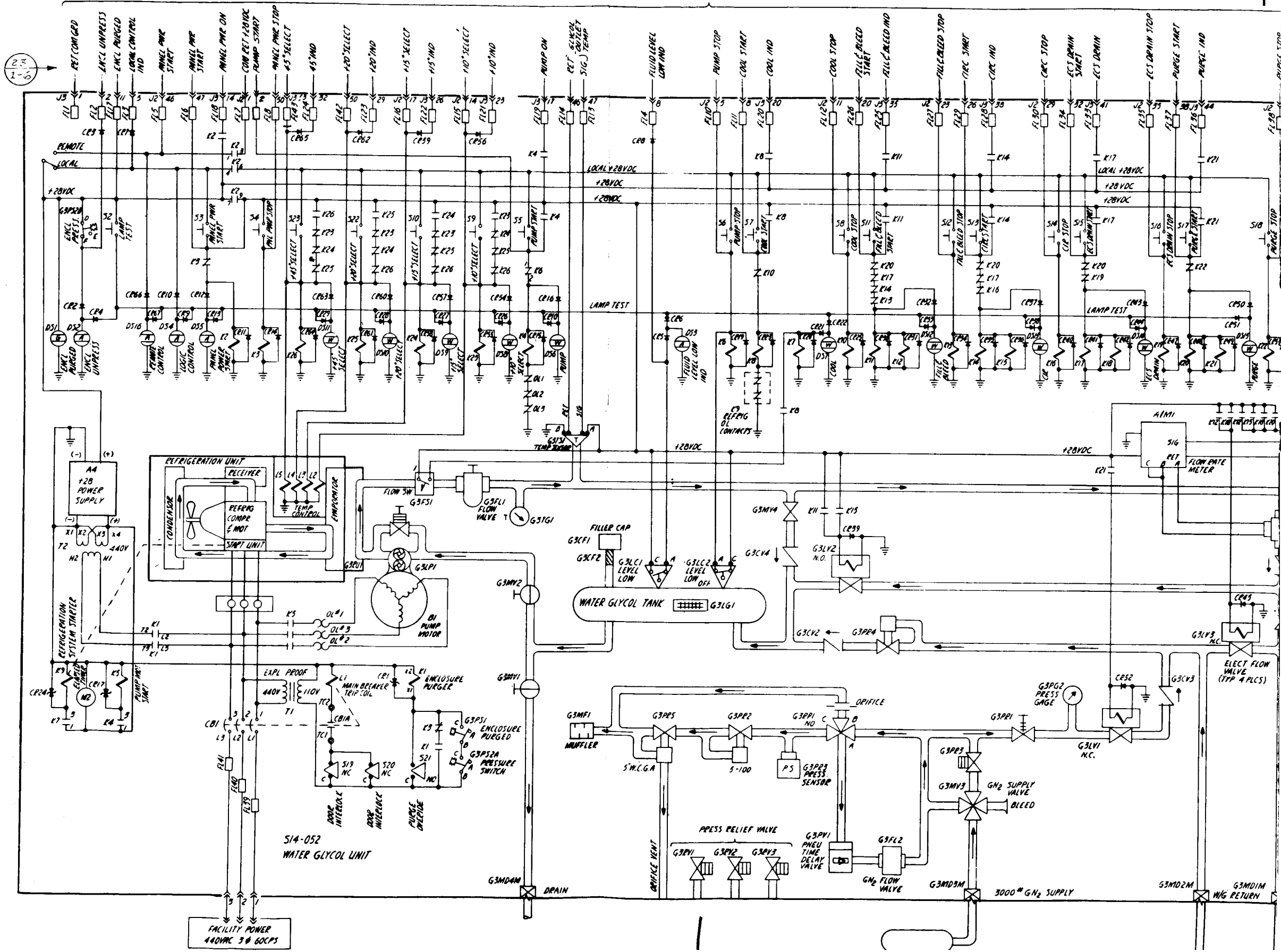


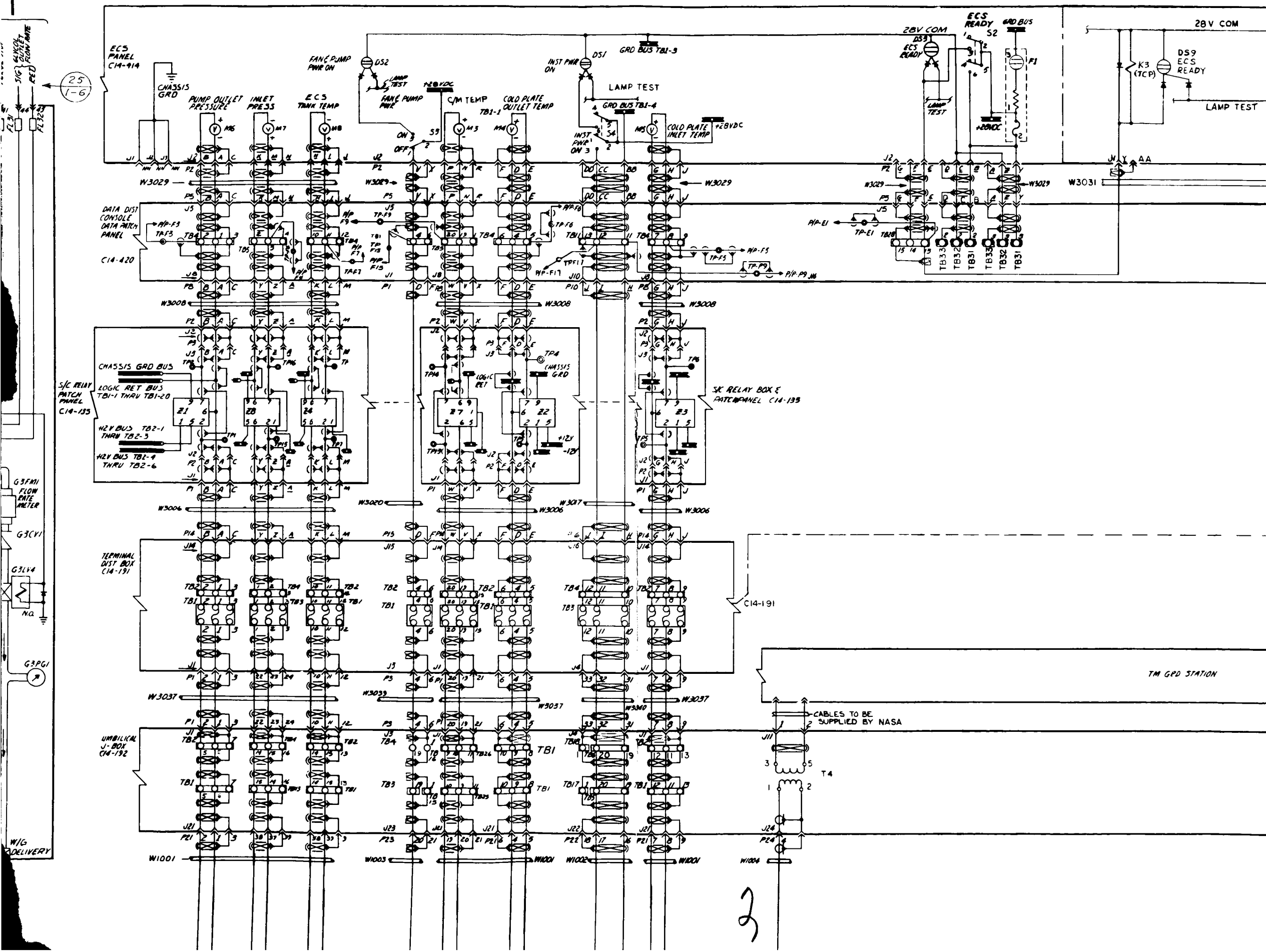
Figure 8-1. Boilerplate 15 and GSE Hangar Checkout Equipment Combined Systems Schematic (Sheet 5 of 5)

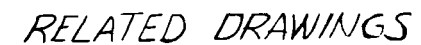
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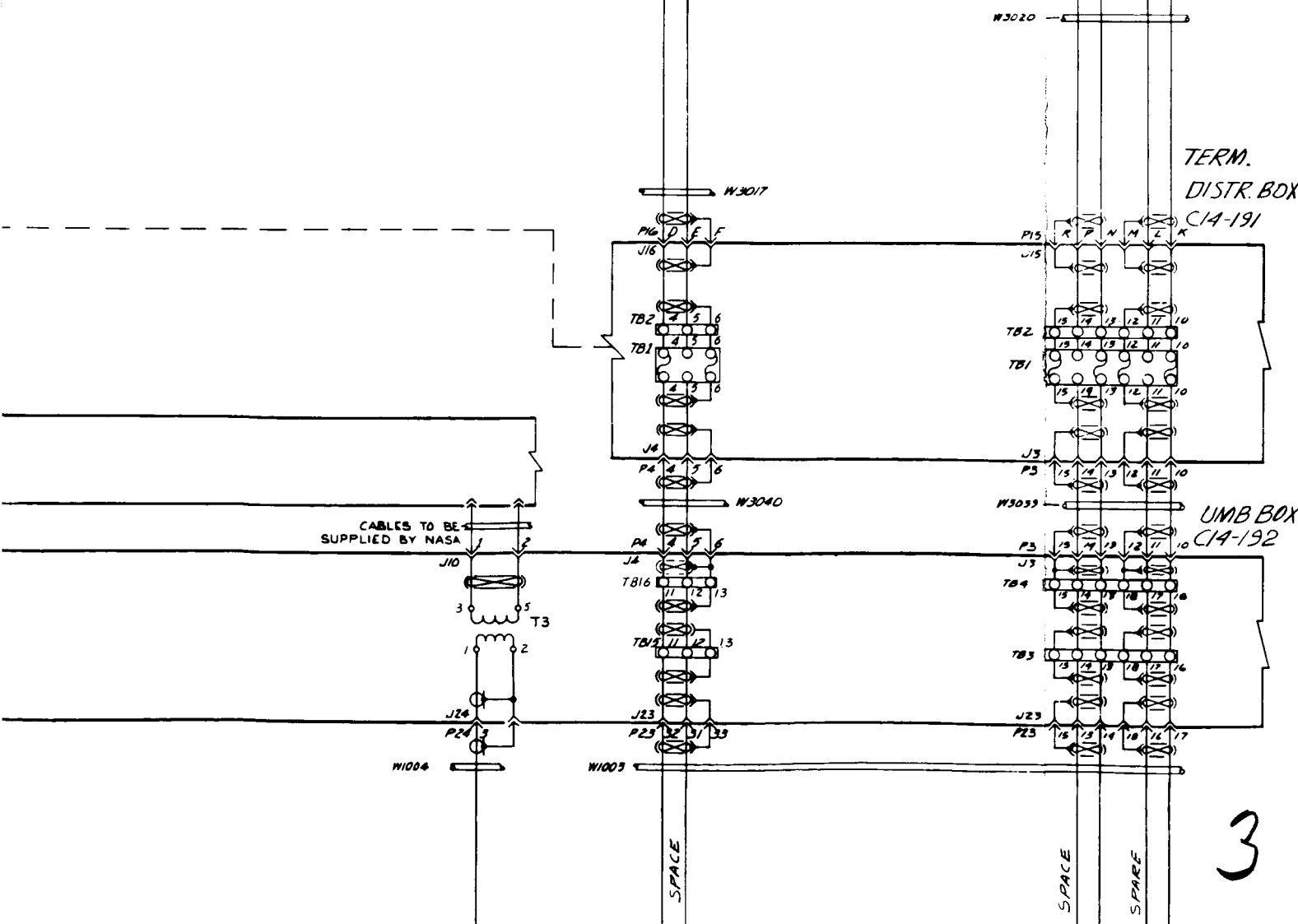
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CM-414  
ECS CONTROLS

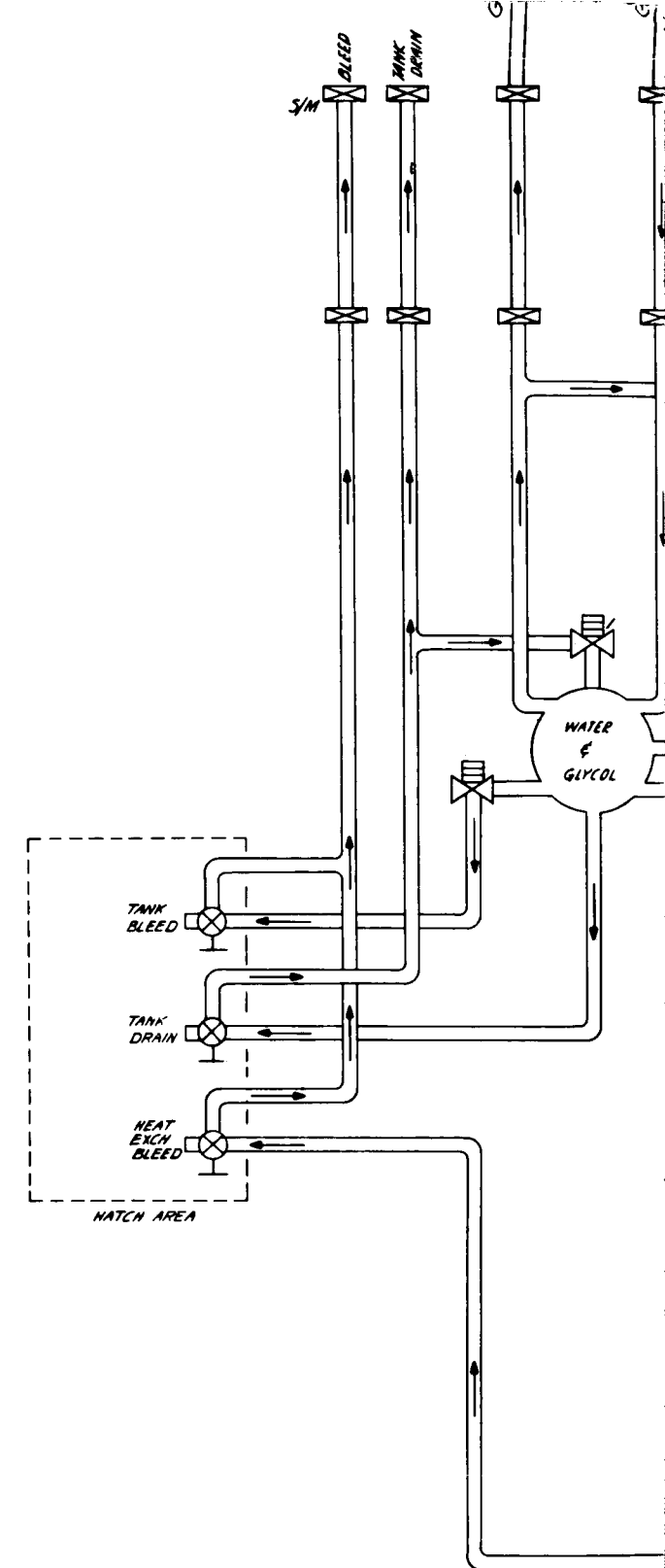


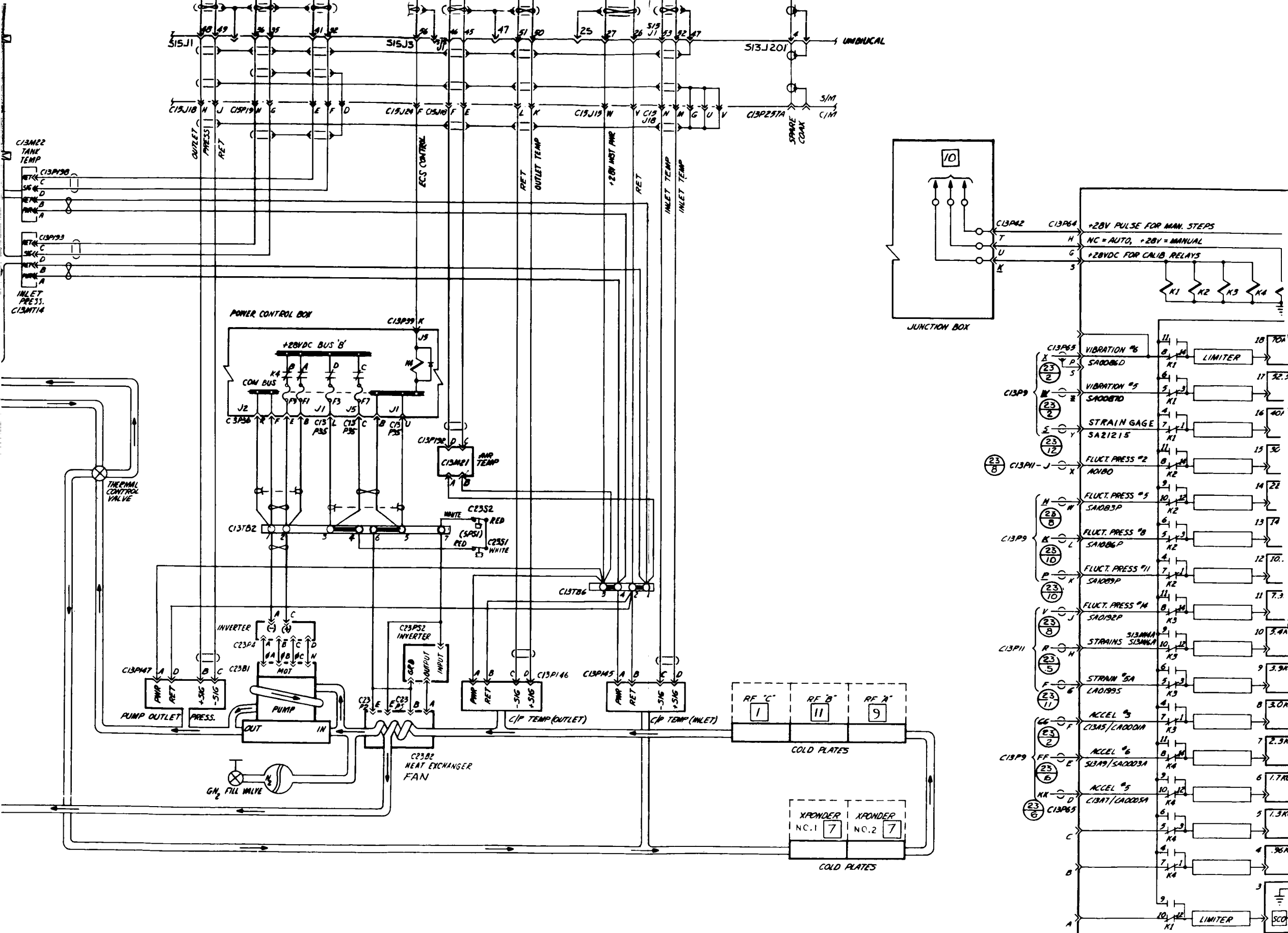
BOILERPLATE

RELAY BOX	_____	B17-450221B
PWR CONT BOX	_____	SX540,007(NASA)
SIG COND BOX	_____	SX530,106(NASA)
90 X 1 1/4 COMM(SIG W/D)	_____	SX530,057(NASA)
TM R-F PKG	_____	SD530,136(NASA)
TM MOD PKG "A"	_____	SX530,135(NASA)
TM MOD PKG "B" & "C"	_____	SX530,097(NASA)

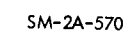


RELAY NO.	NO. OF POLES	ZONE LOCATION	
		COILS	POLES
K1	3	6	6
K2	4	6	6
K3	2	6	6
K4	3	6	6
K5	3	6	6
K6	1	5	6
K7	1	5	6
K8	3	5	5
K9	2	6	5
K10	1	5	5
K11	3	5	5
K12	2	5	5
K13	1	5	5
K14	3	5	5
K15	2	5	5
K16	1	5	5
K17	4	5	5
K18	2	5	4, 5
K19	1	5	5
K20	4	5	4, 5
K21	3	5	5
K22	1	4	5
K23	4	6	6
K24	4	6	6
K25	4	6	6
K26	4	6	6

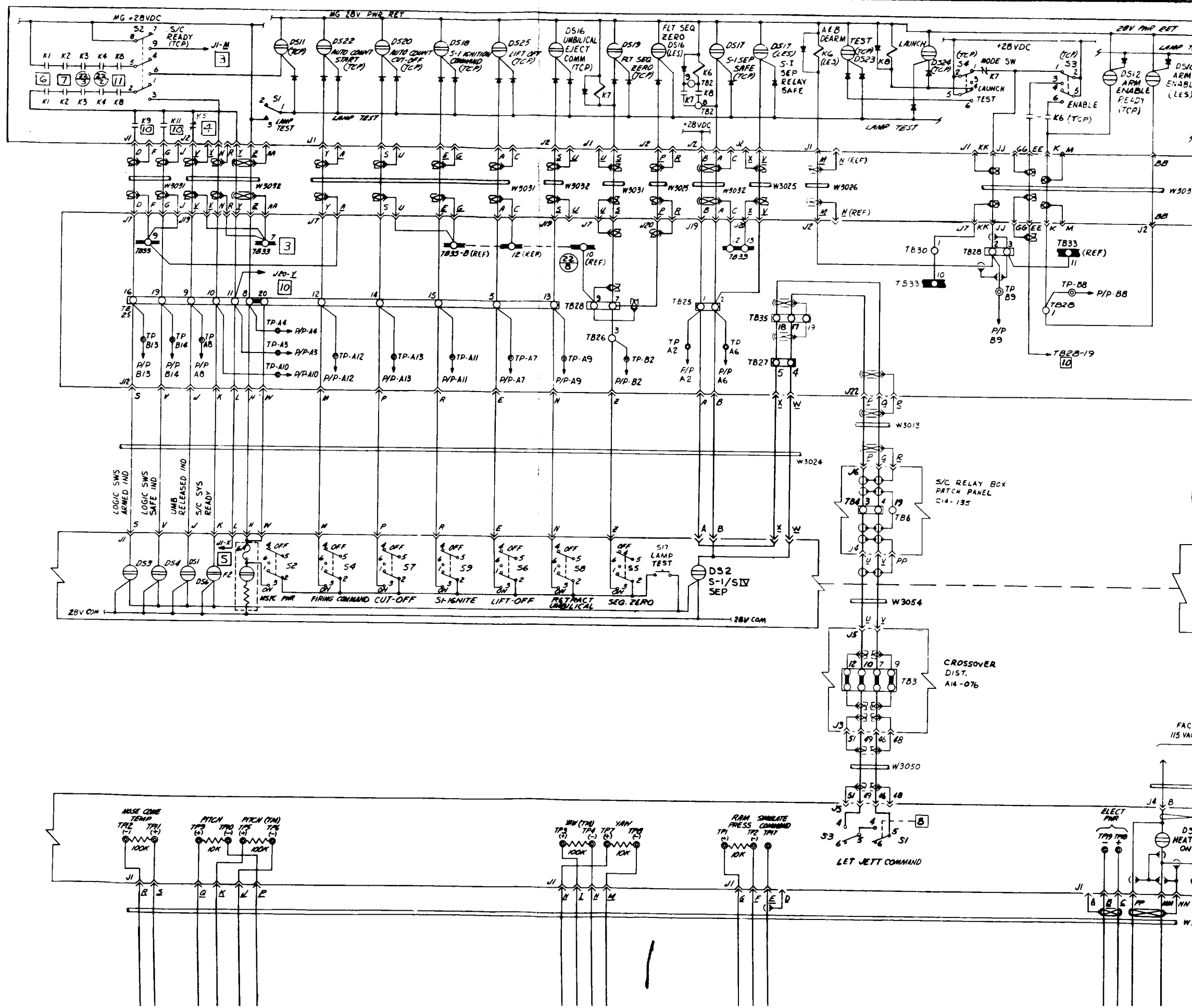


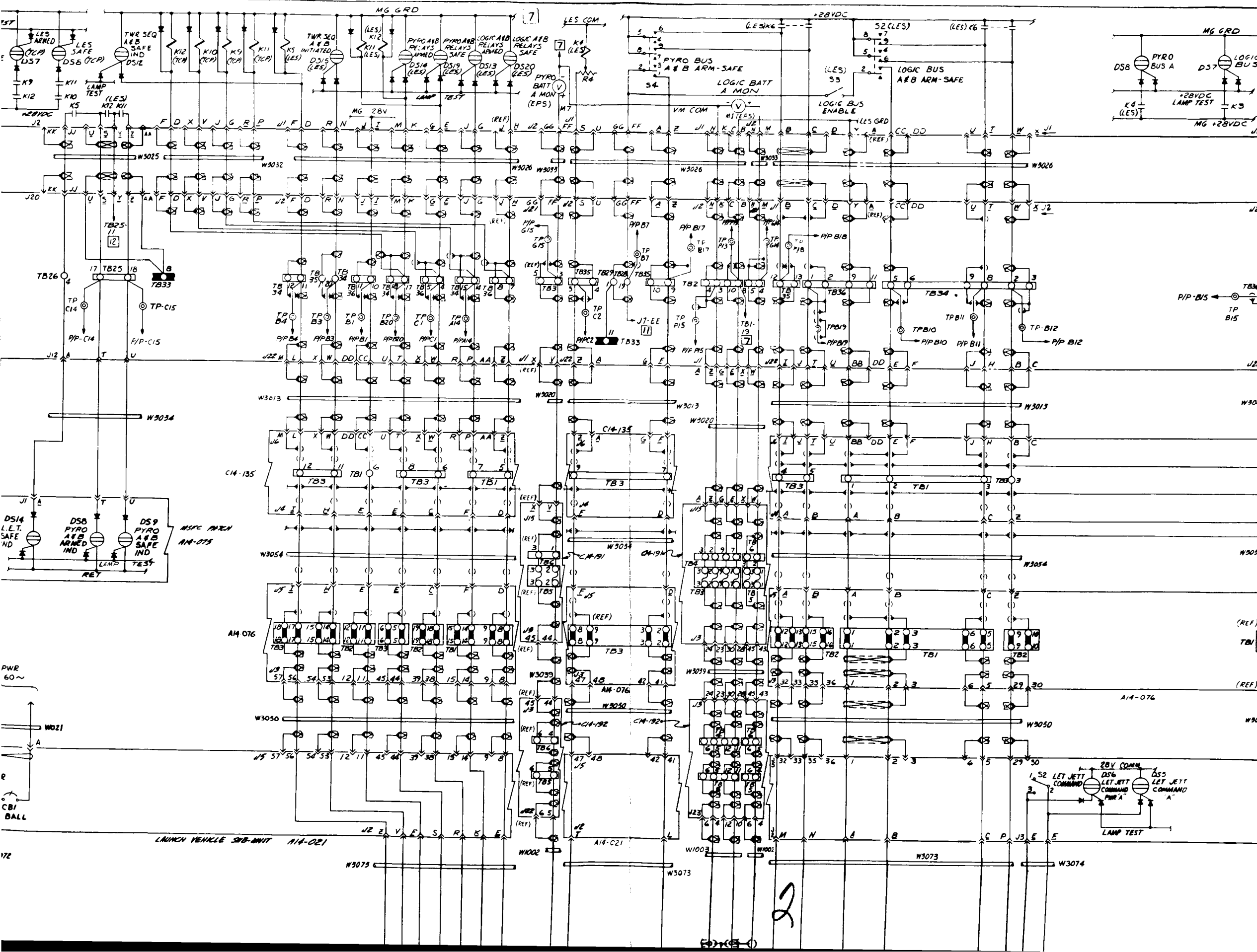


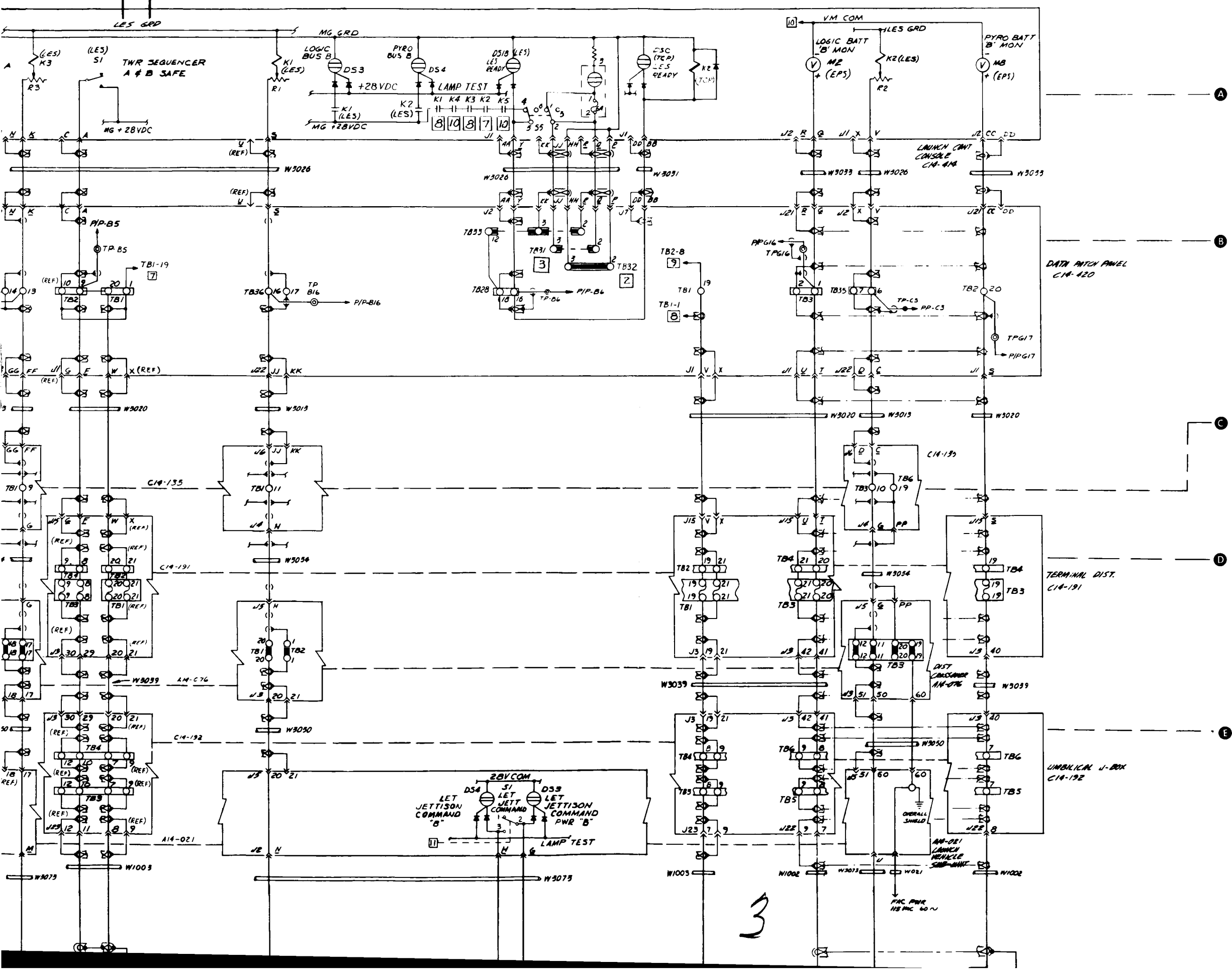


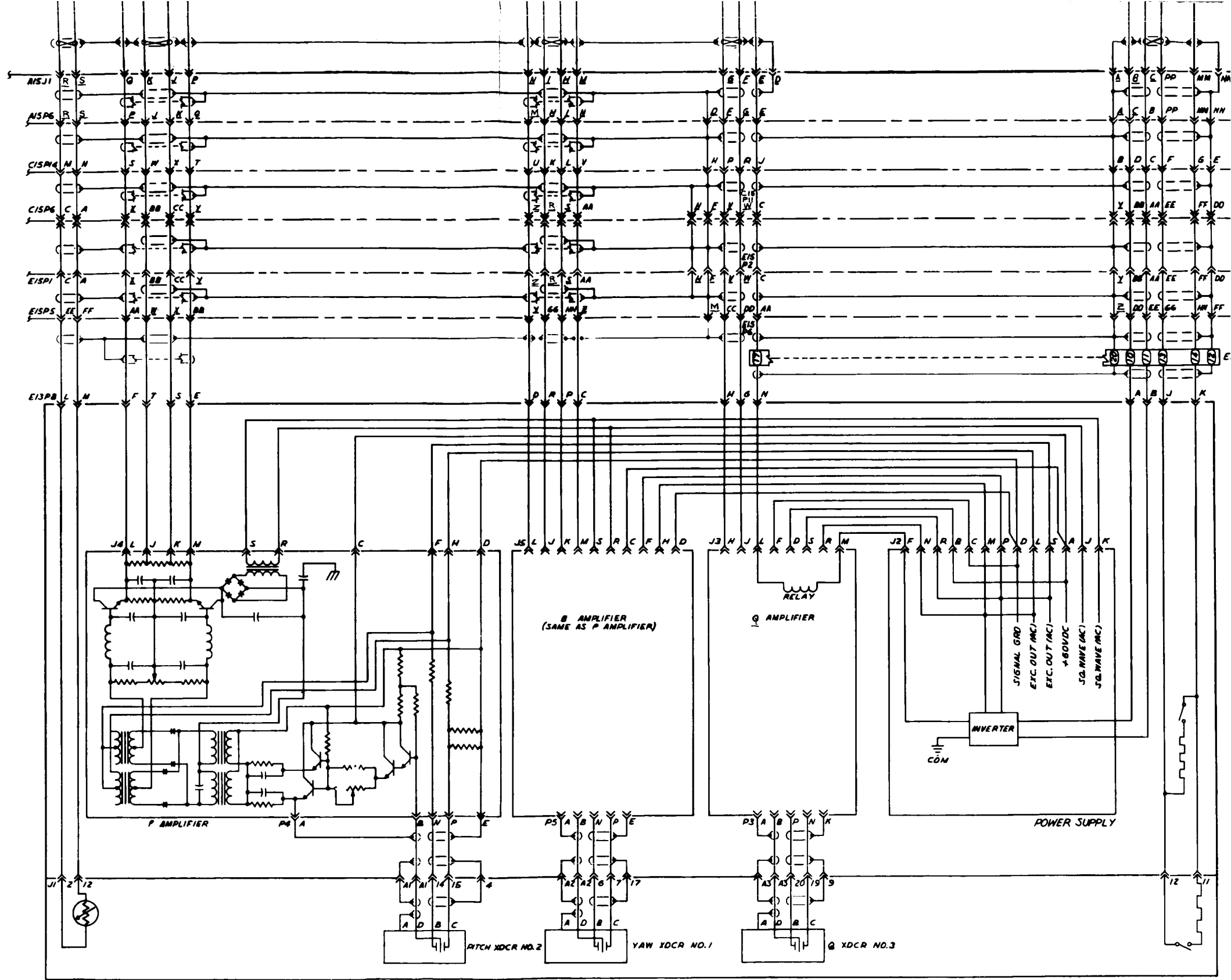


6









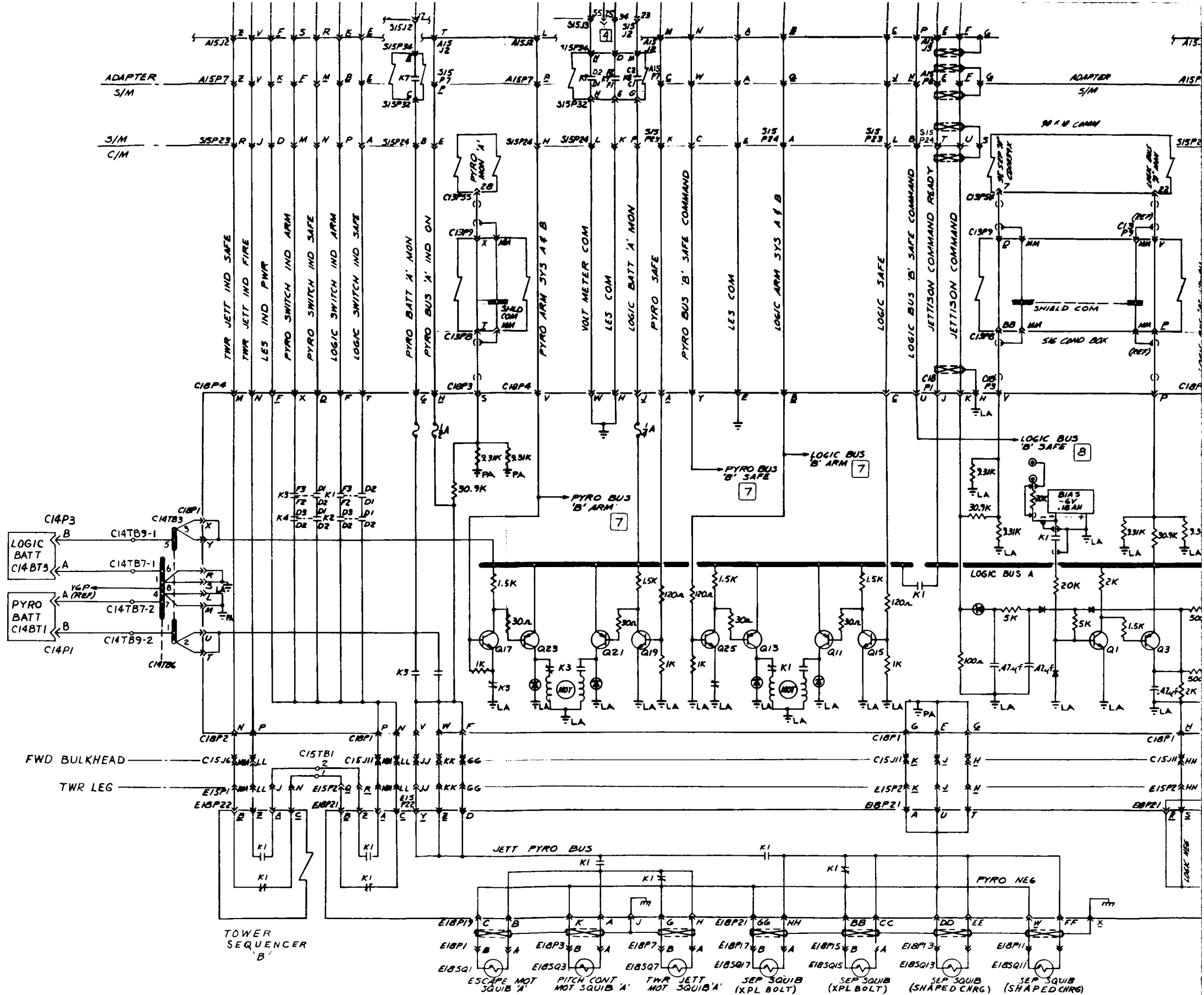
"Q" BALL

ADAPTER  
S/M  
S/M  
C/M  
C/M  
FWD BULKHEAD

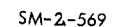
TWR LEG

TWR

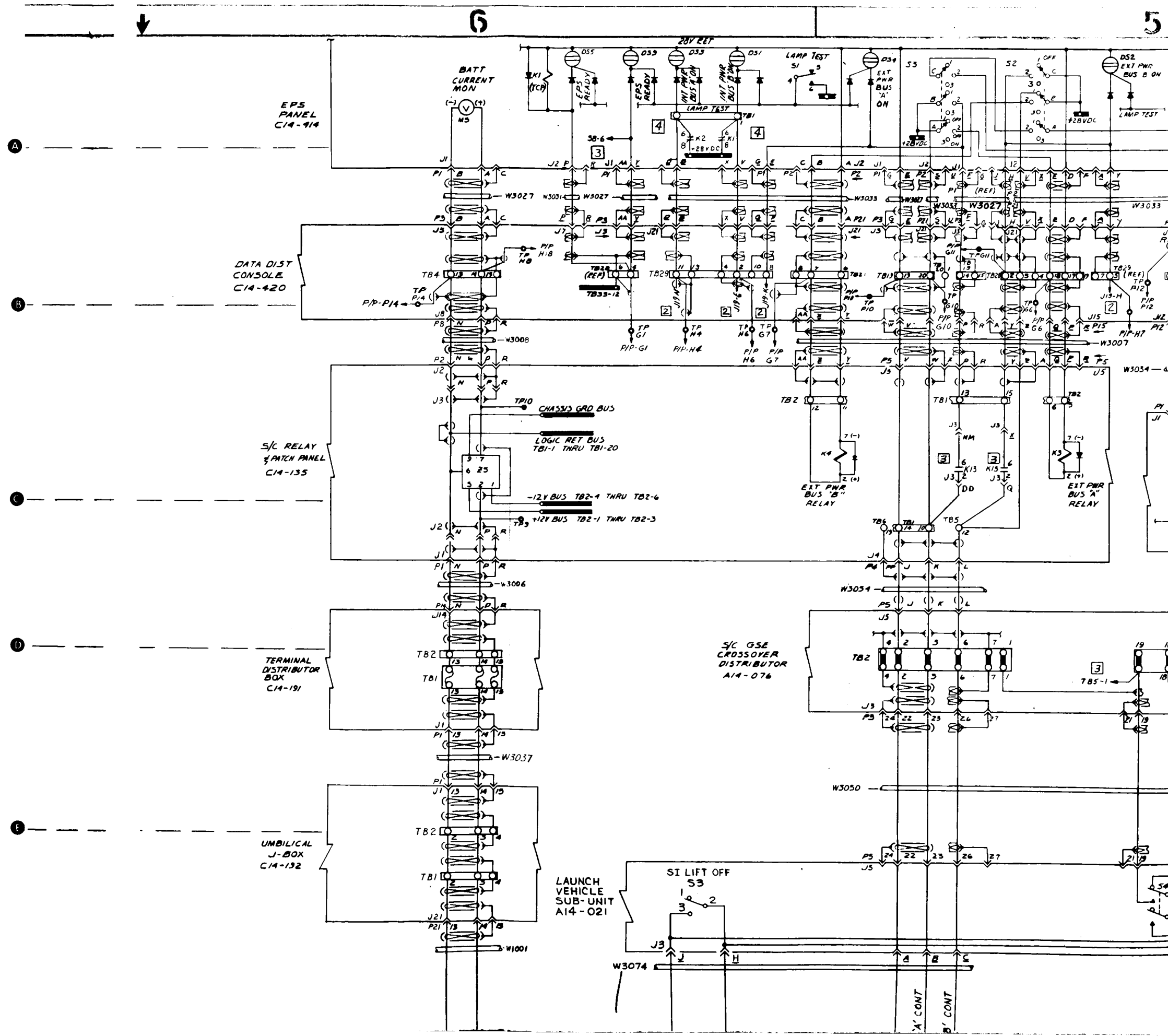
3TB4



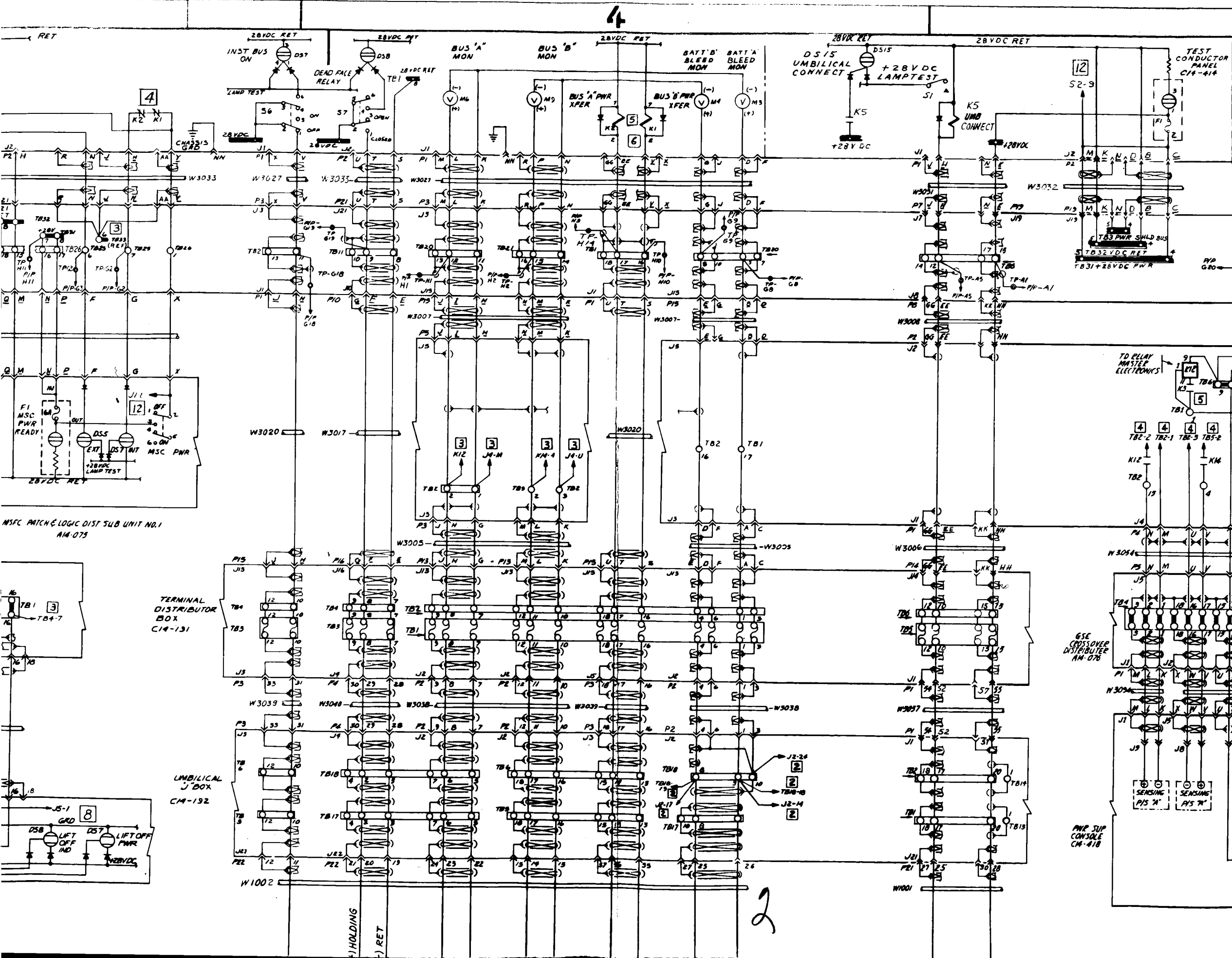
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6

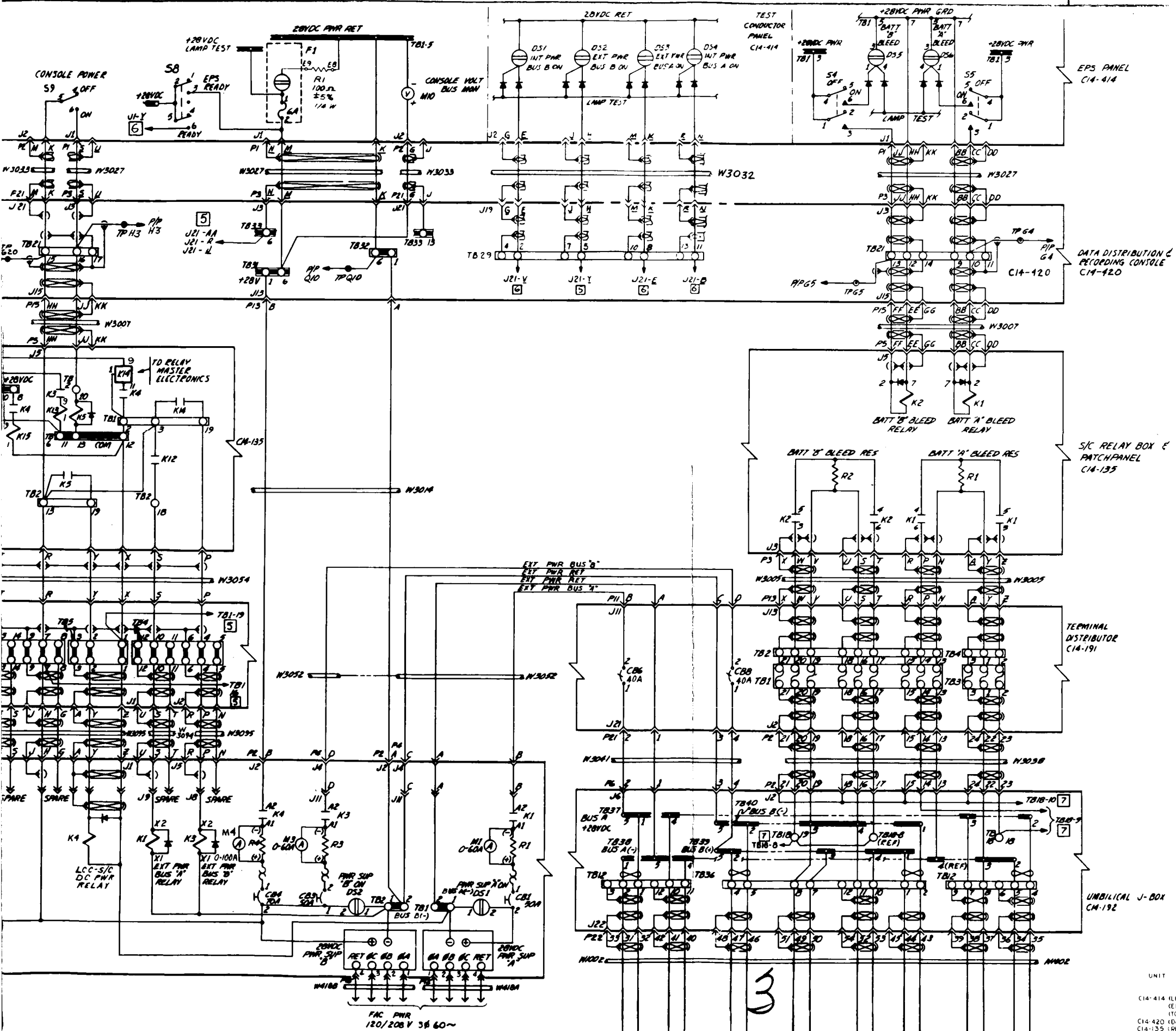






3

2



RELATED DRAWINGS

UNIT SCHEMATIC WIRING DIAGRAM

C14-414 (EPS PANEL) G16-985130C

C14-420 (DATA DIST) G16-985132A

C14-135 (RELAY BOX) G16-985128A

G16-853943B G16-853993A G16-853953A G16-850533 G16-852563





C14-192 (UMB J-BOX)  
 A14-076 (CROSSOVER DIST)  
 C14-418 (PWR SUP CONS)  
 A14-075 (MSFC)

G16-851315  
 G16-851318A  
 G16-852057  
 G16-853057  
 G16-853072  
 G16-985371  
 G16-985381  
 G16-985363A  
 G16-853067A

BOILERPLATE  
 RELAY BOX  
 POWER CONT BOX  
 SIGNAL COND BOX  
 90 x 10 COMM  
 LES SEQUENCER  
 TOWER SEQUENCER

B17-450221B  
 SX540.007  
 SX530.106  
 SX530.057  
 B14-945214  
 B15-945901C

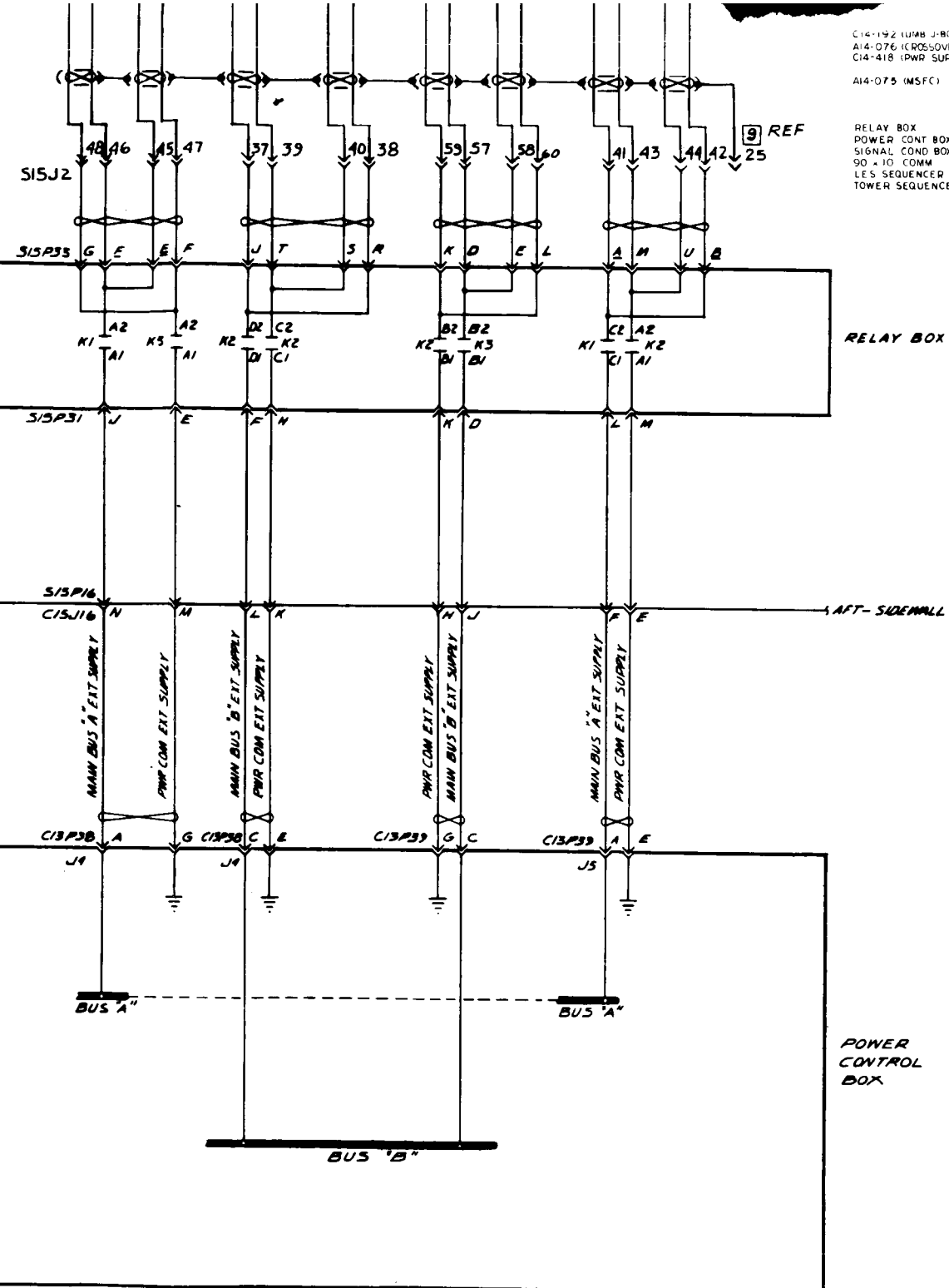


Figure 8-1. Boilerplate 15 and GSE Hangar Checkout Equipment Combined Systems Schematic (Sheet 8 of 8)

SM-2A-571



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